OPTIMIZATION OF ISOLATORS BETWEEN FLOORS OF A HIGH-RISE BUILDING

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ABSTRACT

OPTIMIZATION OF ISOLATORS BETWEEN FLOORS OF A HIGH-RISE BUILDING

Earthquake vibrations are natural phenomena that can cause tremors on the ground surface and lead to serious loss of life and property. Especially large-scale earthquakes have the potential to significantly damage infrastructure systems and the durability of structures. Several strategies are available to reduce these damages and increase the resistance of structures to earthquakes.

One of these strategies is the implementation of seismic isolators. Seismic isolation minimizes earthquake damage to structures. The main purpose of the study is to examine the effectiveness of the seismic isolator being installed at various story levels of 3D 20-story steel building model. The building had two sets of 20 evaluation models, each with a different isolator story. The first set had identical evaluation models, except for the isolation story which is incremented in each model. The second set is similar to the first set except that the lower stories are strengthened by shear walls.

The goal was to determine the best dimensions for the isolator to minimize the inter-story drift values. For this purpose, a set of 12 earthquake records are selected. These records are scaled according to the determined design spectrum. The optimization is performed for one of these earthquake records. Nonlinear dynamic analyses are carried out to evaluate the building model responses for all 12 earthquake records. Response values such as story shear forces and story drift ratios were analyzed and interpreted. This analysis will contribute to a better understanding of the impact of isolators with optimization methods on structural performance.

Keywords: Midstory isolation, Base isolation, Optimization, Opensees, Time-history analysis

ÖZET

YÜKSEK BİR BİNANIN KATLARI ARASINDA KULLANILACAK İZOLATÖRLERİN OPTİMİZASYONU

Deprem titreşimleri, zemin yüzeyinde titremelere neden olabilen ve ciddi can ve mal kaybına yol açabilen doğal olaylardır. Özellikle büyük ölçekli depremler altyapı sistemlerine ve yapıların dayanıklılığına önemli ölçüde zarar verme potansiyeline sahiptir. Bu hasarları azaltmak ve yapıların depreme karşı direncini artırmak için çeşitli strateji ve yöntemler mevcuttur.

Bu stratejilerden biri sismik izolatörlerin uygulanmasıdır. Sismik izolasyon, deprem sırasında yapılarda oluşabilecek hasarı en aza indirmek için etkili bir strateji olarak öne çıkmaktadır. Bu çalışmanın temel amacı, 3 boyutlu 20 katlı çelik çerçeve bina modelinin çeşitli kat seviyelerinde kurulan sismik izolatörün etkinliğini incelemektir. Bina modeli, her biri izolatör katının farklı olduğu 20 değerlendirme modeline sahip iki farklı sete bölünmüştür. İlk sette, her modelde artan izolasyon katı dışında değerlendirme modelleri aynıdır. İkinci set ise, izolatör altında kalan katlara perde duvar ile güçlendirilmesi dışında birinci sete benzerdir.

Amaç, en az göreli kat ötelemesi oranı değerleriyle sonuçlanan en uygun izolatör boyutlarını bulmaktır. Bu amaçla bir dizi 12 deprem kaydı seçilmiştir. Bu kayıtlar belirlenen tasarım spektrumuna göre ölçeklendirilir. Bu deprem kayıtlarından biri için optimizasyon yapılır. 12 deprem kaydının tamamında bina modeli tepkilerini değerlendirmek için doğrusal olmayan dinamik analizler yapılmaktadır. Kat kesme kuvvetleri ve göreli kat ötelemesi oranları gibi tepki değerleri analiz edildi ve yorumlandı. Bu kapsamlı analiz, optimizasyon yöntemleriyle 20 katlı bir bina için tasarlanan izolatörlerin yapısal performans üzerindeki etkisinin daha iyi anlaşılmasına katkıda bulunacaktır.

Anahtar kelimeler: Ara kat sismik izolasyonu, taban sismik izolasyonu, optimizasyon, Opensees, zaman tanım analizi

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CHAPTER 1

INTRODUCTION

1.1 Inter-story Isolation

Earthquakes are seismic waves that result from the movement of tectonic plates in the earth's crust. These waves can create tremors on the ground surface, which can result in significant loss of life and property. Large earthquakes can cause extensive damage to infrastructure and compromise the structural integrity of buildings.

Various techniques have been devised to mitigate the destructive impact of earthquakes and fortify constructions against seismic activity. Among these methods is seismic isolation, which aims to minimize the potential harm inflicted on structures during an earthquake.

Seismic isolation involves increasing the fundamental period of a structure (1st mode) and relocating it to an area where earthquake acceleration is lower. This helps to minimize any floor displacements that may occur during an earthquake by utilizing seismic isolators that have high damping, low rigidity, and high displacement capacity. Seismic isolation is a crucial technique for reducing the impact of earthquakes on structures and enhancing the safety of individuals. It is extensively utilized in engineering applications to make structures more secure in earthquake-prone areas.

Building type structures focus on two basic applications in which seismic isolators can be applied: "base isolation" and "inter-story isolation". These two applications offer different approaches to the earthquake effects of the structure. The main purpose of base isolation is to reduce the energy input to the structure by increasing the fundamental period of the structure, while the purpose of inter-story isolation is to provide additional damping by triggering the transfer of vibration energy from the substructure to the isolated superstructure (Opensees Wiki - Shell Element 2022). In addition, some of the seismic energy is absorbed by the isolators and less earthquake load is applied to the load-bearing elements of the structure.

The application of base isolators is limited to low-rise buildings, and therefore highrise buildings may not be base isolated. However, inter-story isolator systems can be used for the isolation of top-level floors of high-rise buildings.

This thesis considers the design of isolators for middle floors in buildings, as a means of mitigating the effects of earthquakes. To achieve maximum effectiveness, isolator properties must be carefully selected based on the building's dynamics. Numerous research studies (Zhou, P. and Y. 2016) (Tsuneki, et al. 2008) (Earl 2007) (Chey, et al. 2013) have been conducted on this topic, resulting in the development of several methods for optimizing inter-story isolation systems. These studies utilized two different lumped models to formulate optimized values for isolator parameters, namely a structure with two degrees of freedom and a structure with three degrees of freedom. According to Tsuneki, the ratio of superstructure mass to total structure mass has a great effect on reducing earthquake reactions in the structure (Tsuneki, et al. 2008). It is also not necessary that the rigidity of the substructure is very large. It is possible that the rigidity of the substructure will remain elastic during vibration, the seismic energy will be concentrated in the isolation layer.

In the study by Zhou, the aim was to minimize base shear forces in order to calculate isolator parameters. He used a two-degree-of-freedom system to optimize isolator parameters. It is assumed that the structural elements will remain elastic under strong ground motion, and the calculated optimum isolator parameters correspond to the equivalent stiffness and damping ratio of the isolator (Zhou, P. and Y. 2016).

In Earl's study, isolators were placed on only one floor in 4 different models: ground floor, first floor, middle floor and roof floor. As a second configuration this study considered the placement of two isolators in the building model – one at the base and one at mid-height. In another model, isolators were placed on all floors. As a result, 6 different linear elastic models were created. The isolator parameters are optimized so that the first mode period of the structure models is 2.5 seconds. (Earl 2007)

Chey considered a different approach to reduce earthquake response of a high-rise building by implementing seismic isolators. He considers the design approach for tuned mass dampers (TMD) in which the isolated top two or four floors were considered as the tuned mass and the isolator stiffness is considered as the tuned stiffness (Chey, et al. 2013).

In this study, a 20 story and three-dimensional steel frame building structure is modelled. The Bridgestone catalog is used for the optimum isolator design parameter such that story drift ratios are minimized. The isolator is placed at each story to identify the best isolator floor level. The parameters are optimized according to simulation results of one earthquake and its effectiveness is analyzed by simulations with respect to a total of 12 different scaled earthquake ground motions.

1.2 Optimization Technique

In the pursuit of optimization for seismic resilience, the Bolu Earthquake has been selected as the ground excitation. Isolator parameters are the main optimization variables, however the selection is limited to available isolators which are reported in the Bridgestone catalog (Bridgestone Corporation 2022). Thus, the optimization procedure obtained isolator rubber height, cross-sectional area, and axial compression stiffness from Table 1.1. The implementation of this table constraints the optimization process which probably leads to less optimum design, however the end product may be considered being more realistic.

For the optimal isolator location and dimensions, the floor drift ratio of the structure was found by using each type of isolator in each model after the time history analysis. According to the results obtained later, the type of isolator that gave the minimum drift ratio was accepted as the optimal type of isolator.

PRODUCT	Compressive	Effective plane area	Total rubber thickness
	(x10 ³ kN/m) stiffness	(x10 ² mm ²)	(mm)
HM060X3R	1740	2826	160,00
HM070X3R	2370	3847	159,30
HM080X3R	3140	5023	156,40
HN060X3R	1390	2826	200,00
HN070X3R	1880	3847	200,60
HN080X3R	2490	5023	197,20
HH060X4S	1700	2826	200,00
HH065X4S	2020	3317	198,00
HH070X4S	2290	3847	202,00
HH075X4S	2660	4416	200,00
HH080X4S	3030	5023	200,00
HH085X4S	3420	5671	200,00
HH090X4S	3870	6359	198,00
HH095X4S	4300	7085	198,00
HH100X4S	4700	7849	201,00
HH110X4S	5690	9480	200,00
HH120X4S	6780	11286	200,00
HH130X4S	7960	13249	200,00
HH140X4S	9230	15361	200,00
HH150X4S	10600	17638	200,00
HH160X4S	12200	20056	198,00
HH060X6R	1970	2826	200,00
HH065X6R	2340	3317	198,00
HH070X6R	2660	3847	202,00
HH075X6R	3090	4416	200,00
HH080X6R	3510	5023	200,00
HH085X6R	3970	5671	200,00
HH090X6R	4490	6359	198,00
HH095X6R	4980	7085	198,00
HH100X6R	5450	7849	201,00
HH110X6R	6590	9480	200,00
HH120X6R	7860	11286	200,00
HH130X6R	9220	13249	200,00
HH140X6R	10700	15361	200,00
HH150X6R	12300	17638	200,00
HH160X6R	14200	20056	198,00
HL060X4S	2110	2826	162,00
HL065X4S	2450	3317	163,00
HL070X4S	2760	3847	167,00

Table 1.1 Bridgestone HDR isolator parameters

(cont. on the next page)

Table 1.1 (cont.)

PRODUCT	Compressive	Effective plane area	Total rubber thickness
	(x10 ³ kN/m) stiffness	(x10 ² mm ²)	(mm)
HL075X4S	3240	4416	165,00
HL080X4S	3620	5023	168,00
HL085X4S	4110	5671	168,00
HL090X4S	4560	6359	170,00
HL095X4S	5120	7085	168,00
HL100X4S	5770	7849	165,00
HL110X4S	6890	9480	166,00
HL120X4S	8050	11286	169,00
HL130X4S	9590	13249	168,00
HL060X6R	2440	2826	162,00
HL065X6R	2840	3317	163,00
HL070X6R	3200	3847	167,00
HL075X6R	3760	4416	165,00
HL080X6R	4190	5023	168,00
HL085X6R	4760	5671	168,00
HL090X6R	5280	6359	170,00
HL100X6R	6680	7849	165,00
HL110X6R	7990	9480	166,00
HL120X6R	9330	11286	169,00
HL130X6R	11100	13249	168,00
HT090X4S	3040	6359	252,00
HT095X4S	3420	7085	250,00
HT100X4S	3810	7849	248,00
HT110X4S	4520	9480	252,00
HT120X4S	5470	11286	248,00
HT130X4S	6310	13249	252,00
HT140X4S	7450	15361	247,00
HT150X4S	8480	17638	250,00
HT160X4S	9690	20056	250,00
HT090X6R	3530	6359	252,00
HT095X6R	3960	7085	250,00
HT100X6R	4420	7849	248,00
HT110X6R	5240	9480	252,00
HT120X6R	6340	11286	248,00
HT130X6R	7310	13249	252,00
HT140X6R	8640	15361	247,00
HT150X6R	9830	17638	250,00
HT160X6R	11200	20056	250,00
HS070X4S	3290	3847	141,00
HS075X4S	3550	4416	150,00

(cont. on the next page)

Table 1.1 (cont.)

DRODUCT	Compressive	Effective plane area	Total rubber thickness
PRODUCT	(x10 ³ kN/m) stiffness	(x10 ² mm ²)	(mm)
HS080X4S	3730	5023	162,00
HS085X4S	4000	5671	171,00
HS090X4S	4260	6359	180,00
HS095X4S	4440	7085	192,00
HS100X4S	4700	7849	201,00
HS110X4S	5120	9480	222,00
HS120X4S	5650	11286	240,00
HS130X4S	6100	13249	261,00
HS140X4S	6620	15361	279,00
HU150X4S	7280	17638	298,00
HD160X6R	8690	20056	322,00
HD170X6R	9890	22641	322,00
HD180X6R	10900	25328	322,00

CHAPTER 2

APPLICATION OF TWENTY STORY BUILDING

2.1 Example Model

In this study, a 20-storey building was modeled from Medina (Medina and Mathiasson 2014). The building is designed for office and first floor has a height of 4.57 meters and all other story has 3.96. The overall dimensions of the building are 58x36.58 meters and the total height is 79.8 meters. The column application plan of the building is shown in Figure 2.1. In the design of the building, steel structural elements were used in accordance with the (ASCE 7-10 2010), (ANSI/AISC 341-10 2010), and (ANSI/AISC 360-10 2010) regulations. Three-dimensional structure was analyzed for optimization using OpenSeesPy and the necessary analyzes were made and compared for the optimum isolator parameters and location.

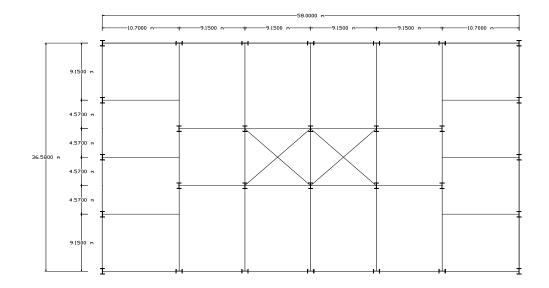


Figure 2.1 Plan view of the structure

The sectional characteristics are delineated in Table 2.1. Each beam exhibits uniformity within the same floor level, whereby identical sections are employed across identical floors. For instance, the W36X282 section is utilized for the first story, while the W24X94 section is designated for the twentieth story. Within each story, the columns are categorized into two distinct groups: inner columns and outer columns. Inner columns share identical section properties, ensuring uniformity within their designated group. Also, outer columns exhibit same section properties across the entirety of the same floor level. Steel profile properties are presented in

Table 2.2. Building floors were given 407 kgf/m2 dead load and 243 kgf/m2 live load. This load is treated as structure load in OpenSeespy software. In OpenSeespy, steel columns and beams were designed as "ElasticTimoshenkoBeam" elements, and reinforced concrete shear walls were used as "ShellMITC4" elements and "ElasticMembranePlateSection" material properties.

Story	Beams	Interior columns	Exterior columns
20	W24X94	W36X231	W36X231
19	W24X103	W36X231	W36X231
18	W30X148	W36X231	W36X231
17	W30X148	W36X231	W36X231
16	W36X182	W36X247	W36X231
15	W36X182	W36X247	W36X231
14	W36X194	W36X302	W36X262
13	W36X194	W36X302	W36X262
12	W36X232	W36X330	W36X302
11	W36X232	W36X330	W36X302
10	W36X256	W36X395	W36X361
9	W36X256	W36X395	W36X361
8	W36X256	W36X395	W36X395
7	W36X256	W36X395	W36X395
6	W36X262	W36X441	W36X487
5	W36X262	W36X441	W36X487
4	W36X282	W36X487	W36X529
3	W36X282	W36X487	W36X529
2	W36X282	W36X487	W36X652
1	W36X282	W36X487	W36X652

Section Name	Material	Area	Torsional Constant	Moment of Inertia (Major)	Moment of Inertia (Minor)	Shear Area (Minor)	Shear Area (Major)
		m²	m ⁴	m ⁴	m ⁴	m²	m²
W24X103	S355	0.019548	0.000002943	0.001249	0.00005	0.008694	0.009484
W24X94	S355	0.017871	0.000002189	0.001124	0.000045	0.008074	0.008534
W30X148	S355	0.028064	0.000006035	0.00278	0.000094	0.012874	0.013323
W36X182	S355	0.034581	0.0000077	0.004703	0.000144	0.016979	0.015353
W36X194	S355	0.036774	0.00000924	0.005036	0.000156	0.018014	0.016394
W36X231	S355	0.043935	0.000012	0.006493	0.000391	0.017897	0.022355
W36X232	S355	0.043935	0.000016	0.006243	0.000195	0.020824	0.020427
W36X247	S355	0.046774	0.000014	0.006951	0.00042	0.018942	0.023952
W36X256	S355	0.048645	0.000022	0.006993	0.00022	0.023164	0.022695
W36X262	S355	0.049677	0.000017	0.007451	0.000454	0.019997	0.025703
W36X282	S355	0.053484	0.000022	0.008158	0.000499	0.021183	0.028024
W36X302	S355	0.05729	0.000027	0.008782	0.000541	0.022741	0.030168
W36X330	S355	0.062581	0.000035	0.009698	0.000591	0.024809	0.033021
W36X361	S355	0.068387	0.000045	0.010697	0.000653	0.027458	0.036093
W36X395	S355	0.074839	0.000059	0.011863	0.000728	0.030224	0.039742
W36X441	S355	0.083871	0.000081	0.013361	0.000828	0.034132	0.044602
W36X487	S355	0.092258	0.000107	0.014984	0.000937	0.038032	0.049277
W36X529	S355	0.100645	0.000136	0.016483	0.001036	0.041341	0.053819
W36X652	S355	0.123871	0.000247	0.021061	0.001344	0.052237	0.066993

Table 2.2 Properties of the steel sections

20 models were prepared to optimize the isolator parameters and location for midstory (19 models) and base isolation (1 models), and in each model the isolator was positioned on a different floor. "KikuchiAikenHDR" material was used for the isolator and the isolator was defined with the "twoNodeLink" element. 'X0.6' was used as the elastomer type and optimum isolator parameters were tried to be found by changing the elastomer area and rubber height. The "ElasticTimoshenkoBeam" element used for steel columns and beams is modeled based on the Timoshenko–Ehrenfest beam theory, taking into account the shear deformation effect that will occur in the element. The "ShellMITC4" element used in the modeling of reinforced concrete shear walls is modeled using the bilinear isometric formulation with modified shear interpolation to improve the thin plate bending performance [10]. The "ElasticMembranePlateSection" section is section where we can define the plate assigned to the "ShellMITC4" element mass

of the element suitable for the Shell element. The model will be defined in openseespy with the elements defined here and optimization will be made with time history analysis.

2.2 Earthquake Time Histories

This section provides detailed information about earthquakes used to analyze the structure in the time history. A total of 12 different earthquakes were used in the structural analysis and these earthquakes are as follows:

- EQ1. Menderes(Izmir, Turkey) Earthquake of November 06, 1992
- EQ2. Seferihisar(Izmir, Turkey) Earthquake of October 20, 2020
- EQ3. Karaburun(Izmir, Turkey) Earthquake of June 12, 2020
- EQ4. The Chi-Chi (Taiwan) Earthquake of September 20, 1999
- EQ5. The Friuli (Italy) Earthquake of May 06, 1976
- EQ6. The Hollister (USA) Earthquake of April 09, 1961
- EQ7. The Imperial Valley (USA) Earthquake of October 15, 1979
- EQ8. The Kobe (Japan) Earthquake of January 16, 1995
- EQ9. The Kocaeli (Turkey) Earthquake of August 17, 1999
- EQ10. The Northridge (USA) Earthquake of January 17, 1994
- EQ11. Pazarcık (Kahramanmaras, Turkey) Earthquake of February 06, 2023
- EQ12. The Bolu (Turkey) Earthquake of November 11, 1999

Of these 12 earthquakes, 9 are known important earthquakes and the remaining 3 are important major earthquakes that occurred in Izmir, Turkey. Additionally, earthquakes were recorded with a step interval of 0.01 seconds.

The earthquake data have been scaled according to the earthquake design spectrum used for the structure design which is presented in Figure 2.2. The conceptual reason is to obtain maximum displacements within the same range, so that the effective isolator stiffness does not significantly vary among the different earthquake excitations. TEC 2018 regulation was used to create earthquake design spectra. The coordinates of the

building location is selected as 38.380151, 27.191009, and the earthquake ground motion level was taken as DD-2. DD-2 ground motion level corresponds to a 10% probability of being exceeded in 50 years with a recurrence period of 475 years. Accordingly, the short-term map spectral acceleration (Ss) was taken as 1.093 and the 1-second period map spectral acceleration (S1) was taken as 0.267. The soil class was chosen as ZD whose features are as follows:

- The average shear wave velocity (Vs)30 is between 180-360 m/s.
- The average standard penetration number of blows (N60)30 pulses/30cm is between 15-50.
- The average undrained shear strength (cu)30 kPa is between 70-250.

According to TBDY 2018, the short period design spectral acceleration coefficient (SDS) is calculated as 1.162, the design spectral acceleration coefficient (SD1) for the 1.0 second period is calculated as 0.552, and the corner periods of the horizontal elastic design acceleration spectrum, T_A and T_B , are 0.095 s and 0.475 s, respectively. T_L , which is the transition period to the constant displacement region in the horizontal elastic design spectrum, is 6 seconds. By substituting these data in Figure 2.2, the horizontal elastic design acceleration graph was obtained, and Figure 2.3 was obtained for the DD-2 earthquake ground motion level.

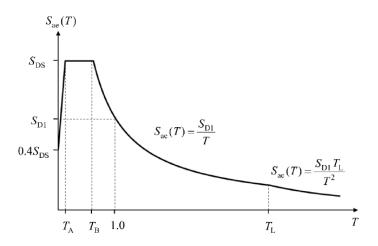


Figure 2.2 Horizontal design spectrum from TEC 2018

The scaling process was done by determining the range that would be suitable for the fundamental period of all building models. SeismoMatch (Seismosoft 2023) program was used to scale earthquake data and this software uses the algorithm developed by Al Atik & Abrahamson (Atik and Abrahamson 2010) . In this algorithm, to avoid the possibility of drift in the tuned velocity and displacement time series, a tuning waveform with zero integral for velocity and displacement is selected.

The earthquakes to be used for optimization have been scaled based on the design spectral acceleration graph (Figure 2.3) used when the structure was initially designed, and this scaling process covers the range of 1.4-6 seconds. Scaled and unscaled versions of earthquake spectral accelerations are given in Figure 2.5 and Figure 2.3, respectively. Additionally, the scaled period region is shown in more detail in its scaled version in Figure 2.6 and its unscaled version in Figure 2.4. Earthquake ground motion parameters are given in and Table 2.4 for unscaled and scaled earthquakes, respectively.

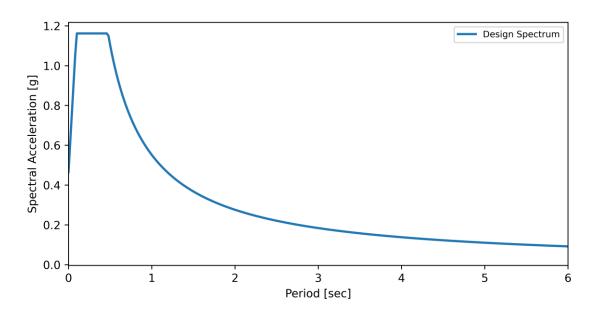


Figure 2.3 Design horizontal spectrum of 3D structure

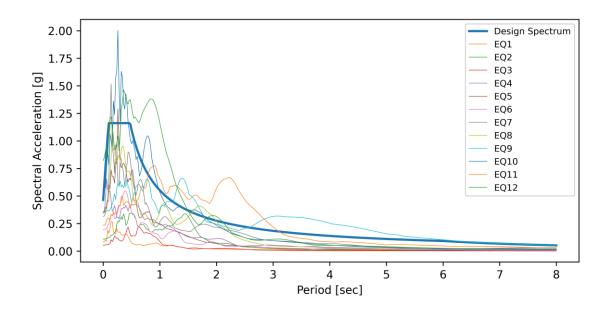


Figure 2.4 Unmatched Spectral Acceleration for all Earthquake

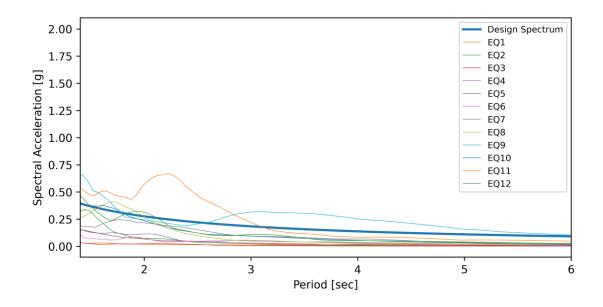


Figure 2.5 Close look unmatched Spectral Acceleration for all Earthquake

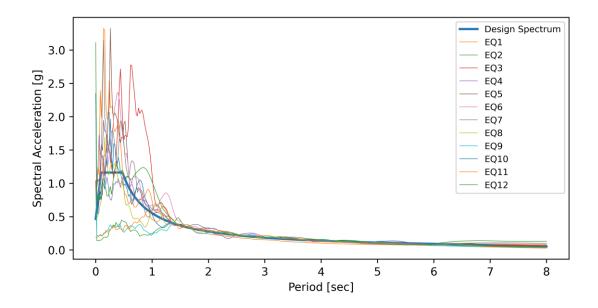


Figure 2.6 Matched Spectral Acceleration for all Earthquake

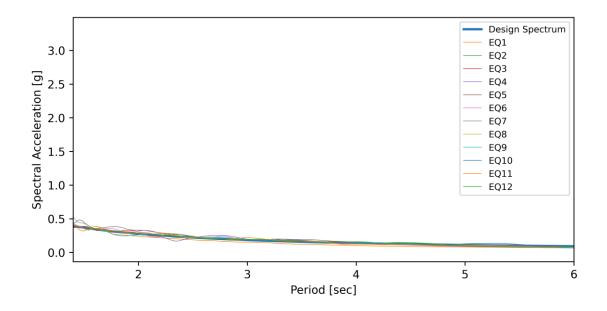


Figure 2.7 Close look matched Spectral Acceleration for all Earthquake

		0	iround Mot	ion Parame	Ground Motion Parameter for Original Accelerograms	ginal Accele	erograms					
Accelerogram	1	2	3	4	5	9	7	8	6	10	11	12
Max Aceleration (g)	0.08376	0.10838	0.05426	0.361	0.3513	0.1948	0.3152	0.3447	0.349	0.5683	0.23573	0.82243
Max Velocity (cm/sec)	7.27379	17.08519	4.84319		21.54766 22.01953		31.49599	12.35471 31.49599 27.67793	62.18167	51.82672	58.08495	62.10125
Max Displacement (cm)	5.54122	2.89623	1.51534	21.88302	4.0671	4.30014	14.12637	9.69435	51.30239	9.0347	32.11539	13.55936
Vmax/Amax (sec)	0.08853	0.1607	0.09099	0.06084	0.06389	0.06465	0.10186	0.08185	0.18162	0.09296	0.25118	0.07697
Acceleration RMS (g)	0.01366	0.01432	0.0065	0.02148	0.03733	0.02046	0.04559	0.05174	0.04954	0.06667	0.04352	0.05311
Velocity RMS (cm/sec)	1.58103	2.33691	0.71355	4.08563	2.87789	2.732	6.56596	6.30432	17.19039	7.274	10.44089	7.72856
Displacement RMS (cm)	2.50511	0.5949	0.21039	6.46829	0.83609	1.14019	5.18814	2.29461	15.00798	2.38022	5.13369	2.85096
Arias Intensity	0.06537	0.33178	0.0799	0.37522	0.78025	0.25754	1.2646	1.68744	1.32244	2.7321	2.41567	2.43008
Characteristic Intensity	0.00761	0.01756	0.00581	0.02287	0.04348	0.01849	0.06116	0.07527	0.0652	0.10872	0.0826	0.09152
Specific Energy Density (cm2/sec)	56.81689	573.4207	62.43773	881.1901	300.8952	298.1053	1702.485	1625.944	10333.97	2110.622	9024.036	3338.939
Cum. Abs. Velocity (cm/sec)	194.8873	677.5817	382.8608	500.1236	557.1354	458.6146 891.5995	891.5995	1161.368	991.3535	1292.805	2189.896	1165.445
Acc Spectrum Intensity (g*sec)	0.06598	0.09822	0.04977	0.15579	0.30148	0.16194	0.3366	0.32993	0.21397	0.52434	0.15777	0.47956
Vel Spectrum Intensity (cm)	18.56124	80.12688	25.0747	80.72922	93.48024	56.81163	139.6276	153.5786	168.0304	212.5725	264.1482	255.4487
Housner Intensity (cm)	16.75999	73.51774	22.4872	73.31293	22.4872 73.31293 73.07337	51.60288	124.0143	51.60288 124.0143 141.6449	176.1751	$176.1751 \ 184.0054 \ 269.1029$	269.1029	237.1019
Sustained Max.Acceleration (g)	0.05328	0.10425	0.04551	0.19	0.2628	0.0712	0.2717	0.2664	0.2046	0.4121	0.22221	0.33321
Sustained Max.Velocity (cm/sec)	4.64224	13.23406	4.0712	14.67576 14.06116	14.06116	9.0664	23.10157	9.0664 23.10157 23.63425	40.54963	32.69281	42.75458	26.32703
Effective Design Acceleration (g)	0.07795	0.10603	0.05323	0.22432	0.32878	0.19825	0.33328	0.32884	0.32705	0.59429	0.22967	0.78601
A95 parameter (g)	0.00008	0.00011	0.00005	0.23176	0.24134	0.14376	0.23514	0.22785	0.23174	0.41088	0.17067	0.65877
Predominant Period (sec)	0	0	0	0	0	0	0	0	0	0	0.9	0
Significant Duration (sec)	9.19	20.59	27.27	11.78	4.24	16.53	8.92	12.86	15.62	90.6	38.02	9.35

Table 2.3 Ground motion parameters for unmatched accelerograms

Accelerogram 1 2 3 4 5 6 7 8 9 10 11 Max Acceleration (g) 1.03333 0.13933 0.32315 0.23756 0.48103 0.27728 0.54363 0.110130 2.73553 Max Aceleration (g) 1.03333 0.13933 0.13933 0.58403 0.92877 0.93956 0.7005 0.48103 0.27788 0.54363 2.73659 Max Nisplacement (cm) 68.75962 3.134555 5.60073 6.040607 148.517 1.128393 2.03149 0.15952 0.13933 0.03169 0.07547 0.03169 0.05723 0.09958 0.09958 0.097547 0.03169 0.07577 1.13202 9.2005 Vinas Intensity 0.16952 7.23358 10.5718 1.1.48306 15.1114 12.77469 1.1.9702 9.2005 Vinas Intensity 0.166501 0.92283 1.2.7474 1.84806 1.7.4418 1.3.4836 1.1.4122 1.1.9202 9.2005 Vinas Intensity 0.106501		Ground Motion Parameter for Matched Accelerograms	ion Parame	ter for Mat	ched Accel	erograms					
	1 2		4	5	9	7	8	6	10	11	12
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			0.92872	0.93916	0.83966	0.7005	0.48103	0.20728	0.54363	0.19159	0.72803
68.75962 23.18455 42.60773 60.40607 148.5187 37.68838 0.08853 0.28673 0.0973 0.06954 0.00958 0.16952 0.231845 0.09121 0.05722 0.09798 0.09088 19.61855 7.23586 10.67018 12.74746 11.84806 15.19197 31.08522 5.70287 5.91772 17.21362 90.67396 21.34777 31.08522 5.70287 5.91772 17.21362 90.67396 21.34777 31.08522 5.70287 5.91772 17.21362 90.67396 21.34777 31.08522 5.70287 5.91772 17.21362 90.67396 21.3477 31.08522 5.70287 5.91772 17.21362 90.67396 21.31719 31.08522 5.70289 12.46517 2639587 5.91772 17.21362 31.08543 0.09524 1240.711 207391 0.17349 0.17349 230.3216 1543017 0.12466 0.609168 0.71391 0.6996 <	90.25864	9 62.40637	60.4348	75.72411	57.28178	65.93892	50.64314	38.93431	63.60308	48.78211	57.02457
	68.75962	5 42.60773		148.5187	37.68838	29.0631	93.87589	27.74894	227.1141	22.73659	121.7577
			0.06633	0.08219	0.06954	0.09595	0.10732	0.19148	0.11926	0.25955	0.07984
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			0.05722	0.09798	0.09088	0.09486	0.07547	0.03169	0.06723	0.03206	0.0519
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	19.61855				15.19197		16.17242	10.96517	11.9202	9.2005	12.64193
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	31.08522			90.67396	21.34777	13.12498	56.25012	10.01777	131.1372	6.09185	71.26817
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			2.66353	5.37403	5.08302	5.47624	3.59084	0.54118	2.77869	1.31078	2.31993
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.33275		0.09945	0.18485	0.17314	0.18361	0.13262	0.03336	0.11011	0.05222	0.08839
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	8748.491				9217.99	8456.406	10699.9	4204.615	5668.017	7007.264	8933.844
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	2418.054	1 4731.231	1445.718	1490.271	2077.495	1879.933	1785.698	645.3177	1785.698 645.3177 1306.594	1671.887	1467.305
230.3216 137.1995 312.1866 209.8993 253.5204 254.6178 261.5799 19 207.9705 142.7059 290.9 196.5347 218.6295 240.6011 228.8583 0.66109 0.12677 0.58421 0.51531 0.65213 0.31208 0.58433 0 57.60433 30.54071 60.12241 40.35156 39.48643 52.88832 48.98421 45 0.96724 0.13791 0.67413 0.57122 0.88233 0.85488 0.73902 0 0.906724 0.13791 0.67413 0.57122 0.88233 0.85488 0.73902 0 0.00104 0.00018 0.57324 0.63769 0.60959 0.50226 0 0.14 0 0 0 0.26 0 0.14	0.8187			0.77891	0.6996	0.71192	0.46837	0.12651	0.5178	0.11888	0.42326
207.9705 142.7059 290.9 196.5347 218.6295 240.6011 228.8583 0.666109 0.12677 0.58421 0.51531 0.65213 0.31208 0.58433 0 57.60433 30.54071 60.12241 40.35156 39.48643 52.88832 48.98421 45 0.96724 0.13791 0.67413 0.57122 0.88233 0.85548 0.73902 0 0.00104 0.00014 0.00068 0.58324 0.63769 0.60959 0.50226 0 0.14 0 0.14 0 0 0.14 0 0.14	230.3216					261.5799	195.0182	127.8504	215.7006	164.0383	235.7832
0.66109 0.12677 0.58421 0.51531 0.65213 0.31208 0.58433 57.60433 30.54071 60.12241 40.35156 39.48643 52.88832 48.98421 4 0.96724 0.13791 0.677112 0.88233 0.8548 0.73902 0.00104 0.00018 0.57122 0.88233 0.60959 0.50226 0.0114 0.00068 0.58324 0.63769 0.60959 0.50226 0.14 0 0 0 0.26 0.26726 0.1348	207.9705			218.6295	240.6011	228.8583	183.42	183.42 137.3222	196.4173	164.4677	234.9426
57.60433 30.54071 60.12241 40.35156 39.48643 52.88832 48.98421 0.96724 0.13791 0.67413 0.57122 0.88233 0.8548 0.73902 0.00104 0.000068 0.58324 0.63779 0.60959 0.50226 0.14 0 0.0026 0.58324 0.26 0 0.14	0.66109		0.51531	0.65213	0.31208	0.58433	0.40254	0.13213	0.44726	0.13314	0.1875
0.96724 0.13791 0.67413 0.57122 0.88233 0.8548 0.73902 0.00104 0.00068 0.58324 0.63769 0.60959 0.50226 0.14 0 0 0 0 0.14 0	57.60433		40.35156	39.48643	52.88832	48.98421	45.64708	23.93374	36.10406	30.09603	39.28817
0.00104 0.00014 0.00068 0.58324 0.63769 0.60959 0.50226 0.14 0 0 0 0 0.14	0.96724		0.57122	0.88233	0.8548	0.73902	0.45732	0.19423	0.56961	0.18828	0.69523
0.14 0 0 0 0.26 0			0.58324	0.63769	0.60959	0.50226	0.33239	0.12457	0.40881	0.11361	0.56277
		0	0	0.26	0	0.14	0	0	0	0.92	0
Significant Duration (sec) 9.19 46.28 26.65 15.77 4.58 17.09 9.37	9.19		15.77	4.58	17.09	9.37	16.04	14.77	60.6	38.61	19.72

Table 2.4 Ground motion parameters for matched accelerograms

CHAPTER 3

TIME HISTORY ANALYSIS FOR BUILDING WITHOUT ISOLATOR

3.1 Earthquake Load Analysis

This section presents the results of the time history analysis performed using Openseespy for the building defined in the Example model section. These results will be compared with the optimization of the isolator structure to be made later, and the results will be examined and interpreted in detail. Analyzes were carried out in the time domain, and structure analysis was performed using the Newmark-Beta method. Alpha and beta coefficients were chosen as 0.5 and 0.25, respectively, in accordance with the average acceleration method. The structure is modeled as a 3D moment frame. Additionally, analyzes were made by taking into account PDelta effects, which expresses the effect of increasing bending moment due to horizontal displacement. The structure, whose 3D view is shown in Figure 3.1, was subjected to time history analysis using 12 different earthquake ground motions.

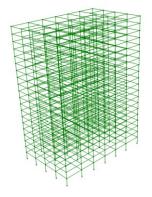


Figure 3.1 3D view of the structure

The modal properties of the structure are presented for the first 20 modes in Table 3.1 Modal properties of which include natural frequency, cyclic frequency, and period. Additionally, the modal participation factor for the first 20 modes in the horizontal (MX and MY), vertical (MZ) and rotational (RMX, RMY and RMZ) directions is shown in Table 3.2.

Mode	Lambda	Omega	Frequency [Hz]	Period [sec]
1	5.874	2.424	0.386	2.593
2	7.334	2.708	0.431	2.320
3	11.165	3.341	0.532	1.880
4	40.322	6.350	1.011	0.989
5	52.484	7.245	1.153	0.867
6	76.621	8.753	1.393	0.718
7	103.607	10.179	1.620	0.617
8	122.897	11.086	1.764	0.567
9	124.279	11.148	1.774	0.564
10	124.579	11.162	1.776	0.563
11	138.117	11.752	1.870	0.535
12	149.571	12.230	1.946	0.514
13	166.611	12.908	2.054	0.487
14	175.414	13.244	2.108	0.474
15	215.239	14.671	2.335	0.428
16	233.999	15.297	2.435	0.411
17	269.235	16.408	2.611	0.383
18	297.799	17.257	2.747	0.364
19	330.945	18.192	2.895	0.345
20	384.050	19.597	3.119	0.321

Table 3.1 Modal properties of uncontrolled building

Table 3.2, where the horizontal participation factor corresponds to the modal participation due to a unit excitation along the horizontal direction. Similarly, the vertical and rotational participation factors are obtained for unit vertical and rotational excitations, respectively. Among the first 20 modal responses, it is expected that modes 1, 2, 4, 5, 8, 11, 12, 14, 16, 18, 19 will have a larger vibrational contribution during horizontal excitations.

Based on Figure 3.2 and Table 3.2, we can conclude that the horizontal mode shape is dominant in the first, second, fourth and fifth modes. This conclusion is supported

by the fact that the horizontal modal participation factor is larger than the vertical modal participation factor in these modes. On the other hand, the vertical mode shape is observed to be dominant in the 10th, 13th and 20th modes. Also, rotational mode shapes are dominant in the 3rd, 6th, 9th, 15th and 17th.

		Moc	lal Participatio	n Factors		
Mode	MX	MY	MZ	RMX	RMY	RMZ
1	4195.11	0	0	0	55947.6	0
2	0	4164.99	0	-57572.1	0	9.56E-08
3	0	0	0	0	0	90451.8
4	1668.36	0	0	0	-71033.4	0
5	0	1729.41	0	70762.6	0	0
6	0	0	0	0	0	-35545.1
7	928.093	0	0	0	-33026.9	0
8	0	51.9358	0	1673.48	0	0
9	0	0	0	0	0	7132.93
10	0	0	75.1231	0	0	0
11	421.74	0	0	0	-12951.9	0
12	0	1034.29	0	35303.1	0	0
13	0	0	54.406	0	0	0
14	-502.85	0	0	0	17243.2	0
15	0	0	0	0	0	-21674.9
16	610.119	0	0	0	-28615.4	0
17	0	0	0	0	0	-2644.61
18	0	-775.753	0	-32296.4	0	0
19	-458.366	0	0	0	13046.6	0
20	0	0	-2625.93	0	0	0

Table 3.2 Modal participation factors

The structure is simulated with respect to twelve scaled horizontal earthquake records, and the maximum drift ratios are indicated in Table 3.3. The largest drift ratio occurs due to earthquake 3, the maximum drift ratio due to each earthquake is different, and they are not close to each other. Further, the maximum story shear force is given in Table 3.4. The largest maximum story shear force is 8,674 tf, while the smallest is 5,039 tf. As a conclusion, scaling the earthquake data does not result in the same order of structural responses.

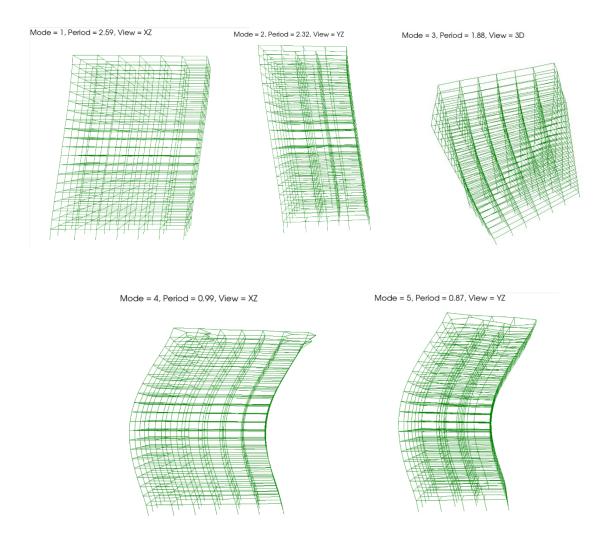


Figure 3.2 First 5 mode shapes for uncontrolled building

				DRIF	DRIFT RATIOS	S						
						EQ DATA	ATA					
STORY	-	2	3	4	5	9	٢	8	6	10	11	12
1	0.39%	0.50%	0.67%	0.54%	0.63%	0.46%	0.39%	0.50%	0.40%	0.54%	0.49%	0.53%
2	0.57%	0.79%	1.06%	0.86%	0.99%	0.72%	0.62%	0.79%	0.64%	0.85%	0.77%	0.84%
3	0.63%	0.89%	1.19%	0.96%	1.08%	0.81%	0.69%	0.89%	0.73%	0.96%	0.86%	0.95%
4	0.64%	0.91%	1.22%	0.99%	1.05%	0.82%	0.70%	0.91%	0.76%	0.98%	0.89%	0.97%
5	0.66%	0.96%	1.26%	1.03%	1.05%	0.84%	0.71%	0.95%	0.80%	1.03%	0.93%	1.02%
9	0.65%	0.97%	1.24%	1.05%	1.00%	0.84%	0.70%	0.96%	0.81%	1.04%	0.94%	1.03%
7	0.64%	1.01%	1.22%	1.09%	0.94%	0.86%	0.72%	1.00%	0.84%	1.09%	0.93%	1.08%
8	0.63%	1.00%	1.10%	1.08%	1.01%	0.84%	0.72%	0.99%	0.82%	1.08%	0.88%	1.07%
6	0.62%	0.99%	1.09%	1.07%	1.14%	0.89%	0.73%	0.97%	0.80%	1.06%	0.91%	1.05%
10	0.63%	0.96%	1.04%	1.04%	1.22%	0.91%	0.74%	0.94%	0.76%	1.03%	0.90%	1.02%
11	0.72%	0.99%	1.13%	1.07%	1.35%	1.00%	0.79%	0.97%	0.77%	1.05%	0.94%	1.05%
12	0.80%	0.96%	1.15%	1.05%	1.36%	1.03%	0.79%	0.95%	0.75%	1.04%	0.95%	1.03%
13	0.90%	0.98%	1.27%	1.06%	1.46%	1.10%	0.79%	0.97%	0.76%	1.20%	1.00%	1.04%
14	0.95%	0.95%	1.45%	1.03%	1.51%	1.11%	0.76%	0.95%	0.74%	1.29%	1.00%	1.03%
15	0.98%	0.92%	1.66%	1.03%	1.53%	1.10%	0.74%	0.92%	0.73%	1.37%	1.02%	1.19%
16	0.92%	0.84%	1.76%	1.03%	1.41%	1.03%	0.70%	0.85%	0.69%	1.33%	0.98%	1.26%
17	0.95%	0.80%	1.92%	1.10%	1.31%	1.00%	0.71%	0.82%	0.69%	1.30%	0.98%	1.38%
18	1.03%	0.75%	1.99%	1.14%	1.30%	0.97%	0.73%	0.77%	0.68%	1.28%	1.06%	1.42%
19	1.03%	0.68%	1.92%	1.12%	1.39%	0.90%	0.73%	0.70%	0.64%	1.22%	1.30%	1.38%
20	1.16%	0.65%	2.02%	1.18%	1.60%	1.12%	0.80%	0.68%	0.68%	1.25%	1.62%	1.47%
MAX DRIFT RATIO	1.16%	1.01%	2.02%	1.18%	1.60%	1.12%	0.80%	1.00%	0.84%	1.37%	1.62%	1.47%

Table 3.3 Maximum drift ratios for uncontrolled building in each earthquake data

				STORY	92	RS [tf]						
						EQ DATA	ATA					
STORY	-	7	m	4	S	9	7	~	6	10	11	12
1	5,308	6,401	8,674	6,970	8,082	5,962	5,039	6,398	5,134	6,883	6,498	6,811
2	4,713	6,335	8,652	6,882	8,088	5,848	5,005	6,311	5,198	6,819	6,359	6,742
3	4,579	6,247	8,639	6,768	7,861	5,703	4,943	6,228	5,230	6,726	6,305	6,648
4	4,498	6,132	8,552	6,628	7,356	5,527	4,792	6,117	5,203	6,602	6,290	6,524
5	4,399	5,989	8,311	6,463	6,962	5,320	4,532	5,970	5,111	6,443	6,242	6,369
9	4,140	5,817	7,863	6,272	6,351	5,085	4,252	5,788	4,955	6,252	6,025	6,185
7	3,754	5,615	7,180	6,051	5,563	4,822	4,016	5,569	4,748	6,027	5,563	5,969
8	3,427	5,383	6,293	5,800	5,479	4,535	3,981	5,314	4,504	5,769	4,982	5,722
6	3,225	5,120	5,834	5,521	6,089	4,554	3,856	5,028	4,230	5,480	4,990	5,442
10	3,247	4,826	5,467	5,212	6,445	4,599	3,827	4,724	3,930	5,159	4,889	5,132
11	3,431	4,505	5,176	4,874	6,503	4,600	3,744	4,410	3,612	4,809	4,533	4,793
12	3,616	4,161	5,135	4,511	6,239	4,530	3,529	4,084	3,298	4,617	4,334	4,429
13	3,726	3,788	5,126	4,117	6,134	4,369	3,166	3,746	3,014	4,834	4,157	4,034
14	3,700	3,398	5,491	3,702	5,931	4,105	2,789	3,396	2,759	4,922	3,701	3,920
15	3,505	2,983	5,843	3,612	5,518	3,731	2,476	3,013	2,499	4,808	3,499	4,221
16	3,084	2,548	5,886	3,436	4,802	3,265	2,186	2,595	2,221	4,408	3,166	4,276
17	2,687	2,087	5,591	3,183	3,835	2,763	1,937	2,141	1,925	3,707	2,693	4,053
18	2,519	1,608	4,917	2,826	3,162	2,275	1,757	1,665	1,606	3,125	2,657	3,538
19	2,040	1,100	3,778	2,222	2,865	1,944	1,417	1,155	1,245	2,374	2,813	2,717
20	1,227	600	2,193	1,320	1,978	1,337	869	637	742	1,363	2,045	1,596
MAX STORY SHEAR	5,308	6,401	8,674	6,970	8,088	5,962	5,039	6,398	5,230	6,883	6,498	6,811

Table 3.4 Story shears for uncontrolled building in each earthquake data

L

CHAPTER 4

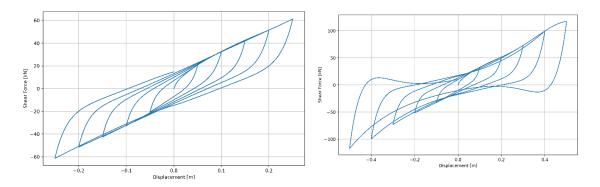
IMPROVEMENTS WITH INTERSTORY ISOLATION

4.1 Example Model

In this section, we will provide an overview of the 20-storey building that is planned to be optimized with isolators. Additionally, we will outline the key features of the isolators and provide information on how to determine the optimal location and parameters for the isolators. This will involve adjusting the isolator parameters and modifying the vertical position of the isolator to ensure that the isolator parameters are optimized as efficiently as possible.

Special materials called isolators are utilized to enhance the structural stability of buildings during earthquakes. These isolators shift the period of the building, separating it from the earthquake's dominant period, and aim to decrease the earthquake's effects by its internal damping. The seismic isolator material utilized in this study was high damping rubber (HDR), known as "KikuchiAikenHDR" which displays a nonlinear hysteresis behavior and was employed in Openseespy for the isolator's horizontal behavior. For the isolator's vertical behavior, an "Elastic" material was used.

The performance of HDR seismic isolators is impacted by the level of shear stress they encounter. In particular, the load history of elastomer bearings affects their mechanical properties. Under low displacements or low shear stresses the stiffness is more or less homogeneous as can be seen in Figure 4.1.a. In the case of high shear stresses in Figure 4.1.b, the stiffness of elastomeric bearings reduces and becomes highly nonlinear (Kikuchi and Aiken 1997). At each cycle of deformation, the energy that is absorbed by the isolator is equivalent to the area under the curve. These graphs were created in Openseespy using the "KikuchiAikenHDR" material.



a) Low shear displacement
 b) Large shear displacement
 Figure 4.1 Shear force – displacement graphs for HDR isolator

As part of our efforts to optimize our building's seismic response, we incorporated "HDR seismic isolators" in various locations throughout our 20-story structure, resulting in 19 distinct models. Each model featured the isolator situated on a different floor, such as the first floor in Model 1, the second floor in Model 2, and so on. To better illustrate these diverse isolator placements, we have included examples. Figure 4.2 displays the isolator on the first floor, while Figure 4.3 showcases it on the third floor. Likewise, Figure 4.4 features the isolator on the eighteenth floor, and Figure 4.5 highlights its placement on the seventeenth floor. In each instance, the isolator was situated on a different level, progressing sequentially from the first floor to the nineteenth floor.

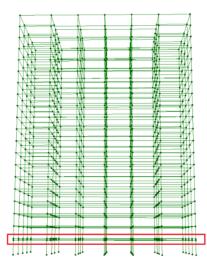


Figure 4.2 Controlled building when isolator is at the 1st floor

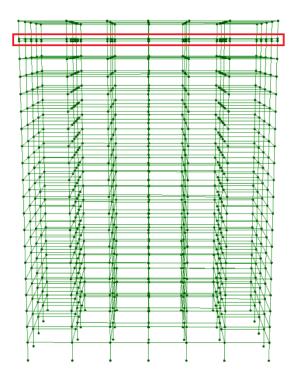


Figure 4.3 Controlled building when isolator at 19th floor

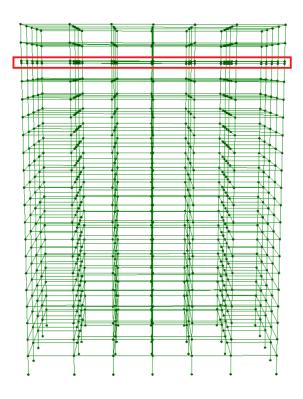


Figure 4.4 Controlled building when isolator at 18th floor

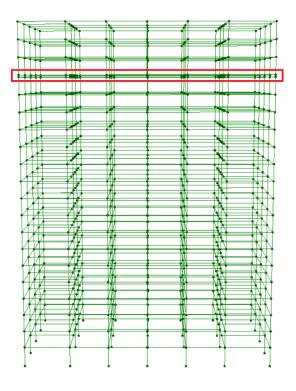


Figure 4.5 Controlled building when isolator at 17th floor

During the optimization of each model, the impact of "EQ12" was considered. The goal was to optimize the isolator parameters. Two distinct methods were employed for isolator optimization. For this purpose, first model (Figure 4.2, Figure 4.3, Figure 4.4, Figure 4.5) taken from the article (Medina and Mathiasson 2014) was used in the same way. The isolator parameters were derived from this optimization by only using "EQ12". Later, the aforementioned earthquakes were applied to each model using these optimized parameters, and the simulation results were documented. In the second model, shear walls were added below the isolator floors to the structural model (Figure 4.6) which taken from the article and tried to determine optimum isolator parameter that would lead to the lowest story drift ratio. These isolator parameters were then employed to conduct a structural analysis using 12 different earthquakes. The results of the analysis, which included story shear forces and drift ratio, were presented in between and Table A2.24.

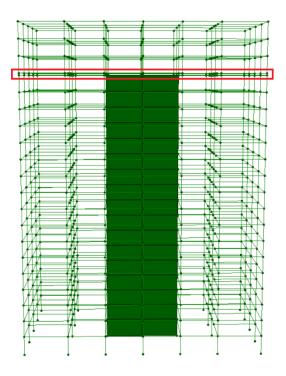


Figure 4.6 Controlled building with shear wall when isolator at 17th floor

4.2 Optimization with First Model

In this section, we have implemented earthquake excitation to the first model with the aim of determining the optimal isolator parameters that would effectively reduce the maximum story drift ratio. The isolator design parameters consist of the elastomer thickness (hr), isolator area (ar), and isolator axial stiffness. The parameters that have been presented in this section were chosen from the Bridgestone catalog, which is cited in section 1.2. Using this catalog is provided to ensure that all results are precise and more accurate for our work.

The objective was to decrease the maximum relative story drift ratio of the building floors (as stated in Equation 4.1), except for the isolator floor. Furthermore, we aimed for the drift ratio of the isolator layer to remain below 200% (as expressed in Equation 4.2), and story drift of the isolator layer remain below isolator radius length

 $(d_{isolator})$ (as expressed in Equation 4.3). With these parameters in mind, our goal was to discover the most efficient and effective values elastomer thickness, isolator area, and isolator axial stiffness.

Minimize
$$\rightarrow f(X) = \left(\frac{\Delta_i}{h_i}\right)_{max}$$
 4.1

Constrains
$$\rightarrow g_1(X) = \left(\frac{\Delta_{isolator}}{h_{isolator}}\right) \le 200\%$$
 4.2

$$g_2(X) = \Delta_{isolator} \le d_{isolator}$$
 4.3

The isolator parameters obtained from this optimization process are detailed in Table 4.1. Upon examining the table, it can be inferred that the optimal isolator parameters for each story are, in fact, not identical. We have observed that the isolator parameters at all levels between stories 13-14 are consistent with one another. Similarly, we have noted that isolator parameters between stories 15-16 are also identical.

Isolator Location	Isolator Model	Product	Cross sectional Area [m ²]	Rubber Height [m]
1	24	HH070X6R	0.3847	0.202
2	9	HH070X4S	0.3847	0.202
3	39	HL070X4S	0.3847	0.167
4	69	HT160X4S	0.6359	0.252
5	27	HH085X6R	0.5671	0.2
6	3	HM080X3R	0.5023	0.1564
7	14	HH095X4S	0.7085	0.198
8	44	HL090X4S	0.7085	0.168
9	30	HH100X6R	0.7849	0.201
10	72	HT100X6R	0.948	0.252
11	85	HS095X4S	0.948	0.222
12	57	HL100X6R	0.948	0.166
13	32	HH120X6R	1.1286	0.2
14	32	HH120X6R	1.1286	0.2
15	46	HL100X4S	0.948	0.166
16	46	HL100X4S	0.948	0.166
17	86	HS100X4S	1.1286	0.24
18	64	HT110X4S	1.1286	0.248
19	16	HH110X4S	0.948	0.2

Table 4.1 Optimized isolator parameters

The following information presents the optimum isolator parameters with maximum story drift ratio and maximum isolator story drift ratio as shown in Table 4.2. Additionally, Table 3.3 indicates that the maximum story drift ratio for an uncontrolled building is 1.00%. According to the data, placing the isolator on the first floor is recommended as it reduces the maximum story drift ratio more significantly than other stories. Conversely, placing the isolator on the 19th floor is not recommended because the maximum story drift ratio is already 1.00% for the uncontrolled building.

alsolator	Isolator	Isolator	Isolator Rubber	Max Story	Max Isolator
Story	Model	Area	Height	Drift Ratio	Drift Ratio
1	24	0.3847	0.202	0.19%	72.21%
2	9	0.3847	0.202	0.20%	65.93%
3	39	0.3847	0.167	0.24%	57.67%
4	69	0.6359	0.252	0.38%	52.11%
5	27	0.5671	0.2	0.49%	49.79%
6	3	0.5023	0.1564	0.65%	48.90%
7	14	0.7085	0.198	0.74%	43.41%
8	44	0.7085	0.168	0.84%	42.84%
9	30	0.7849	0.201	0.84%	49.63%
10	72	0.948	0.252	0.83%	54.85%
11	85	0.948	0.222	0.76%	55.11%
12	57	0.948	0.166	0.72%	48.84%
13	32	1.1286	0.2	0.72%	46.79%
14	32	1.1286	0.2	0.72%	47.99%
15	46	0.948	0.166	0.72%	52.28%
16	46	0.948	0.166	0.69%	54.52%
17	86	1.1286	0.24	0.76%	56.34%
18	64	1.1286	0.248	0.90%	56.13%
19	16	0.948	0.2	1.01%	52.68%

Table 4.2 Optimized isolator parameters with maximum story drift ratios

A set of simulation is undertaken in which the optimum isolator dimensions are used at varying isolation levels under the action of the selected twelve earthquakes. The maximum results are tabulated in APPENDIX 1. Minimum responses are picked from the total responses, and they are presented below. For each earthquake simulation, Table 4.3 presents the minimum drift ratio that occurs due to the optimum isolator placement. By analyzing the data, it is observed that if the isolator is situated on the first floor during EQ7, the maximum story drift ratio in the building will only be 0.14%. This model showcases the least drift ratios when compared to other optimized isolator placements. Further, the optimum isolator floor location is first or second story for each earthquake. Thus, from these outputs it is straight forward to select the isolator floor placement which will be the most beneficial for the building, and optimum isolator location is first 2 story.

	Minimum Drift Ratios							
		Uncontrolled building	Controlled Building	Location Of Isolator	Reduction			
	EQ1	1.16%	0.21%	1	81%			
	EQ2	1.01%	0.23%	4	78%			
	EQ3	2.02%	0.35%	2	83%			
	EQ4	1.18%	0.23%	2	81%			
Data	EQ5	1.60%	0.25%	1	84%			
Earthquake Data	EQ6	1.12%	0.26%	2	77%			
pdu	EQ7	0.80%	0.14%	1	83%			
Eart	EQ8	1.00%	0.16%	2	84%			
	EQ9	0.84%	0.27%	2	68%			
	EQ10	1.37%	0.17%	1	87%			
	EQ11	1.62%	0.19%	1	88%			
	EQ12	1.47%	0.19%	1	87%			
	Min	0.80%	0.14%					
	Max	2.02%	0.35%					

Table 4.3 Summary of drift ratios for all EQ data

In the decision making the maximum floor shear forces may be helpful. In this respect Table 4.4 is presented, in which the maximum floor shear forces are listed. The table shows the maximum floor shear forces of the building with isolators under earthquake loads under the title "Min Story Shear Controlled Building". It corresponds to the smallest of the maximum shear floor force values among all 19 isolator placements. The "isolator location" column reveals the corresponding isolator floor level. According to this table, if the isolator is placed above the first floor, the maximum floor shear force

will be 1140 tf. This value is lower than the floor shear force values of other building models in which the isolator is placed at different floors. In addition, the time history analysis conducted under EQ12 loading of the structure without isolators results in a maximum floor shear force of 6811 tons. Thus, a reduction of 83% has been achieved.

		Story shear	Min story shear	Isolator	
		uncontrolled building	controlled building	location	Reduction
	EQ1	5,308	2,030	1	62%
	EQ2	6,401	1,600	5	75%
	EQ3	8,674	2,067	1	76%
	EQ4	6,970	1,955	1	72%
	EQ5	8,088	1,877	1	77%
Earthquake	EQ6	5,962	1,297	1	78%
Data	EQ7	5,039	1,211	1	76%
	EQ8	6,398	1,185	1	81%
	EQ9	5,230	1,701	2	67%
	EQ10	6,883	1,156	1	83%
	EQ11	6,498	3,572	1	45%
	EQ12	6,811	1,140	1	83%

Table 4.4 Summary of story shear for all EQ data

Between Table A1.1 and Table A1.12 provide detailed information on the story drift ratios of building models, with and without isolators. The drift ratio of the isolator floor can be found in the "isolator floor" row of the table. For models with isolators, the "Isolator level" columns display the maximum drift ratios for each floor during an earthquake. It's worth noting that the drift ratios presented in the table do not occur simultaneously. Additionally, the highest drift ratio is listed in the bottom row and can be cross-checked with Table 4.5 for clarity.

In the event of an earthquake scenario 7, the minimum floor drift ratio of each model occurs when the isolator is placed on the 1st floor, and this drift rate is 0.14% for buildings equipped with isolators. The optimal isolator position is determined by

Equation 4.4, which takes into account the drift ratio. "O.I.L" refers to the optimum isolator location, while Δ_i represents floor displacement and h_i denotes floor height.

$$0.1.L_{1} = \min_{isolator\ levels} \left\{ \left(\frac{\Delta_{i}}{h_{i}} \right)_{\max} \right\}$$

$$4.4$$

Displayed in between Table A1.13 and Table A1.24 are the floor shear forces of structures both with and without isolators. To determine the optimal placement of the isolator, Equation 4.5 is utilized, which takes into account the story shear forces. Within this equation, " F_i " denotes the floor shear force of the respective floor.

$$0.1.L_2 = \min_{isolator\ levels} \{F_{i,\max}\}$$

$$4.5$$

In Table 4.5, you can find a comparison of the periods for the first 5 modes of each structure model with and without isolators. The structure without an isolator has a period of 2.59 seconds for its first mode. However, buildings with isolators have longer periods. The highest period value is 3.60 seconds when the isolator is located on the 1st floor, while the lowest period value among models with isolators is 2.74 seconds when the isolator is placed on the 19th floor. Hence, placing the isolator on the upper floors can bring the period of the structure with isolator closer to that of the structure without isolator.

					PERIODS		
			1	2	3	4	5
		NONISOLATOR BUILDING	2.59	2.32	1.88	0.99	0.87
		1	3.60	3.43	2.43	1.26	1.17
		2	3.56	3.39	2.45	1.23	1.13
		3	3.37	3.18	2.33	1.17	1.07
		4	3.28	3.08	2.25	1.13	1.03
		5	3.18	2.97	2.19	1.10	0.99
RES		6	3.09	2.87	2.19	1.07	0.95
Ē		7	3.01	2.78	2.12	1.04	0.93
STRUCTURES	ISOLATOR LEVEL	8	2.93	2.69	2.07	1.03	0.91
STR	ΓĒ	9	2.93	2.69	2.06	1.03	0.91
Ŧ	OR	10	2.92	2.68	2.06	1.04	0.91
E.	LAT	11	2.86	2.61	2.04	1.05	0.93
0 GE	so	12	2.79	2.53	1.99	1.05	0.93
PERIOD	_	13	2.78	2.51	1.99	1.06	0.94
PER		14	2.77	2.50	1.98	1.06	0.95
_		15	2.76	2.48	1.99	1.06	0.95
		16	2.75	2.47	1.98	1.06	0.95
		17	2.75	2.47	1.98	1.06	0.95
		18	2.75	2.46	1.99	1.06	0.94
		19	2.74	2.46	1.98	1.05	0.92
		MIN PERIOD (sec)	2.59	2.32	1.88	0.99	0.87
		MAX PERIOD (sec)	3.60	3.43	2.45	1.26	1.17

Table 4.5 First 5 periods after optimization for all controlled model

4.3 Optimization with Second Model

In this section, we have integrated earthquake excitation into the second model, which was taken by adding shear walls to the first model. Our objective is to identify the ideal isolator parameters that can efficiently minimize the maximum story drift ratio. The isolator design parameters we have taken into account are the elastomer thickness (hr), isolator area (ar), and isolator axial stiffness. These parameters have been selected from the Bridgestone catalog, same as the first model, as cited in section 1.2. By utilizing this catalog, we are able to aim to get more accurate results for our research.

Our primary goal was to minimize the maximum relative story drift ratio of all building floors, with the exception of the isolator floor. The EQ12 record is utilized during the optimization process to identify optimum isolator parameters. As outlined in Equation 4.1, this was our primary objective. We also strived to ensure that the drift ratio of the isolator layer did not exceed 200% (as noted in Equation 4.2) and that the story drift of the isolator layer remained below the isolator radius length ($d_{isolator}$) (as detailed in Equation 4.3). With these criteria in mind, our main focus was on identifying the most efficient and effective values for the elastomer thickness, isolator area, and isolator axial stiffness.

The section aimed to optimize the isolation parameters for each model which include shear walls. The isolator parameters that were obtained from the optimization process have been presented in Table 4.6. Upon careful examination of the table, it can be inferred that the optimal isolator parameters for each story are not identical. Nevertheless, it has been observed that the isolator parameters for the 1st, 2nd, 5th, and 6th models are consistent with one another. Similarly, the isolator parameters for the 3rd, 4th, and 7th models are also identical. Furthermore, it can be seen that the 10th and 11th models have the same isolators. Similarly, models 14, 15, and 18 share the same isolators, while models 16 and 17 share a common set of isolators.

Isolator Location	Isolator Model	Product	Cross sectional Area [m ²]	Rubber Height [m]	Compressive (x10 ³ kN/m) stiffness
1	9	HH070X4S	0.3847	0.202	2290
2	9	HH070X4S	0.3847	0.202	2290
3	24	HH070X6R	0.3847	0.202	2660
4	24	HH070X6R	0.3847	0.202	2660
5	9	HH070X4S	0.3847	0.202	2290
6	9	HH070X4S	0.3847	0.202	2290
7	24	HH070X6R	0.3847	0.202	2660
8	25	HH075X6R	0.4416	0.2	3090
9	52	HL070X6R	0.4416	0.165	3200
10	26	HH080X6R	0.5023	0.2	3510
11	26	HH080X6R	0.5023	0.2	3510
12	72	HT100X6R	0.948	0.252	4420
13	73	HT110X6R	1.1286	0.248	5240
14	87	HS110X4S	1.3249	0.261	5120
15	87	HS110X4S	1.3249	0.261	5120
16	88	HS120X4S	1.5361	0.279	5650
17	88	HS120X4S	1.5361	0.279	5650
18	87	HS110X4S	1.3249	0.261	5120
19	31	HH110X6R	0.948	0.2	6590

Table 4.6 Optimized isolator parameters

Below, you'll find information on the optimal isolator parameters for maximum story drift ratio and isolator story drift ratio, as presented in Table 4.7. According to Table 3.3, the maximum story drift ratio for an uncontrolled building is 1.47%. Based on this data, it's advised to install the isolator on the fourth floor, as it significantly reduces the maximum story drift ratio compared to other floors. However, it's best to avoid placing the isolator between the 12th and 15th floors, as the maximum story drift ratio is already 1.47% for the uncontrolled building, and maximum drift ratios exceed that of the uncontrolled building.

Isolator	Isolator	Isolator	Isolator Rubber	Max Story	Max Isolator
Story	Model	Area	Height	Drift Ratio	Drift Ratio
1	9	0.3847	0.202	0.256%	87.23%
2	9	0.3847	0.202	0.273%	84.53%
3	24	0.3847	0.202	0.279%	81.22%
4	24	0.3847	0.202	0.263%	74.18%
5	9	0.3847	0.202	0.283%	67.91%
6	9	0.3847	0.202	0.325%	61.37%
7	24	0.3847	0.202	0.370%	59.31%
8	25	0.4416	0.2	0.597%	53.98%
9	52	0.4416	0.165	0.741%	48.45%
10	26	0.5023	0.2	0.797%	49.67%
11	26	0.5023	0.2	0.734%	49.75%
12	72	0.948	0.252	1.593%	50.94%
13	73	1.1286	0.248	2.228%	58.99%
14	87	1.3249	0.261	2.142%	61.05%
15	87	1.3249	0.261	1.543%	64.72%
16	88	1.5361	0.279	1.338%	61.17%
17	88	1.5361	0.279	1.377%	58.35%
18	87	1.3249	0.261	1.283%	58.28%
19	31	0.948	0.2	0.772%	52.26%

Table 4.7 Optimized isolator parameters with maximum story drift ratios

Comprehensive tables (tabulated in APPENDIX 2) illustrates the isolator parameters, story shear, and drift ratio for 12 distinct earthquakes. For each earthquake simulation, Table 4.8 presents the minimum drift ratios that occurs due to the optimum isolator placement. By analyzing the data, it is observed that if the isolator is situated on the fifth floor during EQ8, the maximum story drift ratio in the building will only be 0.17%. This model showcases the least drift ratios when compared to other optimized isolator placements. Further, the optimum isolator floor location varies for each earthquake. Thus, from these outputs it is not straight forward to select the isolator floor placement which will be the most beneficial for the building.

	Minimum Drift Ratios						
		Uncontrolled building	Controlled Building	Location Of Isolator	Reduction		
	EQ1	1.16%	0.27%	4	77%		
	EQ2	1.01%	0.22%	7	78%		
	EQ3	2.02%	0.35%	1	83%		
	EQ4	1.18%	0.26%	6	78%		
Data	EQ5	1.60%	0.32%	2	80%		
Earthquake Data	EQ6	1.12%	0.26%	1	77%		
suph	EQ7	0.80%	0.19%	2	76%		
Eartl	EQ8	1.00%	0.17%	5	83%		
	EQ9	0.84%	0.28%	6	67%		
	EQ10	1.37%	0.21%	5	85%		
	EQ11	1.62%	0.25%	1	85%		
	EQ12	1.47%	0.26%	1	83%		
	Min	0.80%	0.17%				
	Max	2.02%	0.35%				

Table 4.8 Summary of drift ratios for all EQ data

When making decisions, it can be beneficial to take into account the maximum floor shear forces. Table 4.9 offers this data by presenting the highest floor shear forces of a structure with isolators under earthquake loads. The table is labeled "Min Story Shear Controlled Building" and exhibits the minimum maximum shear floor force value among all 19 isolator placements. The "Isolator Location" column indicates the corresponding isolator floor level, which can be determined using equation 4.4. According to this table, if the isolator is placed above the first floor, the maximum floor shear force will be 1417 tf. This value is lower than the floor shear force values of other building models in which the isolator is placed at different floors. In addition, the time history analysis conducted under EQ7 loading of the structure without isolators results in a maximum floor shear force of 5039 tons. Thus, a reduction of 72% has been achieved.

		Story shear	Min story shear	Isolator	
		uncontrolled building	controlled building	location	Reduction
	EQ1	5,308	2,579	1	51%
	EQ2	6,401	1,790	6	72%
	EQ3	8,674	2,560	1	70%
	EQ4	6,970	2,621	1	62%
	EQ5	8,088	2,233	1	72%
Earthquake	EQ6	5,962	1,579	1	74%
Data	EQ7	5,039	1,417	1	72%
	EQ8	6,398	1,583	3	75%
	EQ9	5,230	2,034	1	61%
	EQ10	6,883	1,934	2	72%
	EQ11	6,498	3,531	1	46%
	EQ12	6,811	1,669	1	75%

Table 4.9 Summary of story shears for all EQ datas

Between Table A2.1 and Table A2.12 provide detailed information on the story drift ratios of building models, with and without isolators. The drift ratio of the isolator floor can be found in the "isolator floor" row of the table. For models with isolators, the "Isolator level" columns display the maximum drift ratios for each floor during an earthquake. It's worth noting that the drift ratios presented in the table do not occur simultaneously. Additionally, the highest drift ratio is listed in the bottom row and can be cross-checked with Table 4.8 for clarity.

In the event of an earthquake scenario 8, the minimum floor drift ratio of each model occurs when the isolator is placed on the 5th floor, and this drift rate is 0.17% for buildings equipped with isolators. The optimal isolator position is determined by Equation 4.4, which takes into account the drift ratio. "O.I.L" refers to the optimum isolator location, while Δ_i represents floor displacement and h_i denotes floor height. Table A2.13 and Table A2.24 are the floor shear forces of structures both with and without isolators. To determine the optimal placement of the isolator, Equation 4.5 is utilized, which takes into account the story shear forces. Within this equation, "F_i" denotes the floor shear force of the respective floor.

Table 4.10 displays the periods of the first 5 modes of each structural model with and without an isolator. The fundamental mode of the structure without an isolator has a period of 2.59 seconds, whereas the highest period value is 3.89 seconds when an isolator is placed on the 1st floor. The lowest period of the fundamental mode among models with isolators is 1.59 seconds, which is observed when the isolator is placed on the 19th floor. When the isolator is placed on the mid-floors, the period becomes close to the period of the structure without isolators. This is not helpful to reduce the story drift, because only placing isolator upper floors will making a contribution to the building behaving like have TMD.

					PERIODS		
			1	2	3	4	5
		NONISOLATOR BUILDING	2.59	2.32	1.88	0.99	0.87
		1	3.89	3.73	2.54	1.37	1.28
		2	3.77	3.62	2.48	1.32	1.23
		3	3.64	3.50	2.37	1.27	1.18
		4	3.52	3.40	2.30	1.22	1.13
		5	3.39	3.29	2.27	1.17	1.08
RES		6	3.26	3.18	2.19	1.12	1.03
5		7	3.13	3.06	2.08	1.06	0.98
D D	VEL	8	2.87	2.82	1.93	0.99	0.92
THE STRUCTURES	SOLATOR LEVEL	9	2.60	2.58	1.79	0.91	0.85
뽀	OR	10	2.53	2.52	1.73	0.87	0.81
E E	LAT	11	2.42	2.38	1.65	0.81	0.76
0	so	12	2.12	2.04	1.47	0.73	0.72
IOI	_	13	1.96	1.82	1.35	0.70	0.67
PERIOD OF		14	1.85	1.66	1.26	0.71	0.63
-		15	1.77	1.52	1.19	0.71	0.62
		16	1.70	1.38	1.10	0.70	0.62
		17	1.64	1.25	1.04	0.67	0.61
		18	1.61	1.16	0.99	0.63	0.58
		19	1.59	1.10	0.95	0.55	0.50
		MIN PERIOD (sec)	1.59	1.10	0.95	0.55	0.50
		MAX PERIOD (sec)	3.89	3.73	2.54	1.37	1.28

Table 4.10 First 5 periods for controlled building

CHAPTER 5

IMPROVEMENTS WITH BASE ISOLATION

In this section, we have effected earthquake excitation into the example model which was introduced in section 4.1 by integrating an isolator to the base (Figure 5.1). The primary objective of this endeavor is to determine the optimal isolator parameters, which will effectively reduce the maximum story drift ratio. The isolator design parameters that we have considered consist of the elastomer thickness (hr), isolator area (ar), and isolator axial stiffness. These parameters have been chosen from the Bridgestone catalog, which we have cited in section 1.2.

Our main objective was to reduce the maximum relative story drift ratio of all building floors, except for the isolator floor. This was stated in Equation 4.1. Additionally, we aimed to keep the drift ratio of the isolator layer below 200% (as per Equation 4.2), and to ensure that the story drift of the isolator layer remained below the isolator radius length ($d_{isolator}$) (as per Equation 4.3). To achieve these goals, we set out to determine the most efficient and effective values for the elastomer thickness, isolator area, and isolator axial stiffness.

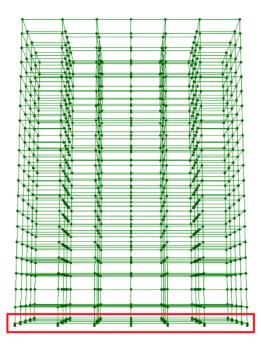


Figure 5.1 Base isolated building

This section aimed to optimize the isolation parameters for the model, which included the base isolator. The isolator parameters obtained from the optimization process have been presented in Table 5.1 and Table 5.2. Based on the results presented in Table 5.2, it can be concluded that the maximum story drift ratio is 0.19% when the isolator is located at the base.

Table 5.1 Optimized isolator parameters

Isolator	Isolator	Product	Cross sectional	Rubber Height	Compressive stiffness
Location	Model		Area [m ²]	[m]	(x10 ³ kN/m)
Base	24	HH070X6R	0.3847	0.202	2660

Table 5.2 Optimized isolator parameters with maximum story drift ratios

Isolator	Isolator	Isolator	Isolator Rubber	Max Story	Max Isolator Drift
Story	Model	Area	Height	Drift Ratio	Ratio
Base	24	0.3847	0.202	0.19%	72.73%

For each earthquake simulation, Table 5.3 presents the minimum drift ratios that occurs due to the optimum isolator parameters. By analyzing the data, it is observed that if the isolator is situated on the fifth floor during EQ8, the minimum story drift ratio in the building will only be 0.14%.

		DRIFT RATIOS		
		UNCONTROLLED	BASE ISOLATION	Reduction
	EQ1	1.16%	0.22%	81%
	EQ2	1.01%	0.24%	76%
	EQ3	2.02%	0.36%	82%
	EQ4	1.18%	0.23%	80%
	EQ5	1.60%	0.25%	85%
	EQ6	1.12%	0.26%	76%
EARTHQUAKE DATAS	EQ7	0.80%	0.14%	82%
EARTHQUARE DATAS	EQ8	1.00%	0.17%	83%
	EQ9	0.84%	0.28%	67%
	EQ10	1.37%	0.17%	87%
	EQ11	1.62%	0.19%	88%
	EQ12	1.47%	0.19%	87%
	Min	0.80%	0.14%	
	Max	2.02%	0.36%	

Table 5.3 Summary of drift ratios for all EQ data

When making decisions, it can be beneficial to take into account the maximum floor shear forces. Table 5.4 offers this data by presenting the highest floor shear forces of a structure with isolators under earthquake loads. According to this table, if the isolator is placed above the base floor, the minimum floor shear force will be 962 tf. In addition, the time history analysis conducted under EQ7 loading of the structure without isolators results in a maximum floor shear force of 5039 tons. Thus, a reduction of 81% has been achieved.

		SHEAR FORCES [t	f]	
		UNCONTROLLED	BASE ISOLATION	Reduction
	EQ1	5,308	1,347	75%
	EQ2	6,401	1,781	72%
	EQ3	8,674	1,918	78%
	EQ4	6,970	1,756	75%
	EQ5	8,088	1,452	82%
	EQ6	5,962	1,223	79%
EARTHQUAKE DATAS	EQ7	5,039	962	81%
LANTIQUARE DATAS	EQ8	6,398	1,167	82%
	EQ9	5,230	1,744	67%
	EQ10	6,883	1,201	83%
	EQ11	6,498	1,126	83%
	EQ12	6,811	1,182	83%
	Min	5,039	962	
	Max	8,674	1,918	

Table 5.4 Summary of story shear forces for all EQ data

The structure is simulated with respect to twelve scaled horizontal earthquake records, and the maximum drift ratios are indicated in Table 5.5. The largest drift ratio occurs due to earthquake 3, the maximum drift ratio due to each earthquake is different, and they are not close to each other. Further, the maximum story shear force is given in Table 5.6. The largest maximum story shear force is 962 tf, while the smallest is 1918 tf.

					DRIFT RATIOS	SOL						
						EQ DATA	TA					
STORY	-	2	ω	4	5	9	L	∞	6	10	11	12
ISOLATOR FLOOR	83.52%	105.62%	110.75%	104.60%	89.52%	75.33%	55.61%	71.65%	103.83%	73.95%	68.34%	72.73%
1	0.13%	0.17%	0.19%	0.16%	0.14%	0.12%	0.09%	0.11%	0.17%	0.11%	0.11%	0.11%
2	0.17%	0.24%	0.27%	0.22%	0.19%	0.17%	0.13%	0.15%	0.24%	0.16%	0.16%	0.15%
æ	0.17%	0.24%	0.29%	0.22%	0.20%	0.18%	0.13%	0.16%	0.25%	0.16%	0.17%	0.15%
4	0.17%	0.24%	0.29%	0.21%	0.20%	0.19%	0.13%	0.16%	0.25%	0.16%	0.17%	0.14%
5	0.17%	0.24%	0.31%	0.22%	0.20%	0.20%	0.14%	0.16%	0.26%	0.17%	0.18%	0.14%
9	0.17%	0.24%	0.32%	0.21%	0.21%	0.20%	0.14%	0.16%	0.27%	0.17%	0.18%	0.15%
7	0.18%	0.24%	0.34%	0.22%	0.22%	0.22%	0.14%	0.17%	0.28%	0.17%	0.19%	0.16%
8	0.18%	0.23%	0.34%	0.22%	0.22%	0.22%	0.14%	0.16%	0.27%	0.17%	0.19%	0.16%
6	0.18%	0.23%	0.34%	0.22%	0.22%	0.22%	0.14%	0.16%	0.27%	0.17%	0.19%	0.16%
10	0.19%	0.22%	0.33%	0.22%	0.22%	0.21%	0.13%	0.16%	0.26%	0.16%	0.19%	0.17%
11	0.20%	0.22%	0.35%	0.23%	0.23%	0.23%	0.13%	0.16%	0.26%	0.17%	0.19%	0.18%
12	0.21%	0.22%	0.35%	0.22%	0.24%	0.24%	0.13%	0.16%	0.26%	0.16%	0.19%	0.18%
13	0.22%	0.23%	0.36%	0.23%	0.25%	0.25%	0.14%	0.16%	0.26%	0.17%	0.19%	0.19%
14	0.22%	0.22%	0.35%	0.23%	0.24%	0.26%	0.14%	0.15%	0.25%	0.16%	0.18%	0.18%
15	0.22%	0.22%	0.34%	0.23%	0.24%	0.26%	0.14%	0.15%	0.24%	0.16%	0.18%	0.19%
16	0.21%	0.20%	0.32%	0.21%	0.22%	0.25%	0.13%	0.14%	0.22%	0.15%	0.17%	0.19%
17	0.20%	0.20%	0.30%	0.21%	0.21%	0.25%	0.13%	0.13%	0.21%	0.14%	0.17%	0.19%
18	0.19%	0.19%	0.29%	0.20%	0.20%	0.24%	0.13%	0.12%	0.19%	0.15%	0.17%	0.19%
19	0.18%	0.17%	0.26%	0.19%	0.18%	0.22%	0.12%	0.11%	0.17%	0.15%	0.16%	0.18%
20	0.17%	0.16%	0.25%	0.18%	0.20%	0.22%	0.12%	0.11%	0.17%	0.16%	0.17%	0.18%
MAX DRIFT RATIO	0.22%	0.24%	0.36%	0.23%	0.25%	0.26%	0.14%	0.17%	0.28%	0.17%	0.19%	0.19%

Table 5.5 Maximum drift ratios for base isolated building for each earthquake data

				STORY	STORY SHEARS [tf]	S [tf]						
						EQ DATA	TA					
STORY	1	2	3	4	5	6	7	8	6	10	11	12
ISOLATOR FLOOR	1,351	1,785	1,906	1,762	1,456	1,223	996	1,171	1,745	1,203	1,126	1,186
1	1,347	1,781	1,902	1,756	1,452	1,223	962	1,167	1,744	1,201	1,125	1,182
0	1,255	1,701	1,900	1,623	1,396	1,209	918	1,108	1,713	1,148	1,126	1,099
3	1,173	1,621	1,912	1,504	1,348	1,202	888	1,064	1,679	1,097	1,124	1,018
4	1,102	1,541	1,918	1,404	1,302	1,199	858	1,024	1,640	1,046	1,111	942
S	1,042	1,460	1,907	1,323	1,259	1,194	827	984	1,595	1,001	1,085	874
6	797	1,380	1,877	1,262	1,223	1,183	794	944	1,544	964	1,051	856
7	996	1,299	1,831	1,212	1,192	1,163	760	902	1,486	925	1,018	842
8	946	1,218	1,774	1,165	1,166	1,132	722	858	1,421	883	066	821
6	933	1,135	1,711	1,115	1,139	1,090	682	811	1,347	838	965	835
10	923	1,050	1,644	1,063	1,110	1,037	639	761	1,265	789	935	838
11	910	986	1,569	1,009	1,076	1,008	596	709	1,175	736	892	820
12	887	930	1,481	951	1,031	994	559	653	1,080	683	833	780
13	851	866	1,379	889	974	968	517	595	LL6	629	756	721
14	799	792	1,261	821	006	925	480	535	870	572	667	660
15	730	708	1,125	745	807	863	436	471	757	509	581	651
16	648	613	973	629	694	LLLLLLLLLLLLLLLLLLLLLLLLLLLLLLLLLLLL	394	404	639	440	528	613
17	551	507	805	560	566	668	353	333	517	392	469	545
18	441	393	626	450	444	535	296	257	410	354	390	448
19	312	270	499	322	379	379	219	177	294	281	285	324
20	172	147	303	180	256	209	125	97	169	169	181	179
MAX STORY SHEAR	1,347	1,781	1,918	1,756	1,452	1,223	962	1,167	1,744	1,201	1,126	1,182

Table 5.6 Story shears for base isolated building for each earthquake data

CHAPTER 6

CONCLUSIONS

The use of base isolators under buildings is widely used in passive control applications, while interstory isolation is still being investigated. The benefits and obligations of this methodology is not well described in the literature. Researchers explore ways to optimize structures by incorporating isolators on intermediate floors. In this particular study, a 20-story building had isolators installed on its intermediate floors resulting in 19 different models, and two different optimization methods were used to determine the optimal isolator dimensions.

In the first and second model, aimed to minimize the maximum drift ratio of all floors except for the isolator floor which involved HDR isolator parameters from the Bridgestone catalog. Afterward, time-history analysis was conducted using the obtained isolator cross-sectional area and elastomer height under 12 earthquake data. The analysis results included story shear, structure periods, and drift ratios.

It is seen that optimizing a building with isolators in interior floor can reduce building drift ratios. While the extent of the reduction depends on the earthquake excitation, it can be concluded that the midfloor isolation is not always minimized the maximum drift ratio. Because of the catalog is not entirely suitable for midstory isolation.

In the optimization of first model, it was found that 12 earthquake ground motions resulted in a maximum drift ratio of 0.35% and a minimum of 0.14%. The maximum story shear force was 3572 tf while the minimum was 1140 tf. Placing isolators on the lower floors proved to be the optimal approach in achieving minimum story shear force but resulted in a longer fundamental period compared to placing isolators on the upper floors. Also, the installation of isolators in mid-floors can have a beneficial effect on reducing both the maximum story drift ratio and the maximum story shear forces.

In the optimization of second model, a study of 12 earthquake data sets found that the maximum drift ratio was 0.35%, while the minimum was 0.17%. Additionally, placing isolators on the first floors can minimize story shear forces. Across all 12 earthquake scenarios, the maximum story shear force was 3531 tonf, and the minimum was 1417 tonf. In conclusion, if optimal results are desired, isolating first eleven floors will achieve the minimum drift ratio. The second model suggests that placing the isolator on the middle and top floors would not be advantageous, unlike the first model. This is because the isolator would not be able to increase the fundamental period enough or relocate it to a region where earthquake acceleration is lower. As a result, the isolator would not be able to serve its intended purpose.

In the optimization of base isolated model, it was found that 12 earthquake ground motions resulted in a maximum drift ratio of 0.36% and a minimum of 0.14%. The maximum story shear force was 1918 tf while the minimum was 962 tf.

When comparing the two models, it was found that the maximum story drift ratios were similar, but the story shear force was significantly lower in the first model. Therefore, if the objective is to achieve minimum story shear force, optimizing the first model is recommended. However, if minimizing drift ratios is the goal, then there is not much difference between the optimization using the first model and the second model.

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																							LOCATION	-
			%																					0.21%
		19	28.78%	0.35%	0.54%	0.58%	0.58%	0.60%	0.60%	0.63%	0.61%	0.60%	0.57%	0.64%	0.70%	0.80%	0.86%	0.91%	0.90%	0.95%	0.92%	0.66%	0.43%	0.95%
		18	29.91%	0.35%	0.54%	0.57%	0.56%	0.58%	0.59%	0.61%	0.60%	0.60%	0.56%	0.59%	0.59%	0.66%	0.70%	0.76%	0.78%	0.78%	0.60%	0.43%	0.56%	0.78%
		17	27.68%	0.34%	0.52%	0.56%	0.55%	0.56%	0.56%	0.58%	0.57%	0.56%	0.55%	0.58%	0.58%	0.60%	0.59%	0.66%	0.63%	0.48%	0.38%	0.43%	0.53%	0.66%
		16	30.38%	0.34%	0.52%	0.56%	0.56%	0.57%	0.56%	0.59%	0.58%	0.57%	0.53%	0.57%	0.58%	0.60%	0.66%	0.67%	0.52%	0.42%	0.48%	0.51%	0.59%	0.67%
		15	38.75%	0.33%	0.50%	0.55%	0.54%	0.55%	0.55%	0.57%	0.56%	0.53%	0.50%	0.54%	0.55%	0.62%	0.63%	0.53%	0.41%	0.49%	0.54%	0.56%	0.63%	0.63%
		14	39.20%	0.32%	0.48%	0.52%	0.52%	0.53%	0.53%	0.54%	0.49%	0.48%	0.49%	0.52%	0.57%	0.61%	0.51%	0.44%	0.49%	0.55%	0.57%	0.56%	0.59%	0.61%
		13	40.12%	0.30%	0.46%	0.50%	0.49%	0.50%	0.48%	0.46%	0.43%	0.43%	0.50%	0.58%	0.57%	0.49%	0.44%	0.52%	0.53%	0.56%	0.56%	0.53%	0.54%	•
		12	43.34%	0.30%	0.45%	0.49%	0.48%	0.47%	0.43%	0.45%	0.46%	0.53%	0.54%	0.54%	0.44%	0.43%	0.52%	0.55%	0.53%	0.54%	0.53%	0.53%	0.58%	•
	EL	11	46.30%	0.31%	0.45%	0.48%	0.45%	0.43%	0.42%	0.47%	0.52%	0.52%	0.47%	0.38%	0.33%	0.45%	0.49%	0.51%	0.51%	0.54%	0.56%	0.55%	0.59%	0.59%
	SOLATOR LEVEL	10	34.22% 4	0.36%	0.52%	0.53%	0.48%	0.48%	0.46%	0.47%	0.43%	0.38%	0.28%	0.28%	0.38%	0.47%	0.52%	0.55%	0.55%	0.60%	0.63%	0.61%		0.64%
	ISOLAT	6	36.09%	0.35%	0.51%	0.52%	0.46%	0.45%	0.44%	0.41%	0.34%	0.26%	0.25%	0.38%	0.47%	0.57%	0.63%	0.68%	0.68%	0.71%	0.73%	0.70%	0.74%	0.74%
s		8	37.10%	0.32%	0.45%	0.45%	0.42%	0.42%	0.41%	0.37%	0.27%	0.25%	0.32%	0.40%	0.46%	0.54%	0.59%	0.63%	0.62%	0.63%	0.64%	0.61%	0.65%	
DRIFT RATIOS		7	39.70%	0.25%	0.35%	0.37%	0.38%	0.39%	0.36%	0.28%	0.23%	0.26%	0.29%	0.35%	0.39%	0.44%	0.48%	0.51%	0.50%	0.52%	0.52%	0.50%	0.53%	
DRIF		9	45.39%	0.25%	0.35%	0.33%	0.31%	0.30%	0.23%	0.20%	0.23%	0.23%	0.24%	0.28%	0.31%	0.35%	0.37%	0.38%	0.37%	0.38%	0.39%	0.39%	0.43%	0.43%
		5	48.25%	0.30%	0.41%	0.36%	0.31%	0.23%	0.18%	0.21%	0.22%	0.22%	0.21%	0.24%	0.27%	0.30%	0.31%	0.31%	0.29%	0.29%	0.34%	0.35%	0.40%	0.41%
		4	51.38%	0.32%	0.42%	0.36%	0.25%	0.18%	0.19%	0.21%	0.22%	0.22%	0.22%	0.23%	0.23%	0.25%	0.26%	0.26%	0.24%	0.22%	0.27%	0.30%	0.35%	0.42%
		3	68.04% 5	0.27%	0.36%	0.27%	0.16%	0.17%	0.18%	0.18%	0.18%	0.18%	0.18%	0.21%	0.22%	0.24%	0.24%	0.23%	0.21%	0.19%	0.19%	0.20%	0.24%	0.36%
		2	7.30% 6	0.20% 0	0.23% 0	0.15% 0	0.16% 0	0.17% 0	0.17% 0	0.19% 0	0.19% 0	0.20% 0	0.20% 0	0.21% 0	0.21% 0	0.22% 0	0.22% 0	0.22% 0	0.20% 0	0.19% 0	0.18% 0	0.17% 0	0.16% 0	0.23% 0
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	21	ED BUILDING	83.	-																				•
	EARTHQUAKE DATA: EQ 1	UNCONTROLLED BUILDING		0.39%	0.57%	0.63%	0.64%	0.66%	0.65%	0.64%	0.63%	0.62%	0.63%	0.72%	0.80%	%06.0	0.95%	0.98%	0.92%	0.95%	1.03%	1.03%	1.16%	0 1.16%
	EARTH	STORY	ISOLATOR FLOOR	1	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	MAX DRIFT RATIO

Table A1.1 Drift ratios after optimization for EQ1 data

Table A1.2 Drift ratios after optimization for EQ2 data

EARTHQUAKE DATA: EQ 2 Ry UNCONTROLLED BUILDING 1	-		2	6	4	5	DRIFI	DRIFT RATIOS	~	ISOLATOR LEVEL 9 10 1	R LEVE	_	12	13	14 15	16	17	81	19		
105.84% 101.25% 79.70% 52.90% 52	101.25% 79.70% 52.90%	101.25% 79.70% 52.90%	6 52.90%		52.53	%	%	%	%	%	%	%	%	%	% 32	31	26	19	13		
0.50% 0.11% 0.13% 0.13% 0.13% 0.12%	0.13% 0.13% 0.13% 0	0.13% 0.13%	0.13%		0.12	%	0.14%	0.14% (0.19% 0.	0.21% 0.	0.23% 0.	0.25% 0.3	0.24% 0.3	0.23% 0.	0.25% 0.27%	7% 0.31%	% 0.34%	6 0.38%	0.42%		
0.79% 0.19% 0.18% 0.19% 0.20% 0.	0.18% 0.19% 0.20% (0.19% 0.20% (0.20% (0).19%	0.22%	0.22% (0.29% 0.	0.32% 0.	0.36% 0.7	0.38% 0.3	0.37% 0.3	0.36% 0.	0.39% 0.42%	2% 0.49%	% 0.55%	6 0.61%	0.66%		
0.89% $0.23%$ $0.20%$ $0.19%$ $0.21%$ 0	0.20% 0.19% 0.21% 0	0.19% 0.21% (0.21% (Ĭ	0	0.22%	0.24%	0.26% (0.31% 0.	0.35% 0.	0.40% 0.4	0.42% 0.4	0.40% 0.4	0.40% 0.4	0.44% 0.47%	⁷⁰ / ₀ 0.55%	% 0.61%	6 0.68%	0.74%		
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0.96% 0.24% 0.23% 0.22% 0.17% 0	0.23% 0.22% 0	0.22% 0		0.17% 0	0	.19%	0.23%	0.28% (0.32% 0.	0.34% 0.	0.40% 0.40%	0.42% 0.4	0.40% 0.4	0.43% 0.4	0.47% 0.50%	0% 0.58%	% 0.65%	6 0.73%	0.79%		
0.97% 0.24% 0.23% 0.23% 0.20% 0	0.23% 0.23% 0.20% 0	0.23% 0.20% (0.20%	Ĭ	0	0.18%	0.20%	0.27% (0.32% 0.	0.32% 0.	0.39% 0.	0.41% 0.4	0.40% 0.4	0.44% 0.4	0.48% 0.51%	% 0.59%	% 0.66%	6 0.73%	0.80%		
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0.99% 0.22% 0.22% 0.23% 0.22% 0.2	0.22% 0.23% 0.22% (0.23% 0.22% (0.22% (Č	0).25%	0.26%	0.27% (0.32% 0.	0.32% 0.	0.32% 0.	0.36% 0.4	0.46% 0.3	0.50% 0.3	0.55% 0.55%	5% 0.63%	% 0.68%	6 0.75%	0.81%		
0.96% 0.22% 0.21% 0.22% 0.22% 0	0.21% 0.22% 0.22% 0	0.22% 0.22% (0.22%	Ū	-	0.25%	0.26%	0.27% (0.32% 0.	0.33% 0.	0.35% 0.	0.34% 0.4	0.40% 0.4	0.49% 0.	0.56% 0.57%	7% 0.63%	% 0.68%	6 0.74%	0.80%		
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0.95% 0.22% 0.21% 0.23% 0.33% 0.	0.21% 0.22% 0.23% 0	0.22% 0.23% (0.23%	Ĩ	o.	0.27%	0.28%	0.29% (0.32% 0.	0.34% 0.	0.37% 0.	0.40% 0.4	0.46% 0.4	0.43% 0.4	0.49% 0.59%	% 0.64%	% 0.71%	6 0.75%	0.82%		
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0.84% 0.20% 0.19% 0.20% 0.21% 0	0.19% 0.20% 0.21% 0	0.20% 0.21% (0.21%	Ĩ	•	0.25%	0.27%	0.27% (0.29% 0.	0.32% 0.	0.35% 0.7	0.37% 0.4	0.43% 0.4	0.46% 0.4	0.47% 0.42%	2% 0.49%	% 0.62%	% 0.70%	0.77%		
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0.75% $0.19%$ $0.17%$ $0.19%$ $0.20%$ 0	0.17% 0.19% 0.20%	0.19% 0.20%	0.20%	-	-	0.24%	0.26%	0.25% (0.26% 0.	0.30% 0.	0.33% 0.	0.35% 0.3	0.39% 0.4	0.43% 0.4	0.45% 0.45%	5% 0.48%	% 0.41%	6 0.55%	0.71%		
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0.84%	0.27% 0.26% 0.26% 0.26% 0.26%	0.26% 0.26% 0.25% 0.25% 0.25% 0.24% 0.24% 0.23% 0.19% 0.19% 0.17% 0.17%	0.31% 0.31% 0.29% 0.29% 0.29% 0.25% 0.25% 0.25% 0.25% 0.22% 0.22%	0.29% 0.27% 0.27% 0.27% 0.27% 0.24% 0.24% 0.24% 0.24%	0.34% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.35% 0.35% 0.35% 0.35% 0.35% 0.35%	0.39% 0.40% 0.40% 0.38% 0.38% 0.38% 0.33% 0.33% 0.33% 0.33% 0.33%	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \textbf{333}^{3,6} \\ \textbf{323}^{3,6} \\ \textbf{323}^{3,6} \\ \textbf{323}^{3,6} \\ \textbf{333}^{3,6} \\ \textbf{333}^{3,6} \\ \textbf{354}^{3,6} \\ \textbf{357}^{3,6} \\ \textbf{357}^{3,6} \\ \textbf{0.57}^{3,6} \\ \textbf{0.42}^{3,6} \\ \textbf{0.42}^{3,6} \\ \textbf{0.57}^{3,6} \\ \textbf{0.57}^{3,6} \end{array}$	$\begin{array}{c} 0.41\% \\ 0.33\% \\ 0.33\% \\ 0.44\% \\ 0.58\% \\ 0.61\% \\ 0.57\% \\ 0.57\% \\ 0.57\% \\ 0.47\% \\ 0.62\% \\ 0.62\% \\ \end{array}$	0.47% 0.42% 0.32% 0.32% 0.51% 0.55% 0.55% 0.55% 0.48% 0.48%			$\begin{array}{c} 0.56\%\\ 0.58\%\\ 0.58\%\\ 0.58\%\\ 0.58\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.59\%\\ 0.59\%\\ \end{array}$	$\begin{array}{c} 0.58\%\\ 0.61\%\\ 0.66\%\\ 0.66\%\\ 0.61\%\\ 0.64\%\\ 0.64\%\\ 0.64\%\\ 0.44\%\\ 0.49\%\\ 0.49\%\\ 0.51\%\\ 0.46\%\\ 0.66\%\\ \end{array}$	$\begin{array}{c} 0.59\%\\ 0.61\%\\ 0.61\%\\ 0.69\%\\ 0.70\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.45\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.42\%\\ 0.12\%\end{array}$	$\begin{array}{c} 0.64\%\\ 0.65\%\\ 0.65\%\\ 0.72\%\\ 0.74\%\\ 0.79\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.74\%\\ 0.74\%\\ 0.74\%\\ 0.74\%\\ 0.74\%\\ 0.79\%\\ 0.46\%\\ 0.96\%\\ 0.79\%\\ \end{array}$	$\begin{array}{c} 0.69\%\\ 0.69\%\\ 0.69\%\\ 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.67\%\\ 0.40\%\\ 0.48\%\\ 0.48\%\\ 0.49\%\\ 0.49\%\\ \end{array}$	$\begin{array}{c} 0.76\%\\ 0.76\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.80\%$			CATION 2
0.82%	0.27% 0.26% 0.26% 0.26%	0.26% 0.25% 0.25% 0.25% 0.24% 0.24% 0.24% 0.22% 0.19% 0.17% 0.17%	031% 029% 029% 029% 022% 025% 025% 025% 022% 032%	0.27% 0.27% 0.27% 0.27% 0.25% 0.24% 0.24% 0.23% 0.30% '	0.33% 0.22% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.35% 0.25%	0.40% 0.39% 0.38% 0.38% 0.38% 0.38% 0.33% 0.33% 0.33% 0.33%	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} $	$\begin{array}{c} 0.33\% \\ 0.34\% \\ 0.34\% \\ 0.51\% \\ 0.51\% \\ 0.61\% \\ 1.005\% \\ 0.57\% \\ 0.47\% \\ 0.47\% \\ 0.47\% \\ 0.62\% \\ \end{array}$	0.42% 0.32% 0.32% 0.54% 0.54% 0.55% 0.55% 0.55% 0.48% 0.48%			$\begin{array}{c} 0.58\%\\ 0.58\%\\ 0.59\%\\ 0.46\%\\ 0.46\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.54\%\\ 0.59\%\\ 0.59\%\\ \end{array}$	$\begin{array}{c} 0.61\%\\ 0.62\%\\ 0.66\%\\ 0.66\%\\ 0.64\%\\ 0.64\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.66\%\\ \end{array}$	$\begin{array}{c} 0.61\%\\ 0.63\%\\ 0.69\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.72\%\\ 0.72\%\\ 0.72\%\\ 0.40\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.72\%\\ \end{array}$	$\begin{array}{c} 0.65\%\\ 0.66\%\\ 0.72\%\\ 0.72\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.47\%\\ 0.42\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.79\%\\ \end{array}$	0.69% 0.74% 0.74% 0.77% 0.77% 0.77% 0.77% 0.77% 0.77% 0.77% 0.77% 0.77% 0.79%	$\begin{array}{c} 0.76\%\\ 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.80\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.70\%\\ 0.40\%\\ 0.60\%\\ 0.80\%$			CATION 2
	$\begin{array}{c} 0.26\%\\ 0.26\%\\ 0.26\%\\ 0.26\%\end{array}$	0.25% 0.25% 0.24% 0.24% 0.23% 0.23% 0.20% 0.19% 0.17% 0.17% 0.17%	0.29% 0.30% 0.29% 0.28% 0.28% 0.25% 0.25% 0.22% 0.22%	0.27% 0.27% 0.27% 0.27% 0.24% 0.24% 0.34%	0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.32% 0.26% 0.25% 0.25%	0.39% 0.49% 0.38% 0.38% 0.33% 0.33% 0.33% 0.33% 0.33%	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3.36\% \\ 3.44\% \\ 1.44\% \\ 1.54\% \\ 1.57\% \\ 1.57\% \\ 1.57\% \\ 1.57\% \\ 1.57\% \\ 1.47\% \\ 1.47\% \\ 1.47\% \\ 1.42\% \\$	$\begin{array}{c} 0.34\% \\ 0.44\% \\ 0.51\% \\ 10.58\% \\ 1.62\% \\ 1.62\% \\ 1.57\% \\ 1.7\% \\ 1.7\% \\ 1.47\% \\ 0.47\% \\ 1.62\% \\ 1.47\% \\ 1.47\% \\ 1.62\% \\ 1.62\% \\ 1.62\% \\ 1.6\% \\ $	0.32% 0.36% 0.51% 0.51% 0.55% 0.55% 0.48% 0.48% 0.48% 0.57%			$\begin{array}{c} 0.58\%\\ 0.58\%\\ 0.46\%\\ 0.46\%\\ 0.54\%\\ 0.54\%\\ 0.55\%\\ 0.55\%\\ 0.59\%\\ 0.59\%\\ \end{array}$	$\begin{array}{c} 0.62\%\\ 0.66\%\\ 0.66\%\\ 0.61\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.49\%\\ 0.46\%\\ 0.66\%\\ \end{array}$	$\begin{array}{c} 0.63\%\\ 0.69\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.49\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.72\%\\ \end{array}$	$\begin{array}{c} 0.66\%\\ 0.72\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.72\%\\ 0.77\%\\ 0.79\%\\ 0.79\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.79\%\\ \end{array}$	0.69% 0.74% 0.77% 0.77% 0.77% 0.67% 0.67% 0.67% 0.67% 0.40% 0.40% 0.48% 0.48%	$\begin{array}{c} 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.80\%\\ 0.70\%\\ 0.70\%\\ 0.70\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.80\%\\ 0.80\%\\ \end{array}$			CATION 2
	0.26% 0.26% 0.26%	0.25% 0.24% 0.24% 0.23% 0.20% 0.19% 0.19% 0.17% 0.17%	0.30% 0.29% 0.29% 0.29% 0.25% 0.25% 0.22% 0.22%	0.27% 0.26% 0.27% 0.27% 0.24% 0.24% 0.23% 0.23%	0.32% 0.32% 0.32% 0.32% 0.30% 0.30% 0.28% 0.28% 0.25% 0.35%	0.40% 0.38% 0.38% 0.35% 0.35% 0.33% 0.31% 0.31%	$\begin{array}{c} 0.42\% \\ 0.42\% \\ 0.45\% \\ 0.45\% \\ 0.39\% \\ 0.39\% \\ 0.39\% \\ 0.37\% \\ 0.37\% \\ 0.37\% \\ 0.52\% \\ 1 \end{array}$	$\begin{array}{c} 0.44\% \\ \hline 0.44\% \\ \hline 0.54\% \\ \hline 0.57\% \\ \hline 0.57\% \\ \hline 0.57\% \\ \hline 0.42\% \\ \hline 0.42\% \\ \hline 0.42\% \\ \hline \end{array}$	0.44% 0.044% 0.051% 0.051% 0.051% 0.051% 0.051% 0.051% 0.051% 0.051% 0.051% 0.057% 0.057% 0.047% 0.047% 0.047% 0.052% 0.047% 0.052% 0.047%	0.36% 0.14% 0.0.51% 0.0.51% 0.0.51% 0.0.51% 0.0.51% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.48% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55% 0.0.55\% 0.0.5\%\% 0.0.55\% 0.0.5\%\%\% 0.0.5\%\%\% 0.0.5\%\%\% 0.0.5\%\%\%			$\begin{array}{c} 0.59\%\\ 0.54\%\\ 0.45\%\\ 0.54\%\\ 0.54\%\\ 0.55\%\\ 0.55\%\\ 0.59\%\\ 0.59\%\end{array}$	$\begin{array}{c} 0.66\%\\ 0.64\%\\ 0.61\%\\ 0.44\%\\ 0.44\%\\ 0.44\%\\ 0.44\%\\ 0.44\%\\ 0.21\%\\ 0.50\%\\ 0.66\%\\ \end{array}$	$\begin{array}{c} 0.69\%\\ 0.70\%\\ 0.77\%\\ 0.67\%\\ 0.64\%\\ 0.45\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.42\%\\ 0.72\%\\ \end{array}$	$\begin{array}{c} 0.72\%\\ 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.72\%\\ 0.47\%\\ 0.47\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.79\%\\ \end{array}$	$\begin{array}{c} 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.77\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.46\%\\ 0.48\%\\ 0.48\%\\ 0.79\%\\ \end{array}$	$\begin{array}{c} 0.77\%\\ 0.77\%\\ 0.80\%\\ 0.78\%\\ 0.76\%\\ 0.76\%\\ 0.76\%\\ 0.76\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.60\%\\ 0.80\%$			CATION 2
0.77%	0.26%	0.24% 0.24% 0.23% 0.20% 0.19% 0.17% 0.17% 0.17% 0.27%	0.29% 0.29% 0.28% 0.25% 0.25% 0.25% 0.22% 0.22%	0.26% 0.27% 0.27% 0.25% 0.25% 0.24% 0.22% 0.23% 0.23%	0.31% 0.32% 0.32% 0.32% 0.32% 0.25% 0.25% 0.25% 0.25% 0.25%	038% 036% 035% 032% 033% 031% 045%	$\begin{array}{c} 0.43\% \\ 0.45\% \\ 0.45\% \\ 0.45\% \\ 0.39\% \\ 0.39\% \\ 0.39\% \\ 0.37\% \\ 0.39\% \\ 0.37\% \\ 0.39\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.52\% \\ 1.0.5\% \\ 1.$).48% ().54% ().57% ().57% ().53% (0.42% (0.42% (0.42% ().57% (0.51% 0 0.51% 0 0.61% 1 0.61% 1 0.57% 1 0.57% 0 0.47% 0 0.47% 0 0.47% 0 0.62% 1	0.44% 0.51% 0.51% 0.51% 0.51% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.55% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57% 0.57\% 0.55\% 0.5\%\% 0.55\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\% 0.5\%\%			0.54% 0.46% 0.45% 0.54% 0.55% 0.55% 0.59%	$\begin{array}{c} 0.64\%\\ 0.61\%\\ 0.41\%\\ 0.49\%\\ 0.44\%\\ 0.44\%\\ 0.49\%\\ 0.51\%\\ 0.46\%\\ \hline 0.66\%\\ \end{array}$	0.70% 0.72% 0.67% 0.44% 0.45% 0.45% 0.45% 0.42% 0.42%	$\begin{array}{c} 0.74\%\\ 0.77\%\\ 0.77\%\\ 0.54\%\\ 0.42\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.46\%\\ 0.079\%\\ \end{array}$	$\begin{array}{c} 0.76\%\\ 0.77\%\\ 0.77\%\\ 0.67\%\\ 0.67\%\\ 0.67\%\\ 0.40\%\\ 0.48\%\\ 0.48\%\\ 0.79\%\\ \end{array}$	0.77% 0.80% 0.78% 0.76% 0.70% 0.67% 0.67% 0.67% 0.50% 0.80%			2 2
	0.26%	0.24% 0.23% 0.22% 0.19% 0.19% 0.17% 0.17% 0.17%	0.29% 0.28% 0.25% 0.25% 0.25% 0.22% 0.32%	0.27% 0.27% 0.25% 0.24% 0.24% 0.22% 0.33%	0.32% 0.32% 0.32% 0.29% 0.28% 0.25% 0.35%	0.38% 0.36% 0.32% 0.33% 0.31% 0.31%	$\begin{array}{c} 0.46\% & 0 \\ 0.45\% & 0 \\ 0.45\% & 0 \\ 0.39\% & 0 \\ 0.39\% & 0 \\ 0.37\% & 0 \\ 0.37\% & 0 \\ 0.32\% & 1 \\ 0.52\% & 1 \\ \end{array}$).54% ().57% ().57% ().53% ().53% ().53% ().47% ().42% ().42% ().42% ().57% (0.58% 0.61% 0.61% 0.61% 0.62% 0.55% 0.55% 0.55% 0.55% 0.47% 0.47% 0.47% 0.62% 0.62%	0.51% 0.54% 0.55% 0.55% 0.55% 0.53% 0.48% 0.48% 0.57%			0.46% 0.45% 0.54% 0.55% 0.55% 0.55% 0.50% 0.50%	$\begin{array}{c} 0.61\%\\ 0.49\%\\ 0.49\%\\ 0.44\%\\ 0.51\%\\ 0.51\%\\ 0.46\%\\ 0.46\%\\ \end{array}$	$\begin{array}{c} 0.72\%\\ 0.67\%\\ 0.64\%\\ 0.40\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.42\%\\ 0.72\%\\ \end{array}$	0.79% 0.77% 0.54% 0.42% 0.47% 0.46% 0.46% 0.46%	0.79% 0.77% 0.75% 0.67% 0.67% 0.67% 0.48% 0.48% 0.48%	0.80% 0.78% 0.76% 0.67% 0.67% 0.80% 0.80%			2
		0.23% 0.22% 0.19% 0.19% 0.17% 0.17% 0.17%	0.28% 0.27% 0.25% 0.25% 0.22% 0.322%	0.27% 0.25% 0.24% 0.24% 0.22% 0.30% 0.33%	0.32% 0.32% 0.29% 0.28% 0.25% 0.35%	0.36% 0.32% 0.33% 0.33% 0.31% 0.45%	$\begin{array}{c} 0.45\% \\ 0.45\% \\ 0.39\% \\ 0.39\% \\ 0.40\% \\ 0.39\% \\ 0.37\% \\ 0.37\% \\ 0.52\% \\ 1 \end{array}$).57% ().57% ().53% ().53% ().53% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().57% ().53% ().5	0.61% 0.62% 0.59% 0.57% 0.53% 0.47% 0.47%	0.54% 0.55% 0.55% 0.55% 0.48% 0.48%			0.45% 0.54% 0.55% 0.55% 0.49% 0.49% 0.59%	0.49% 0.41% 0.51% 0.51% 0.46% 0.46%	$\begin{array}{c} 0.67\%\\ 0.54\%\\ 0.40\%\\ 0.45\%\\ 0.45\%\\ 0.45\%\\ 0.42\%\\ 0.42\%\\ \end{array}$	0.77% 0.54% 0.42% 0.42% 0.46% 0.46% 0.46%	0.77% 0.75% 0.67% 0.52% 0.40% 0.48% 0.48% 0.48%	0.78% 0.76% 0.67% 0.67% 0.40% 0.80%			CATION 2
	0.25%	0.22% 0.20% 0.19% 0.17% 0.17% 0.17%	0.27% 0.25% 0.25% 0.22% 0.22% 0.32%	0.23% 0.24% 0.24% 0.22% 0.23% 0.30%)n for	<u>0.32%</u> 0.30% 0.29% 0.25% 0.35% EQ1	0.35% 0.33% 0.33% 0.31% 0.31%	$\begin{array}{c} \hline 0.44\% & 0\\ \hline 0.39\% & (0\\ 0.40\% & (0\\ 0.39\% & (0\\ 0.37\% & (0\\ 0.37\% & (0\\ 0.52\% & (0\\ 0.52\% & (0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0\\ 0$	<u>).57%</u> <u>().53%</u> <u>().53%</u> <u>().53%</u> <u>().57%</u> <u>().57%</u>	0.62% 0.57% 0.57% 0.57% 0.47% 0.47%	0.57% 0.55% 0.53% 0.48% 0.48% 0.57%			0.54% 0.55% 0.55% 0.54% 0.49% 0.59%	$\begin{array}{c} 0.44\%\\ 0.49\%\\ 0.51\%\\ 0.50\%\\ 0.46\%\\ 0.46\%\\ 0.66\%\end{array}$	0.54% 0.40% 0.45% 0.45% 0.42% 0.72%	0.72% 0.54% 0.42% 0.47% 0.46% 0.46% 0.46%	0.75% 0.67% 0.52% 0.40% 0.48% 0.48% 0.79%	0.76% 0.67% 0.67% 0.53% 0.40% 0.50% 0.80%			CATION 2
15 0.73%	0.24%	0.20% 0.19% 0.17% 0.17% 0.17%	0.25% 0.25% 0.22% 0.22% 0.32%	0.25% 0.24% 0.24% 0.23% 0.30% 0.30% 0.30%	0.30% 0.29% 0.26% 0.25% 0.35% 1.35%	0.32% 0.33% 0.31% 0.31% 0.31%	0.39% 0 0.40% (0.39% (0.37% (0.37% (0.52% 7).53% (0.50% (0.42% (0.42% (0.57% (0.59% 0.57% 0.53% 0.47% 0.47% 0.62%	0.55% 0.55% 0.55% 0.48% 0.48% 0.57%			0.54% 0.55% 0.54% 0.49% 0.50% 0.59%	0.49% 0.51% 0.50% 0.46% 0.46% 0.66%	0.40% 0.45% 0.45% 0.42% 0.72%	0.54% 0.42% 0.47% 0.46% 0.46% 0.79%	0.67% 0.52% 0.40% 0.48% 0.48%	0.70% 0.67% 0.53% 0.40% 0.50%			2
	0.22%	0.19% 0.17% 0.17% 0.17% 0.27%	0.25% 0.24% 0.22% 0.32%	0.24% 0.24% 0.23% 0.30% 0.30% 0.30%	0.29% 0.26% 0.25% 0.35% EQ1	0.33% 0.33% 0.31% 0.45%	0.40% 0.39% 0.39% 0.39% 0.39% 0.39% 0.52% 0.52% 0.52% 0.52%).50% (0.42% (0.57% (0.57% 0.53% 0.47% 0.47% 0.62%	0.55% 0.55% 0.48% 0.48% 0.57%			0.55% 0.54% 0.50% 0.50%	0.51% 0.50% 0.46% 0.66%	0.45% 0.42% 0.42% 0.72%	0.42% 0.47% 0.46% 0.46% 0.79%	0.52% 0.40% 0.45% 0.48% 0.79%	0.67% 0.53% 0.40% 0.50%			CATION 2
17 0 69%	0.21%	0.19% 0.17% 0.17% 0.27%	0.22% 0.22% 0.32%	0.22% 0.22% 0.30% ' 0.30% for	0.28% 0.26% 0.35% r EQ1	0.33% 0.31% 0.31% 0.45%	0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39% (0.39\% (0.33\% (0.39\% (0.33\%)(0.33\% (0.33\%)(0.3	0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57% (0.57\%)(0.57\% (0.57\%))))))))))))))))))))))))))))))))))))	0.63%	0.53%			0.54% 0.49% 0.50% 0.59%	0.50% 0.46% 0.46% 0.66%	0.45% 0.42% 0.72%	0.47% 0.46% 0.46% 0.79%	0.40% 0.45% 0.48% 0.79%	0.53%			2
	0 1002	0.17% 0.17% 0.27%	0.22%	0.22% 0.23% / 0.30% /	0.25% 10.25\% 10.	0.31%	0.52%	0.57% (0.57% (0.57% (0.47% 0.47% 0.62%	0.48%			0.49% 0.50% 0.59%	0.46%	0.42% 0.42% 0.72%	0.46%	0.45% 0.48% 0.79%	0.50%			2
	0/120	0.17% 0.27% 0.27%	0.32%	0.23% 0.30% /	0.25% 0.35% r EQ1	0.31%	0.32% (0.42% (0.57% (0.57% (0.47%	0.57%			0.59% 0.59%	0.46% 0.46% 0.66%	0.42% 0.72%	0.46% 0.46% 0.79%	0.43%	0.40% 0.50% 0.80%			2 2
19 0.04%	0.11%	0.17% 0.27%	0.22%	<u>0.33%</u>	0.25% r 0.35% r EQ1	0.31%	0.39% ().42% (<u>).57% (</u>	0.47%	0.57%		0.56%	0.59%	0.46% 0.66%	0.42% 0.72%	0.46%	0.48%	0.50%			2 2
		0.27%	0.32%	n for	0.35% EQ1	0.45%	0.52% ().57% (0.62%	0.57%		0.56%	0.59%	0.66%	0.72%	0.79%	0.79%	0.80%		27%	2
MAX DRIFT RATIO 0.84%	0.28%			n for	EQ1																
EARTHOUAKE DATA: EO 10	Γ					DRIF	DRIFT RATIOS		TSOLAT	ISOLATOR LEVEL	Tell.										
STORY UNCONTROLLED BUILDING	-	6	6	4	5	9	6	×	6	10	=	6	1	14	2	91	17	81	19		
aloo	%0C5 EL	70 58%	%9L 09	×4 00%	%1 Y 20%	%	%	8 05% 4	48 05% 40 58% 46 80% 43 67%	46 80% 4		37 70°/	44 07%	2	55	Ý	24 00%	%	30 38%		
0 54%	%LU 0		0.24%	%0C U	0/20.10		0.21% 0	0.21%	0.28%	- %^LC 0		0.34%	0 32%			0.31%	0 38%		0/0C./C		
0.85%	0.13%		030%	0.40%	%LE 0	%92.0						0.53%	0 50%	0.52%	0.51%	0 50%	0.60%	0.69%	0.75%		
%96 O	0.15%		0.19%	0.33%	0.37%	0.37%		0.39% (0.58%	0.54%	0.57%	0.57%	0.56%	0.68%	0.78%	0.84%		
0.98%	0.16%		0.17%	0.20%	0.30%	0.33%	I	I	I	I		0.56%	0.53%	0.57%	0.58%	0.58%	0.70%	0.80%	0.87%		
1.03%	0.16%		0.19%	0.20%	0.20%	0.27%						0.55%	0.55%	0.58%	0.58%	0.60%	0.73%	0.84%	0.91%		
1.04%	0.17%		0.20%	0.22%	0.20%	0.23%						0.55%	0.56%	0.58%	0.57%	0.61%	0.74%	0.85%	0.92%		
1.09%	0.17%		0.20%	0.23%	0.23%	0.23%	L	0.38% (L			0.61%	0.61%	0.61%	0.59%	0.63%	0.77%	0.89%	0.96%		
1.08%	0.17%		0.20%	0.22%	0.23%	0.26%						0.62%	0.62%	0.62%	0.59%	0.65%	0.75%	0.88%	0.95%		
1.06%	0.17%		0.19%	0.21%	0.22%	0.26%						0.62%	0.62%	0.62%	0.60%	0.67%	0.74%	0.86%	0.94%		
10 1.03%	0.16%	0.16%	0.19%	0.21%	0.22%	0.26%	I 1	I .	0.26%	0.33% (0.57%	0.61%	0.60%	0.57%	0.67%	0.72%	0.84%	0.91%		
	0.17%		0.20%	0.22%	0.22%	0.27%					0.41%	0.54%	0.60%		0.58%	0.69%	0.77%	0.86%	0.94%		
	0.16%		0.20%	0.21%	0.22%	0.27%						0.44%	0.56%		0.63%	0.67%	0.79%	0.86%	0.93%		
	0.17%		0.20%	0.22%	0.22%	0.28%						0.40%	0.50%			0.70%	0.83%	0.93%	1.03%		
14 1.29%	0.16%	0.16%	0.20%	0.22%	0.22%	0.27%	0.31% 0			0.43%		0.45%	0.44%		0.65%	0.72%	0.85%	0.95%	1.07%		
15 1.37%	0.16%	0.15%	0.20%	0.21%	0.21%	0.26%	0.34% 0			0.49%	0.43%	0.48%	0.52%	0.48%	0.53%	0.73%	0.89%	0.99%	1.10%		
	0.15%	0.14%	0.19%	0.19%	0.20%	0.24%	0.34% 0					0.46%	0.52%	0.53%	0.49%	0.58%	0.83%	0.99%	1.08%		
17 1.30%	0.14%		0.18%	0.19%	0.20%	0.26%						0.46%	0.54%		0.54%		0.66%	1.00%	1.16%		
18 1.28%	0.15%		0.17%	0.19%	0.22%	0.27%					0.54%	0.49%	0.54%		0.53%		0.60%	0.80%	1.15%		
19 1.22%	0.15%	0.12%	0.16%	0.20%		0.27%			0.60%				0.51%		0.53%	0.71%	0.72%	0.60%	0.85%		
1 75%	0 16%	0 14%	015%	0.25%	0 24%			0 53% (0.61%	0.68%		0.58%	0.51%	0 60%	0 59%	0 75%	0.81%	0.74%	0.62%	10	LOCATION
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1 62%	•		•	n for			0.56% 0	50% 0.			9% 0.68%		0.67% 0.75%	5% 0.81%	% 0.94%	% 0 92%	% 0.95%	•	0 19%	-
						DRIFT	DRIFT RATIOS		1021 10											
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0.97%				0.20%									2% 0.58%							
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1.03%				0.20%	0.18%															
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1.07%			0.18%	0.21%																
1.05%			0.18%	0.21%	0.23%		- 1	- 1	- 1											
1.02%			0.18%	0.22%																
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1.03%			0.22%				- 1	- 1	- 1	- 1	- 1	- 1	- 1	- 1	- 1	- 1				
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1.03%			0.23%								0.60% 0.6									
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1.26%	0.19%		0.22%																	
1.38%	0.19%	0.19%	0.23%	0.38%	0.47%	0.57%		0.82% 0.8	0.82% 0.7	0.73% 0.6	0.67% 0.70	0.70% 0.70%		0% 0.63%		% 0.53%				
1.42%	0.19%	0.18%	0.22%	0.37%	0.49%	0.57%	0.71% 0.	- 1	0.84% 0.7	0.77% 0.6	0.68% 0.69%	9% 0.69%	- 1	0% 0.65%		% 0.45%	% 0.61%			
1.38%	0.18%	0.17%	0.20%	0.35%		0.54%		0.79% 0.81%		0.77% 0.66%				5% 0.62%	%09 ^{.0} %	% 0.56%	% 0.55%			
1.47%	0.18%	0.17%	0.22%	0.36%	0.47%		0.70% 0.	0.82% 0.8	84% 0.8	0.83% 0.7	5% 0.7.	72% 0.71%	1% 0.69%	9% 0.66	% 0.67	% 0.65%	% 0.73%	0.59%		LOCATION
	•	•	70700	•			0 7/% 0	0 84% 0 84%	0.40/ 0.0	0 839/ 0 769/	70/1 0 7/0/	•	•	70/2020 7/06	-/0 V 0 200/	7020 70	2 0 00%	1 01%	0.10%	

FORM SHEARING 2 STORY SHEARING STORY SHEARING STORY SHEARING STORY SHEARING STORY SHEARING STORY SHEARING STORY SHEARING STORY STORY SHEARING STORY STORY SHEARING STORY STORY SHEARING IDEATOR SLATE SECTION LEVEL STORY STORY STORY SHEARING IDEATOR SLATE SECTION STORY SHEARING IDEATOR STORY STORY SHEARING IDEATOR STORY STORY STORY STORY SHEARING IDEATOR STORY
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STORY SHEARIT 3 4 5 6 7 8 1586 1,41 1578 1,400 1,234 1,244 1,655 1,622 1,588 1,876 1,734 2,734 1,645 1,652 1,588 1,876 1,734 2,740 1,645 1,653 1,641 1,738 2,490 2,740 1,608 1,634 1,733 1,873 1,771 2,400 1,608 1,634 1,733 1,876 1,773 2,400 1,608 1,634 1,733 1,876 1,774 2,013 1,608 1,634 1,733 1,876 1,774 2,013 1,614 1,744 2,011 1,744 2,011 1,744 2,011 1,525 1,406 1,521 1,845 2,003 1,931 1,744 2,011 1,525 1,406 1,521 1,521 1,744 2,011 1,744 2,011
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STORY SHEARIG 33 4 5 6 7 136 14 1378 1420 1638 1665 1652 1588 1,270 1638 1666 1668 1,538 1,570 1,793 1666 1,668 1,566 1,733 1,841 1666 1,648 1,566 1,733 1,841 1666 1,648 1,566 1,573 1,841 1648 1,543 1,566 1,573 1,843 1548 1,538 1,771 1,845 1,546 1,544 1548 1,256 1,527 1,524 1,546 1,544 1,258 1,118 1,227 1,246 1,546 1,546 1,258 1,118 1,229 1,246 1,512 1,541 1,060 1,087 1,179 1,246 1,512 1,541
3 4 5 6 1586 1,341 1,378 1,4 1,646 1,632 1,544 1,378 1,4 1,646 1,632 1,544 1,378 1,4 1,626 1,543 1,546 1,37 1,37 1,626 1,548 1,364 1,37 1,346 1,37 1,938 1,436 1,538 1,406 1,63 1,41 1,338 1,406 1,63 1,41 1,338 1,406 1,63 1,237
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EARTHQUAKE DATA: EQ 3 STORY LINCONTROLLED							STOR	STORY SHEAR[tr]	F													
	3 DATA: EQ 3									ISOLATOR LEVEL	R LEVEL											
	UNCONTROLLED BUILDING	-	2		4	5	9	7	8	6	10		12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,930	1,886	2,139	1,925	2,348	2,804	2,635	2,672	2,282	2,314 2		2,612	2,430	2,091 2	2,160	2,152 2		2,262	2,072		
1	8,674	2,067	2,965	3,772	4,900	6,757	7,874	8,712	7,622	8,988	-		5,278						5,829	6,569		
2	8,652	1,906	2,318	3,409	3,929	6,158	7,205	8,254	7,188	8,883		7,281	5,507			4,424		5,236	5,658	6,471		
3	8,639	1,913	1,903	2.573	3,435	5,104	6,123	7,642	6,746	8,574	-		5,702			4,222		- ,	5,459	6,313		
4	8,552	1,921	1,935	2,178	2,624	3,639	4,680	6,644	6,407	8,022	7,888 7				3,900	3,869	4,131 4		5,258	6,080		
5	8,311	1,915	1,946	2,202	1,959	2,454	3,092	5,156	5,905	7,212	7,415 6	6,813	5,686			3,506	3,947	4,773	5,118	5,853		
9	7,863	1,888	1,930	2,199	2,042	2,442	2,401	3,247	5,093	6,192	-					3,703			5,038	5,621		
7	7,180	1,845	1,889	2,172	2,132	2,520	2,796	2,447	3,944	5,056	5,720 5	5,497			4,095 3	3,844	3,950 4		4,930	5,377		
8	6,293	1,788	1,826	2,123	2,178	2,553	2,779	2,306	2,651	3,777			4,392			Ĵ		4,328 4	4,808	5,189		
6	5,834	1,723	1,746	2,048	2,167	2,527	2,703	2,101	2,416	2,356									4,821	5,072		
10	5,467	1,654	1,656	1,946	2,098	2,435	2,544	2,130	2,451	2,575		2,363		3,533	3,575 2	3,592	3,879 4	4,345	4,783	4,939		
11	5,176	1,576	1,556	1,824	1,980	2,277	2,311	2,239	2,686	3,057		-							4,590	4,630		
12	5,135	1,489	1,448	1,688	1,825	2,059	2,023	2,410	3,068	3,606	3,122 2	2,534	2,344						4,222	4,086		
13	5,126	1,386	1,329	1,538	1,643	1,802	1,747	2,619	3,528	4,132						2,686	3,294	3,748	3,821	3,737		
14	5,491	1,267	1,203	1,375	1,440	1,529	1,940	2,786	3,906	4,502	3,768 2		2,292		2,517	2,458	3,089	.,	3,549	3,521		
15	5,843	1,130	1,063	1,195	1,225	1,445	2,052	2,844	4,085	4,637	3,866 2	2,788 2	2,234	1,947		2,083	2,736 2	2,871	3,496	3,586		
16	5,886	776	912	1,007	1,096	1,390	2,019	2,739	3,995	4,477			2,213	1,873		1,819	2,138		3,374	3,571		
17	5,591	808	748	862	945	1,232	1,832	2,465	3,633	4,036			2,102	1,806	1,776	1,780	1,890	1,884	2,923	3,307		
18	4,917	631	658	747	935	1,106	1,519	2,046	3,032	3,344	2,962 2	2,151	1,863	1,676	1,697	1,628	1,852	1,786	2,238	2,772		
19	3,778	504	516	591	<i>L6L</i>	886	1,120	1,495	2,213	2,418		1,648	1,453	1,385	1,390	1,396		1,505	1,560	2,062	Į	
20	2,193	306	302	367	499	534	650	843	1,237	1,328				881					912			LOCATION
MAX STORY SHEAR	8,674	2,067	2,965	3,772	4,900	6,757	7,874	8,712	7,622	8,988	8,297 7	7,293	5,770	4,894	4,831 4	4,472	5,134 5	5,369	5,829	6,569	2,067	-

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Table A

																							LOCATION	-
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		19	1,624	5,773	5,706	5,617	5,506	5,371	5,214	5,034	4,831	4,605	4,354	4,083	3,793	3,483	3,159	3,049	3,034	2,817	2,380	1,806	846	5,773
		18	1,887	5,382	5,312	5,223	5,112	4,979	4,827	4,653	4,458	4,242	4,006	3,753	3,488	3,207	3,122	3,097	2,873	2,412	1,872	1,302	701	5,382
		17	2,048	4,881	4,808	4,717	4,607	4,476	4,328	4,163	3,984	3,792	3,589	3,378	3,301	3,262	3,205	2,942	2,443	1,898	1,593	1,113	601	4,881
		16	2,189	4,751	4,542	4,348	4,160	3,986	3,885	3,816	3,753	3,676	3,586	3,491	3,421	3,301	2,982	2,456	1,967	1,849	1,483	1,056	609	4,751
		15	2,303	4,900	4,700	4,523	4,345	4,170	4,068	3,998	3,925	3,835	3,744	3,649	3,453	3,063	2,509	2,020	2,034	1,743	1,423	1,134	699	4,900
		14	2,430	1,999	4,790	4,605	4,427	4,261	4,183	4,119	4,052	3,974	3,835	3,566	3,144	2,579	2,117	2,221	2,000	1,742	1,433	1,049	650	1,999
		13	2,540	5,207	2,000	118,4	1,628	1,465	1,395	1,309	f,193	1,017	3,723	3,286	2,715	2,180	2,387	2,227	2,041	1,807	1,505	1,112	628	5,207
		12	619	5,176	5,030	. 916,1	1,805	· 669't	1,569	1,426	1,228	3,904	3,439	2,840	2,259	2,509	2,348	2,170	. 996,1	1,723	414	1,015	617	5,176
		-	,586	,109	984	737 7	,838	1,720 4	,596	404	1 1/0/1	909	2,960	2,199	2,446	2,305	2,146	. 096	,748	,496	308	,025	809	,109
	LEVEL	10	,596 2	279 5	,194	,108 4	,969	,836 4	1,618 4	1,278 4	3,785 4	E 660'	2,263 2	2,487 2	2,385 2	2,264 2	2,116 2	,943	,852 1	,766]	,558]	,200	969	,279 5
	ISOLATOR LEVEL		2,771 2	513 5	5,387 5	5,196 5	,984 4	774 4	,447 4	3,931 4	3,214 3	2,343 3	2,655 2	2,566 2	2,476 2	2,365 2	2,233 2	2,071 1	997 1	,867 1	,599 1	,195 1	683	5,513 5
	SI	9	,912 2	5,451 5,	5,215 5,	,980 5	,757 4	,433 4,	3,924 4	3,213 3,	2,348 3,	2,763 2.	2,646 2	2,552 2,	2,467 2	2,378 2,	2,275 2,	2,143 2,	,964 1	1 617,	,506 1	,170 1	687	5,451 5,
STORY SHEAR[tf]		8	,520 2,	6,135 5,	,850 5,	4,613 4,	1,285 4,	3,767 4,	,042 3,	2,174 3,	2,380 2,	2,260 2,	2,151 2,	2,052 2,	,967 2,	,892 2,	,818 2,	,730 2,	603 1,	,416 1,	159 1,	922 1,		,135 5,
STORY S		7	2,283 2,	4,594 5,	4,310 4,	3,964 4,	3,407 4,	2,657 3,	,901 3,	2,163 2,	2,063 2,	,956 2,	,847 2,	1,742 2,	1,647 1,	,566 1,	1,498 1,	,436 1,	1,355 1,	,232 1,	,045 1,	783	490	,594 5,
		9			1														995 1,	904 1,7	787 1,	656	405	,069 4,
		5	1,843	4,069	3,849	3,475		1,945	1,780	1,717	1,650	1,569		1,372	1,291	1,189	1,123	1,061						4
		4	1,734	3,761	3,542	2,996	2,279	1,614	1,529	1,461	1,394	1,329	1,253	1,174	1,100	1,032	67	906	829	743	625	462	261	3,761
		3	1,764	2,910	2,560	2,104	1,641	1,532	1,434	1,344	1,268	1,210	1,158	1,097	1,020	939	866	796	713	611	490	348	196	2,910
		2	1,694	2,248	1,869	1,567	1,459	1,370	1,299	1,239	1,182	1,124	1,065	1,004	942	878	812	739	657	563	454	327	184	2,248
		-	1,771	1,955	1,637	1,509	1,405	1,321	1,258	1,207	1,159	1,109	1,057	1,001	943	881	814	738	653	557	447	320	179	1,955
	ATA: EQ 4	UNCONTROLLED BUILDING		6,970	6,882	6,768	6,628	6,463	6,272	6,051	5,800	5,521	5,212	4,874	4,511	4,117	3,702	3,612	3,436	3,183	2,826	2,222	1,320	6,970
	EARTHQUAKE DATA: EQ 4	STORY UNCC	ISOLATOR FLOOR	1	2	3	4	5	6	7	8	9	10	п	12	13	14	15	16	17	18	19	20	MAX STORY SHEAR

STORY STORY <th< th=""><th></th><th>2</th><th></th><th></th><th></th><th></th><th>STORY SHEAR[tf]</th><th></th><th>IUal</th><th>IANA I GOLF IOS</th><th>-</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<>		2					STORY SHEAR[tf]		IUal	IANA I GOLF IOS	-										
	7 8 - 9 0 - 6 9 9 9 9 4 - 8 0 9 0 8		6	4	5	9	7	~	9 0	10 10		12	13	14	15	16	17	81	10		
1 3 2 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	■ .										2,294	3,039	3,302	3,313	3,197	3,080	2,756	2,603	2,069		
2 4 5 6 9 9 11 11 11 11 11 11 11 11 11 11 11 11											7,340	6,943	6,178	5,536	5,764	5,571	5,461	6,162	6,212		
4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		1,453 2,1 1 397 1 4	2,146 5,0								6,852	6,788	6,307	5,533	5,710	5,328	5,216 4 901	6,057 5 897	6,124		
5 7 8 8 9 8 10 11 11 13 13 13 13 13 13 13 13 13 13 13						Ι.					5,398	5,686	5,785	5,703	5,352	4,870	4,927	5,785	5,980		
7 8 8 9 9 11 12 12 13 14 14 15 16 15 16 15 15 15 16 15 16 16 16 16 16 16 16 16 16 16 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18		1,292 1,3	1,387 1,6	1,695 1,	1,796 2,4	2,473 3,186	_	4,537 5,636	36 5,200	4,807	4,857	5,063	5,156	5,360	5,421	5,048	4,948 4 700	5,738	5,890		
8 9 10 11 13 13 14 13 16 18 18 18 20 20 20 20 20 8112AR											4,02/	4,020	4,604	4,1/8	4.729	5.083	4,789	5.234	5.727		
9 10 11 13 13 13 16 16 17 18 20 20 20 20 20 20 20 20 20 20 20 20 20									╝		4,261	4,246	4,551	4,395	4,199	4,713	4,982	4,846	5,662		
11 12 13 13 14 16 16 16 19 20 20 20 20 20 20 20 20 20 20 20 20 20											4,134	4,435	4,273	4,325	4,154	4,292	4,724	4,896	5,284		
12 13 14 16 16 16 19 19 19 20 20 20 20 20 20 20 20 20 20 20 20 20											3,402	4,310	4,351	4,254	4,158	4,029	4,434	4,736	4,804		
13 14 15 16 17 18 19 20 20 20 20			1,118 1,3								2,203	2,337	3,587	4,154	4,302	3,617	4,001	4,474	4,879		
14 15 16 18 20 20 20 20 20											2,261	2,838	2,495	3,563	4,015	3,862	3,823	4,309	4,883		
10 16 18 19 20 20 20 20 20											2,257	2,650	2,777	2,563	3,478	3,999	4,047	4,121	4,681		
17 18 19 20 20 20 20											1 943	2.032	1 912	2,116	2.607	2,803	3 797	4 305	4315		
18 19 20 S STORY SHEAR											1,661	1,593	1,718	2,169	2,190	2,536	2,914	3,929	4,394		
19 20 ¢ STORY SHEAR											1,436	1,202	1,591	2,105	2,059	2,148	2,311	3,045	3,978		
20 (STORY SHEAR											1,145	971	1,212	1,680	1,774	1,683	1,798	1,757	2,963		
			292 4								711	631	7997	1,021	1,118	1,019	1,082	956	1,096	1 077	LOCATION
							STORY SHEAR[tf]	IEAR [tf]	IOSI	IANA I GOLY IOS											
STORY UNCONTROLLED BUILDING	IDING	2	3	4	5	9		~	9 6	10	11	12	13	14	15	16	17	18	19		
JOOR		Ι.	1,195 1,4								2,169	2,393	2,379	2,347	2,287	2,200	2,164	2,044	1,605		
											3,733	4,211	4,360	4,145	3,779	3,869	3,986	4,781	5,494		
3 2		1,203 1,1	27 577 511 51 51	_							3,659	4,149	4,384	4,105	3,610 3,610	3,084 3,513	3,901 3,912	4,608	5,348 5,348		
4	[[Ι.					3,541	4,023	4,243	4,002	3,537	3,449	3,838	4,419	5,200		
5											3,361	3,836	4,063 3,815	3,833	3,452	3,371	3,738	4,169 4.048	4,993		
6	[2,833	3,305	3,514	3,353	3,170	3,282	3,466	3,902	4,605		
∞ (_								2,634	2,984	3,181	3,084	3,163	3,229	3,300	3,754	4,487		
10											1.809	2,643	2,559	2,805	3,110	3.047	3,118	3,650	4,32/		
II											1,951	2,145	2,264	2,533	2,789	2,884	2,884	3,434	4,021		
12											2,028	2,277	2,258	2,305	2,514	2,664	2,892	3,442	3,996		
13											1, 241	2,219	2,329	2,325	2,297	2,411	2,871	3,414	3,923		
15											1,635	1,792	1,903	2,077	2,177	2,193	2,460	3,078	3,585		
16											1,487	1,523	1,631	1,805	1,944	2,102	2,085	2,740	3,291		
1/											1 151	1,362	1 222	1 258	1,748	1,803	1.945	1 979	2,403		
19											168	988	980	1,006	1,153	1,158	1,163	1,389	1,862	Į	
20	1,337	212 2	201 201	209	335 4	409 4	456 4	415 506	06 527	645	528	588	591	600	676 2 770 °	776	713	729	876	1 107	LOCATION

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																								1,211
		19	1,126	4,644	4,521	4,380	4,266	4,216	4,181	4,090	3,936	3,751	3,526	3,237	3,095	3,082	2,985	2,765	2,519	2,245	1.856	1.381	640	4,644
		18	1,539	4,169	4,049	4,005	4,032	4,062	4,049	3,966	3,799	3,555	3,285	3,245	3,192	3,153	3,012	2,770	2,413	1,983	1.550	1,058	564	4,169
		17	1,900	3,859	3,860	3,915	3,954	3,934	3,825	3,635	3,446	3,315	3,318	3,300	3,286	3,161	2,909	2,540	2,099	1,877	1,472	1,026	557	3,954
		16	2,166	3,926	3,955	3.973	3,914	3,755	3,512	3,284	3,308	3,305	3,299	3,294	3,176	2,929	2,569	2,334	2.157	1,832	1,481	1,065	596	3,973
		15	2,289	3,966	3,919	3,806	3,607	3,336	3,117	3,178	3,159	3,225	3,187	3,039	2,859	2,862	2,674	2.354	2,044	1,772	1,446	1,041	580	3,966
		14	2,345	3,804	3,674	3,505	3,341	3,203	3,022	3,058	3,112	3,061	2,918	2,963	2,978	2,850	2,640	2,155	1,977	1,747	1,455	1,073	610	3,804
		13	2,403	3,522	3,460	3,405	3,339	3,214	3,012	2,908	2,904	2,804	2,949	2,966	2,845	2.622	2,217	2,035	1,859	1,643	1,372	1,020	586	3,522
		12	2,310	3,343	3,274	3,256	3,176	3,026	2,924	2,824	2,646	2,637	2,667	2,573	2,415	2,197	2,074	1,934	1,771	1,561	1,294	950	541	3,343
		11	1,875	3,192	3,130	3,110	3,069	2,908	2,811	2,699	2,562	2,397	2,198	1,975	1,822	1,758	1,668	1,536	1,402	1,287	1,090	799	458	3,192
	RLEVEL	10	1,990	3,183	3,116	3,011	2,921	2,890	2,794	2,648	2,435	2,158	2.026	1,897	1,813	1,749	1,684	1,586	1,436	1,306	1,081	770	415	3,183
	ISOLATOR LEVEL	6	2,044	3,137	2,957	2,968	2,929	2,806	2,623	2,377	2,042	1,959	1,952	1,863	1,786	1,718	1,654	1,577	1,459	1,280	1,041	740	407	3,137
HEAR[tf]		8	2,102	3,201	3,174	3,034	2,915	2,747	2,415	1,947	1.837	1,918	1,783	1,686	1,621	1,581	1,545	1,491	1,404	1,268	1,072	798	453	3,201
STORY SHEAR[tf]		7	1,872	3,163	3,095	3,119	3,003	2,686	2,208	1,888	1,817	1,740	1,643	1,528	1,386	1,210	1,114	1,071	1,008	916	780	664	422	3,163
		9	1,545	3,161	3,052	2,673	2,226	2,063	1.683	1,477	1,411	1,344	1,271	1,187	1,086	1,000	940	875	944	940	841	647	388	3,161
		5	1,444	2,993	2,730	2,225	1,853	1.593	1,375	1,309	1,249	1,192	1,135	1,076	1,044	1,015	893	752	853	862	770	583	377	2,993
			,342	,794	.586	.220	1,720	,256	.200	,169	,129	.077	,024	976	912	838	763	689	639	612	623	545	350	,794
		4	1,015 1	2,726 2	2,354 2	.615 2		962 1					795 1									355	221	2,726 2,
		3	918 1,	2,067 2,	.415 2.	888 1.	862		795		726			637			522			353	281	218	132	2,067 2,
		2	959 9	.211 2,0		880 8	850 8		788 7		717 717						490 5				292 2		123 1	,211 2,0
		1 10	6	-																				
	EARTHQUAKE DATA: EQ 7	CONTROLLED BUILDI	~	5,039	5,005	4,943	4,792	4,532	4,252	4,016	3,981	3,856	3,827	3,744	3,529	3,16	2,789	2,47(2,186	1,937	1,757	1,417	869	.R 5,039
	EARTHQU	STORY	ISOLATOR FLOOR	1	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	MAX STORY SHEAR

Table A1.19 Story shears after optimization for EQ7 data

Table A1.20 Story shears after optimization for EQ8 data

							STOR	STORY SHEAR[tf]	_												
EARTHQU	EARTHQUAKE DATA: EQ 8									ISOLATOR LEVEL	LEVEL										
STORY	UNCONTROLLED BUILDING	1	7		4	5	9	7	8	9 1	10 11	1 12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,167	1,121	1,114	1,289	1,267	1,252	1,404	1,535 1	1,465 1	1,522 1,	,648 2,	2,237 2,2	2,270 2,1	53 1,965	5 1,764	1,614	1,387	1,079		
1	6,398	1.185	1,192	1,700	1,755	1,569	1,751	2,227	2,064 2	2,148 2	2,497 2,	2,950 3,	,277 3,2	,204 2,978	78 3,13.	8 3,383	\$ 4,012	4,740	5,347		
7	6,311	1,107	1,155	1,522	1,740	1,488	1,663	2,071	1,987 2	2,013 2	2,431 2,	2,888 3,	,224 3,1	3,156 2,9	2,930 3,112	2 3,377	3,964	4,660	5,261		
3	6,228	1.063	1.060	1.157	1.588	1.452	1.647	1.848	1.896 1	1.914 2	2.326 2.	2.800 3.	3.137 3.0	3.068 2.8	.860 3.064	4 3,348	3.920	4,556	5.177		
4	6,117	1,021	1,003	1,040	1.321	1,392	1,563	1,535	1,785 1	1,874 2	2,168 2.	2,684 3,		2,929 2,844	44 2,988	8 3,309	3,858	4,429	5,083		
5	5,970	982	961	980	1,223	1,306	1,400	1,450	1,786 1	1,825 1	1,976 2,	2,547 2,	2,875 2,7	2,765 2,8	2,807 2,904	4 3,275	3,785	4,330	4,959		
9	5,788	942	920	945	1.163	1.219	1.231	1.402	1.735 1	1.770 1	1.902 2.	2,411 2,	2.723 2.6	2,618 2.7	2.727 2.891	1 3.241	3.706	4,225	4,814		
7	5,569	901	877	606	1,110	1,173	1,200	1,395	1,636 1	1,705 1	1,909 2.	2,314 2,		2,491 2,6	2,609 2,843	3 3,195	5 3,613	4,107	4,656		
8	5,314	857	834	874	1,077	1,126	1,147	1,332	1.563 1	1,629 1	1,858 2,	2,224 2,	2,458 2,3	2,341 2,461	61 2,759	9 3,127	3,497	3,981	4,486		
6	5.028	810	792	838	1.058	1.085	1.089	1.262	1.425 1	1.543 1	1.738 2.	2.097 2.	2.322 2.2	2.257 2.2	2.289 2.638	8 3.030	3.359	3,840	4,303		
10	4,724	760	746	799	1,024	1,053	1,027	1,195	1,346 1	1,373 1	1,567 1.			2,206 2,250	50 2,486	6 2,899	3,201	3,690	4,110		
11	4,410	708	696	754	975	1,007	985	1,132	1,270 1	1,329 1	1,441 1.	1,703 2,		2,271 2,246	46 2,315	5 2,735	3,028	3,526	3,900		
12	4,084	653	643	703	912	949	936	1.055	1.188 1	1.276 1	1.369 1.	1.483 2.	2.172 2.3	2.301 2.261	61 2.189	9 2,545	5 2.843	3.319	3.658		
13	3,746	595	589	647	836	881	878	959	1,103 1	1,208 1	1,287 1,	1,329 2,	2,014 2,2	2,294 2,254	54 2,164	4 2,335	5 2,636	3,064	3,373		
14	3,396	535	533	586	763	803	814	848	1,012 1	1,123 1	1,190 1,	1,181 1,	1,807 2,0	2,032 2.2	2,215 2,124	4 2,146	5 2,411	2,773	3,054		
15	3,013	471	471	519	721	724	746	749	909 1	1.021 1	1.077 1.	.042 1.	.616 1.8	.803 1.8	.897 2.057	7 2,021	2.167	2,483	2,696		
16	2,595	404	405	446	654	683	672	642	798	904			1,436 1,5	1,578 1,6	,641 1,698	8 1.898	1.980	2,182	2,423		
17	2,141	333	333	365	562	631	586	526	676	768	800	774 1.	1,237 1,3	1,329 1,3	.366 1,411	1 1,451	1.796	1,918	2,120		
18	1,665	258	258	281	451	543	483	466	542	611	634	635	997 1,0	.047 1.0	,067 1,103	3 1,143	3 1,230	1,641	1,793		
19	1,155	177	177	197	329	409	374	357	401	430	445	464	704	726 7	736 765	5 804	1 830	938	1.437		
20	637	76	100	127	190	235	220	208	227					397 3	397 416			489	624		LOCATION
MAX STORY SHEAR	6 398	1 185	1 100	1 700	1 755	1 560	1 751	2 222 5		2 140 7	2 107	020		Ì	010 2120	0 2 202	1012			1 105	-

							STOR	STORY SHEAR[tr]	-													
KE DA	EARTHQUAKE DATA: EQ 9									ISOLATOR LEVEL	R LEVEL											
UNC	UNCONTROLLED BUILDING	-	2	æ	4	5	9	7	8	6	10	=	12	13	14	15	16	17	18	19		
		1,758	1,751	2,063	1,947	2,036	2,235	2,069	2,234	2,012	2,084	2,349	2,359	2,198	2,034	1,937	1,695	1,587	1,340	1,071		
	5,134	1,646	1,572	1,899	2,266	2,980	3,742	4,185	3,861	4,127	4,017	3,749	3,464	3,300	3,329	3,697	3,698	3,964	4,415	4,648		
	5,198	1,725	1,672	1,822	2,144	2,833	3,587	4,031	3,641	3,930	3,870	3,628	3,303	3,112	3,202	3,609	3,698	4,043	4,494	4,741		
	5,230	1,689	1,701	1,900	2,072	2,595	3,303	3,768	3,373	3,688	3,708	3,484	3,118	3,015	3,084	3,480	3,696	4,098	4,528	4,787		
	5,203	1,648	1,644	1,990	1,962	2,400	2,881	3,388	3,106	3,458	3,539	3,308	2,908	2,911	2,998	3,311	3,651	4,107	4,516	4,777		
	5,111	1,602	1,581	1,916	1,853	2,211	2,333	2,917	2,816	3,248	3,356	3,101	2,680	2,806	3,019	3,161	3,585	4,066	4,476	4,725		
	4,955	1,549	1,515	1,836	1,759	1,926	2,099	2,441	2,563	3,016	3,148	2,869	2,669	2,834	3,033	3,184	3,536	3,978	4,409	4,640		
	4,748	1,490	1,444	1,749	1,659	1,881	2,214	2,062	2,278	2,733	2,911	2,615	2,831	2,982	3,067	3,203	3,511	3,868	4,312	4,527		
	4,504	1,424	1,369	1,655	1,553	1,821	2,176	2,015	2,196	2,401	2,635	2,348	2,883	3,103	3,150	3,204	3,484	3,749	4,179	4,388		
	4,230	1,349	1,288	1,552	1,442	1,733	2,104	1,942	1,965	2,060	2,313	2,342	2,812	3,132	3,229	3,221	3,440	3,633	4,013	4,219		
	3,930	1,267	1,201	1,442	1,331	1,615	1,991	1,909	1,860	1,959	1,950	2,270	2,616	3,041	3,227	3,252	3,404	3,526	3,816	4,026		
	3,612	1,177	1,108	1,326	1,215	1,473	1,839	1,912	1,998	2,093	1,872	2,148	2,480	2,828	3,115	3,240	3,381	3,459	3,620	3,800		
	3,298	1,081	1,012	1,208	1,125	1,320	1,657	1,884	2,128	2,245	1,980	2,122	2,323	2,493	2,883	3,136	3,326	3,382	3,439	3,518		
	3,014	978	910	1,088	1,057	1,251	1,458	1,801	2,182	2,326	2,041	1,953	2,203	2,228	2,534	2,929	3,190	3,199	3,213	3,185		
	2,759	871	807	967	979	1,162	1,280	1,657	2,132	2,298	2,033	1,844	2,084	2,090	2,097	2,590	2,943	2,906	2,921	2,844		
	2,499	757	701	865	879	1,055	1,130	1,454	1,969	2,154	1,949	1,752	1,961	1,962	1,859	2,136	2,561	2,577	2,589	2,524		
	2,221	639	592	776	761	929	1,025	1,252	1,709	1,904	1,785	1,633	1,800	1,788	1,666	1,599	2,060	2,261	2,263	2,283		
	1,925	516	522	664	629	785	917	1,103	1,390	1,576	1,541	1,457	1,581	1,558	1,434	1,293	1,436	1,839	1,992	2,136		
	1,606	417	426	533	561	624	766	906	1,071	1,215	1,233	1,209	1,294	1,269	1,159	1,011	1,187	1,246	1,611	1,847		
	1,245	301	305	385	417	444	567	668	761	890	870	118	931	911	827	718	875	006	919	1,365		
	742	172	173	217	236	251	322	383	432	513	481	484	514	504	457	418	492	527	562	588		LOCATION
	5.230	1.725	1.701	1.990	2.266	2.980	3.742	4.185	3.861	4.127	4.017	3.749	3.464	3 300	3.329	3.697	3.698	4.107	4.528	4.787 1.	.701	2

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Table A1.22 Story shears after optimization for EQ10 data

ULINGE DATA: EQ 10 1107 112 1197 1155 136 1197 1155 136 1197 1155 136 137 135 136 137 135 136 137 135 136 137 135 136 136 137 135 136 136 136 136 136 136 136 136 136 136								STOR	STORY SHEAR[tf]	F													
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	RTHQUAKE DATA: EQ 10	_									ISOLATO	R LEVEL											
	UNCONTROLLEL	D BUILDING	-	2	3	4	5	9	7	8	6			12 1	13 1/	14 15	5 16	5 17	18		19		
	OOR		1,197	1,155	1,364	1,512	1,542	1,580	1,620	1,824	1,829	1	1	,093 2	,475 2,	,684 2,	2,732 2,	2,719 2,5	2,504 2,3	2,334 1	,918		
		6,883	1,156	1,951	3,566	4,007	3,567	3,198	2,647	2,892	3,834	3,747 4	1,098 4	1,432 4	,127 4,	,341 4,	,136 4,	,024 4,8	,855 5,5	569 6	6,023		
		6,819	1,142	1,208	2,772	3,567	3,194	3,028	2,824	2,706	3,670	4	1,021 4	1,391 4	,131 4	,281 4,	,163 4,	,011 4,8	,835 5,5	5,537 5	5,980		
		6,726	1,091	1,112	1,481	2,638	2,806	2,816	2,906	2,851	3,579		4	(,199 3	955 4	1,136 4,	098 3,	966 4,7	781 5,4	5,474 5	5,909		
		6,602	1,041	1,068	1,305	1,619	2,175	2,399	2,787	2,987	3,377	_		,906 3	664 3	,935 3,	,947 3,	,916 4,6	,693 5,3	5,377 5	5,807		
		6,443	966	1,023	1,242	1,430	1,500	1,848	2,390	2,900	3,122			3,611 3	3,508 3,	,712 3,	,739 3,	,824 4,5	571 5,2	5,248 5	5,672		
		6,252	962	976	1,177	1,345	1,432	1,632	1,750	2,588	3,024		641	,400 3	,442 3,	545 3,	,508 3,	,662 4,4	1,421 5,0	5,091 5,	5,505		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		6,027	924	927	1,111	1,257	1,333	1,490	1,575	2,304	2,839			3,490 3	3,447 3,	3,475 3,	,322 3,	,600 4,2	1,244 4,5	4,907 5	5,318		
5,480 839 829 971 1,092 1,321 1,360 1,392 2,440 3,090 5,193 791 778 931 1,006 1,391 1,391 1,395 1,271 1,395 2,440 3,090 4,807 738 831 1,006 1,331 1,396 1,731 1,936 2,744 3,095 4,807 630 630 840 913 936 1,136 1,737 1,936 1,738 2,233 4,817 640 773 848 910 1,736 1,936 1,738 2,233 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,721 1,887 1,501 1,561 1,581 1,7		5,769	884	878	1,042	1,176	1,242	1,415	1,533	1,817	2,461				6,433 3,	,421 3,	,398 3,	,660 4,0	1,043 4,6	4,698 5	5,104		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		5,480	839	829	1/6	1,092	1,160	1,352	1,443	1,680	1,926			3,324 3	3,350 3,	,314 3,	,328 3,	,656 3,8	3,828 4,4	467 4	4,859		
4,80 739 725 888 974 1,010 1,256 1,530 1,537 1,509 1,738 2,332 2,332 2,332 2,332 2,332 2,332 2,332 2,332 2,332 2,332 2,332 2,332 1,509 1,738 2,332 1,509 1,738 2,332 2,332 1,231 2,332 1,537 1,538 <td></td> <td>5,159</td> <td>161</td> <td>778</td> <td>931</td> <td>1,026</td> <td>1,084</td> <td>1,291</td> <td>1,395</td> <td>1,582</td> <td>1,721</td> <td></td> <td></td> <td>3,017 3</td> <td>3,186 3,</td> <td>3,153 3,</td> <td>3,068 3,</td> <td>,564 3,7</td> <td>3,708 4,2</td> <td>4,215 4</td> <td>1,587</td> <td></td> <td></td>		5,159	161	778	931	1,026	1,084	1,291	1,395	1,582	1,721			3,017 3	3,186 3,	3,153 3,	3,068 3,	,564 3,7	3,708 4,2	4,215 4	1,587		
4617 684 670 840 913 956 1,151 1,280 1,667 1,871 1,871 4,922 573 548 630 640 773 966 1,196 1,922 1,660 1,867 1,821 1,221 4,922 573 548 719 767 773 960 1,212 1,887 1,500 1,605 1,827 1,887 1,501 1,605 1,827 1,887 1,501 1,605 1,827 1,887 1,501 1,605 1,887 1,501 1,605 1,887 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501 1,605 1,501		4,809	739	725	888	974	1,010	1,226	1,350	1,527	1,639			2,645 2	2,904 2,	2,948 2,	2,731 3,	,351 3,7	3,718 3,5	3,947 4	1,292		
48.4 630 610 783 844 857 1126 1126 1126 1137 1182 1271 1827 1271 4922 572 588 719 662 690 857 1212 1822 2064 1887 1201 1690 4,808 590 686 650 682 690 857 1212 1882 2164 1791 1690 4,808 441 419 579 588 003 774 1400 1775 1408 3,707 333 239 388 486 580 063 1575 1408 1777 1409 3,707 333 239 388 486 580 0691 1055 1577 1408 2,374 168 151 204 313 310 3564 057 1366 1577 1409 2,374 168 151 204 131 377 1409		4,617	684	670	840	913	936	1,153	1,280	1,492	1,630			2,324 2	2,700 2,	2,987 2,	3,889 3,	3,047 3,6	3,622 3,5	3,912 4	4,075		
4922 572 548 719 767 775 969 1.212 1,822 2,024 1,887 1,500 1,995 4,088 509 466 650 682 600 877 1,212 1,882 2,024 1,887 1,500 1,995 3,707 391 347 600 520 683 603 794 1,101 1,772 1,241 1,773 1,366 1,366 1,366 1,366 1,366 1,366 1,376 1,366		4,834	630	610	783	844	857	1,066	1,196	1,674	1,835			1,952 2	2,527 2,	2,839 2,	2,831 2,	2,846 3,4	3,417 3,8	3,848 4	4,211		
488 509 466 650 682 600 857 1.212 1.862 2.146 1.701 1.905 3.707 3.88 603 877 1.212 1.862 2.146 1.773 1.368 3.707 3.88 603 782 1.160 1.777 1.248 1.773 1.368 3.707 3.53 2.88 360 782 1.055 1.582 1.368 1.773 1.368 3.707 3.53 2.88 360 470 782 1.368 1.737 1.368 3.77 3.73 3.03 480 580 693 1.268 1.377 1.306 3.77 1.68 1.51 2.04 3.13 3.10 5.66 677 3.74 1.68 1.51 2.04 3.13 3.10 5.66 677 3.74 1.68 1.51 2.04 3.13 3.10 5.66 677 1.566 1.51		4,922	572	548	719	767	775	969	1,212	1,822	2,024			,869 2	2,158 2,	2,534 2,	2,532 2,	2,811 3,2	,265 3,6	3,637 4	4,127		
4,408 441 419 579 588 603 794 1,160 1,777 2,124 1,773 1,368 3,707 391 347 490 520 603 794 1,160 1,777 2,124 1,773 1,368 3,707 391 347 490 520 608 782 1,035 1,938 1,777 1,368 3,707 353 293 388 460 580 644 883 1,598 1,601 1,571 1,905 2,574 280 241 302 449 471 578 0,693 1,66 1,511 1,905 1,365 168 151 204 313 310 364 422 646 576 677 4365 151 204 313 310 364 422 646 576 677		4,808	509	486	650	682	690	857	1,212	1,862	2,146	_		,758 1	,946 2	2,180 2.	2,269 2,	,686 3,1	3,189 3,4	3,454 3,	3,838		
3.707 391 347 400 520 608 782 1155 1582 1598 1737 1,400 3.17 2.374 280 388 449 471 578 0.93 1,577 1,346 2.374 280 281 308 449 471 578 0.93 1,136 1,346 1.365 158 211 204 313 310 364 422 644 1571 1,095 1.366 151 204 313 310 364 422 644 688 756 677		4,408	441	419	579	588	603	794	1,160	1,777	2,124			587 1	,756 1	,831 2,	2,109 2,	,387 2,5	2,951 3,3	3,345 3,	3,548		
2132 233 228 388 480 580 604 821 298 1003 1272 1346 2374 203 203 308 480 471 578 693 1035 1146 1231 1005 1366 151 204 313 310 310 364 422 634 635 755 647 1366 151 204 313 310 364 422 634 635 755 677		3,707	391	347	490	520	608	782	1,055	1,582	1,938			354 1	,543 1	,570 1,	,596 2,	,225 2.4	2,490 3,0	,080	3,388		
2,374 280 241 302 449 471 578 699 1,035 1,46 1,251 1,095 1,366 168 151 204 313 310 364 422 654 668 776 677 7.007 107 107 107 107 107 107 107 107 107		3,125	353	298	388	486	580	694	883	1,298	1,603		-	,263 1	,286 1.	,365 1;	,251 1,	,843 2,0	2,037 2,5	2,568 3	3,079		
1365 168 151 204 313 310 364 422 64 688 756 677		2,374	280	241	302	449	471	578	669	1,035	1,146		-	060	953 1	,077	997 1,	,405 1,5	,516 1,5	1,575 2	2,477		
constructions and and and and and and and and		1,363	168	151	204	313	310	364		634	688						630	839 8	874 8	837 1	,053	T	LOCATION
2,000 2,000 3,000 4,000 3,000 3,000 2,000 2,000 2,000 3,834 3,000 4,000	HEAR	6,883	1,156	1,951	3,566	4,007	3,567	3,198	2,906	2,987	3,834	3,784 4	1,098 4	1,432 4	131 4.	341 4,	,163 4,0	.024 4.8	855 5.5	569 6	6,023 1,	1,156	-

EXPERIPOLARE DATA- EQ1 2 3 4 5 6 7 STORY UNCONTROLLED BULLIDIG 1 2 3 4 5 6 7 ISOLATOR FLOOR UNCONTROLLED BULLIDIG 1 2 3 4 5 6 7 ISOLATOR FLOOR UNCONTROLLED BULLIDIG 1 3 6.50 9.236 8.60 7.84 5.84 5.85 4.48 5.85 4.58 4.48 5.85 4.58 4.48 5.86 4.58 4.48 5.85 4.58 4.48 5.86 5.86 7.37 4.58 4.48 5.86 5.98 5.910 7.39 6.39 1.39 1.48 6.90 7.88 4.58 6.39 2.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.39 6.43 6.34 6.35 6.43 6.35 6.43 6.39 6.39	7 8 1,681 1,918 4,458 5,652 4,329 4,476 4,195 3,866	ISOLATOR LEVEL 9 10 1,739 1,709	R LEVEL	:									
UNCONTROLLED BUILDING 1 2 3 4 5 6 7 134 1123 1124 125 2034 1752 1667 1681 6,498 3,572 6,599 2,216 8,610 7,844 5,785 4,488 6,399 1,113 1,620 7,648 8,466 7,376 5,715 4,329 6,390 1,112 1,162 4,451 6,805 5,940 6,4195 6,290 1,100 1,153 1,900 3,599 4,362 4,171 4,254 6,290 1,100 1,153 1,900 3,599 4,362 4,171 4,254 6,290 1,100 1,153 1,900 3,599 4,362 4,171 4,254 6,290 1,100 1,153 1,900 3,599 4,362 4,171 4,254 6,025 1,022 1,111 1,747 1,647 2,980 3,110		9 1,739	10 11	;									
6498 3173 1,134 1,139 2,109 2,136 1,136 1,160 2,646 3,448 5,958 9,216 8,610 7,844 5,985 4,548 5,956 5,116 1,166 4,648 4,548 5,765 2,216 4,458 6,215 4,458 6,215 4,458 6,215 4,458 6,215 4,458 6,215 4,458 6,215 4,428 6,215 4,173 4,294 4,294 4,254 4,264 4,264 4,264 4,264 4,264 4,264 4,264 2,664 4,264 4,264 2,664 4,264 2,664 4,264 2,664 4,264 2,664 4,264 2,664 4,264 4,264 2,664 4,264 2,664 1		1,739		12	13	14	15	16	17	18	19		
3372 6.595 9.236 8.610 7.84 5.785 4.485 1,130 4.507 7.68 8.451 5.785 4.485 1,112 1,102 1,451 6.805 5.900 5.900 4.105 1,100 1,153 1,900 3.590 4.362 6.403 4.033 1,000 1,134 1,844 1,737 1,423 4.033 4.033 4.033 4.033 4.034			1,709 1,7	1,775 1,930		2,073	1,997	1,917	1,823	1,668	1,468		
1130 1300 7.681 8.456 7.56 3.76 3.76 3.75 4.72 4.72 1112 1.162 4.161 6.805 5.900 5.900 4.92 1.95 1.102 1.153 1.900 4.590 4.013 4.254 1.95 1.002 1.134 1.814 1.734 3.139 4.033 3.624 1.062 1.111 1.744 1.697 4.132 2.638 3.110		7,317	-	5,116 5,697	7 5,595	5,924	5,758	5,842	6,010	6,297	7,044		
1,112 1,102 4,451 6,805 5,940 5,040 4,195 1,100 1,153 1,900 5,390 4,362 4,171 4,254 1,002 1,134 1,814 1,731 3,159 4,033 3,624 1,002 1,134 1,814 1,771 1,662 3,110 1,264 2,264 1,002 1,134 1,814 1,771 1,673 3,129 3,100 3,100		6,634	5,477 5,2	5,266 5,245		5,576	5,509	5,440	5,545	6,187	6,353		
1,100 1,153 1,900 3,599 4,562 4,171 4,254 1,100 1,131 1,129 1,100 1,133 3,564 1,102 1,111 1,747 1,697 1,643 2,599 3,110		5,328	5,467 4,4	4,495 4,583	3 4,782	5,147	5,319	5,180	5,283	5,963	6,115		
1,082 1,134 1,814 1,731 3,159 4,033 3,624 1,052 1,111 1,747 1,697 1,643 2,989 3,110				4,430 4,198			4,940	5,104	5,199	5,585	5,903		
1,052 1,111 1,747 1,697 1,643 2,989 3,110		4,268	4,323 4,5	4,535 4,297	7 4,287		4,540	4,808	5,054	5,626	5,651		
	3,110 3,632			4			4,237	4,439	4,823	5,582	5,657		
1,018 1,084 1,702 1,638 1,561 1,474 2,378			3,682 3,9	3,950 4,124		4,116	3,971	4,130	4,563	5,261	5,660		
984 1,049 1,657 1,563 1,418 1,381 1,600		3,690	3,609 3,7	3,746 3,860		4,016	3,968	3,950	4,321	4,706	5,469		
9 4,990 954 1,002 1,592 1,481 1,267 1,358 1,527 1		2,123	3,355 3,3	3,377 3,562	2 3,698	3,795	4,020	4,155	4,386	4,548	5,015		
921 943 1,486 1,392 1,353 1,339 1,454			2,402 3,1	3,135 3,260			3,847	4,259	4,212	4,436	4,759		
4,533 879 874 1,347 1,295 1,336 1,320 1,519	1,519 1,881	1,892		2,385 3,004		3,384	3,551	4,256	4,213	4,246	4,654		
824 798 1,188 1,179 1,286 1,319 1,544			1,844 1,7	1,784 2,429		3,524	3,256	3,970	4,163	4,162	4,486		
4,157 753 728 1,036 1,109 1,237 1,326 1,478			_	_			3,412	3,457	3,838	3,988	4,165		
668 669 895 1,017 1,112 1,251 1,401				1,820 1,745		2,657	3,295	3,358	3,533	3,604	3,691		
3,499 579 597 828 898 1,021 1,132 1,377		1,969		,856 1,649			2,630	3,117	3,307	3,366	3,132		
3,166 523 518 770 823 1,013 1,136 1,388	1,388 1,705	1,780	1,754 1,6	1,649 1,443	3 1,549		1,669	2,469	2,829	3,078	3,287		
17 2,693 467 472 661 816 939 1,061 1,354 1	1,354 1,549	1,576	2,1 999 1,5	1,507 1,440	0 1,417	1,554	1,675	1,638	2,191	2,726	3,224		
783 810	1,167 1,284	1,363	1,375 1,3	,328 1,302		1,377	1,567	1,610	1,492	2.209	2,833		
289 336 483 642 747 755	-	-	1,109 1,2	-	-	1,182	1,316		1,440	1,344	2,082		
2,045 183 212 357 456 509 479 576				808 742			920		1,065	686	865	TOC	LOCATION
7 9,236 8,610 7,834 5,785 4,458	۰.	7,317		6,116 5,69	7 5,595	5,924	5,758		6,010	6,297	7,044	3,572	-

Table A1.23 Story shears after optimization for EQ11 data

																							LOCATION	-
																						I		1,140
		19	2,304	6,147	6,086	6,004	5,896	5,762	5,603	5,417	5,205	4,967	4,702	4,413	4,104	3,772	3,583	3,609	3,398	2,981	2,600	2,361	1,199	6,147
		18	2,488	5,706	5,645	5,561	5,452	5,318	5,159	4,976	4,770	4,540	4,288	4,017	3,732	3,428	3,114	2,868	2,517	2,275	2,241	1,823	1,047	5,706
		17	2,545	4,858	4,800	4,722	4,622	4,501	4,359	4,197	4,016	3,818	3,606	3,433	3,206	2,907	2,649	2,379	2,105	2,088	1,901	1,393	874	4,858 7
		16	2,703	4,165	4,093	3,968	3,852	3,736	3,605	3,636	3,750	3,786	3,670	3,366	2,939	2,585	2,215	2,017	1,906	2,056	1,611	1,213	716	4,165
		15	2,617	4,346	4,210	4,022	3,838	3,795	3,922	4,047	4,074	3,934	3,590	3,065	2,612	2,198	1,857	1,668	2,282	2,044	1,716	1,252	714	4,346
		14	2,581	4,444	4,256	4,038	3,974	4,093	4,203	4,216	4,067	3,720	3,173	2,613	2,440	2,298	2,152	2,522	2,430	2,195	1,805	1,300	753	4,444
		13	2,539	4,547	4,237	4,166	4,302	4,410	4,412	4,260	3,912	3,361	2,648	2,456	2,345	2,231	2,593	2,578	2,431	2,146	1,757	1,306	783	4,547
		12	2,489	4,576	4,559	4,727	4,806	4,765	4,565	4,185	3,624	2,934	2,280	2,211	2,140	2,590	2,632	2,563	2,378	2,100	1,751	1,332	803	4,806
		П	2,219	5,392	5,544	5,555	5,388	5,053	4,560	3,953	3,282	2,440	1,944	1,916	2,318	2,419	2,455	2,408	2,268	2,036	1,723	1,360	856	5,555
	R LEVEL	10	2,044	6,183	6,163	5,932	5,474	5,065	4,642	3,935	2,878	1,903	1,772	2,190	2,344	2,476	2,542	2,518	2,391	2,165	1,972	1,568	938	6,183
	ISOLATOR LEVEL	6	1,831	6,255	6,267	6,139	5,844	5,299	4,438	3,236	1,895	1,575	1,997	2,180	2,352	2,505	2,598	2,586	2,567	2,430	2,116	1,601	912	6,267
E		8	1,688	6,435	6,392	6,094	5,492	4,567	3,343	2,005	1,613	1,840	2,013	2,182	2,340	2,496	2,626	2,659	2,543	2,452	2,132	1,577	869	6,435
STORY SHEAR(d)		7	1,533	6,559	6,214	5,596	4,670	3,463	2,238	1,492	1,487	1,626	1,768	1,900	2,019	2,148	2,285	2,363	2,305	2,088	1,732	1,316	741	6,559
STOR		9	1,380	6,232	5,580	4,671	3,517	2,321	1,434	1,281	1,242	1,326	1,420	1,505	1,542	1,509	1,609	1,728	1,760	1,657	1,410	1,031	568	6,232
		5	1,330	4,774	4,284	3,509	2,391	1,531	1,261	1,202	1,217	1,275	1,359	1,417	1,394	1,349	1,246	1,373	1,444	1,396	1,213	106	500	4,774
		4	,329	1,240	3,465	2,371	165,1	1,270	,227	1,180	1,129	1,073	1,155	1,285	,356	,349	1,275	1,307	1,244	1,094	890	649	369	1,240
		4	144	2,631	080	,374	068	995	935	937	932	917	168	949	217	957	887	792	766	677	542	387	233	2,631
		3	093 1,	,376 2,	44 2	12 1.	940 1,	882	883	881	872	855	836	839	817	771	702	633	589	521	429	=	73	,376 2,
		2	,178 1,0	40 1,3	,093 1.0	0,1 1,0	934 9	67 8	860 8	847 8	826 8	829 8	833 8	815 8	8 177 8	720 7	665 7	655 6	615 5	546 5	450 4	325 3	80 1	,140 1,3
		-	1,1	1,1	-	-		8 69							-		-	-						_
	EARTHQUAKE DATA: EQ 12	UNCONTROLLED BUILDING		6,811	6,742	6,648	6,524	6'369	6,185	5,969	5,722	5,442	5,132	4,793	4,429	4,034	3,920	4,221	4,276	4,053	3,538	2,717	1,596	6,811
	EARTHQU	STORY	ISOLATOR FLOOR	1	2	6	4	5	6	7	80	9	10	11	12	13	14	15	16	17	18	19	20	MAX STORY SHEAR

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DRIFT		9	92.54%	0.02%	0.03%	0.03%	0.04%	0.04%	0.05%	0.19%	0.24%	0.24%	0.23%	0.24%	0.23%	0.23%	0.22%	0.22%	0.20%	0.19%	0.17%	0.15%	0.19%	•
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	EARTHQUAKE DATA: EQ 2	UNCONTROLLED BUILDING		0.50%	0.79%	0.89%	0.91%	%96.0	0.97%	1.01%	1.00%	0.99%	0.96%	%66.0	%96.0	0.98%	0.95%	0.92%	0.84%	0.80%	0.75%	0.68%	0.65%	1.01%
	EARTHQ	STORY	ISOLATOR FLOOR	1	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	MAX DRIFT RATIO

APPENDIX 2

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Table A2.3 Drift ratios after ontimization for EO3 data

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		19	64.67%	0.13%	0.23%	0.27%	0.30%	0.34%	0.37%	0.40%	0.42%	0.47%	0.54%	0.60%	0.66%	0.71%	0.75%	0.77%	0.78%	0.78%	0.78%	0.75%	1.04%	1.04%
		18	66.69%	0.12%	0.20%	0.24%	0.29%	0.32%	0.35%	0.38%	0.40%	0.45%	0.51%	0.56%	0.60%	0.64%	0.66%	0.67%	0.67^{0}_{0}	0.67%	0.64%	0.49%	1.53%	1.53%
		17	69.02%	0.15%	0.25%	0.29%	0.31%	0.32%	0.33%	0.35%	0.37%	0.42%	0.47%	0.51%	0.55%	0.57%	0.58%	0.58%	0.58%	0.56%	0.53%	0.89%	1.68%	1.68%
		16	70.68%	0.15%	0.24%	0.26%	0.27%	0.28%	0.29%	0.30%	0.34%	0.40%	0.45%	0.49%	0.52%	0.53%	0.53%	0.52%	0.50%	0.57%	0.98%	1.15%	2.01%	2.01%
		15	70.49%	0.13%	0.22%	0.26%	0.30%	0.33%	0.37%	0.42%	0.46%	0.50%	0.54%	0.56%	0.57%	0.57%	0.56%	0.53%	0.47%	0.71%	0.90%	1.00%	2.00%	2.00%
		14	59.42%	0.12%	0.22%	0.26%	0.31%	0.37%	0.43%	0.48%	0.52%	0.55%	0.57%	0.57%	0.57%	0.56%	0.52%	0.46%	0.70%	0.91%	1.09%	1.20%	2.46%	2.46%
		13	60.72%	0.13%	0.23%	0.28%	0.33%	0.38%	0.43%	0.47%	0.50%	0.51%	0.52%	0.52%	0.51%	0.47%	0.39%	0.66%	0.82%	1.03%	1.19%	1.26%	2.34%	2.34%
		12	63.19%	0.12%	0.23%	0.29%	0.34%	0.38%	0.40%	0.41%	0.42%	0.43%	0.43%	0.42%	0.40%	0.30%	0.44%	0.54%	0.61%	0.70%	0.81%	0.87%	1.62%	1.62%
	VEL	=	94.31%	0.18%	0.33%	0.40%	0.47%	0.51%	0.53%	0.54%	0.54%	0.53%	0.51%	0.47%	0.22%	0.33%	0.35%	0.36%	0.33%	0.32%	0.39%	0.43%	0.85%	0.85%
	ISOLATOR LEVEL	10	89.66%	0.17%	0.32%	0.38%	0.44%	0.48%	0.50%	0.51%	0.50%	0.48%	0.44%	0.22%	0.34%	0.39%	0.40%	0.38%	0.33%	0.44%	0.57%	0.65%	1.31%	1.31%
	10SI	6	85.58%	0.16%	0.30%	0.36%	0.42%	0.44%	0.46%	0.45%	0.43%	0.39%	0.22%	0.32%	0.34%	0.38%	0.37%	0.37%	0.36%	0.36%	0.34%	0.41%	0.97%	0.97%
201		8	92.83%	0.18%	0.31%	0.35%	0.39%	0.40%	0.39%	0.37%	0.33%	0.21%	0.26%	0.29%	0.29%	0.31%	0.31%	0.32%	0.30%	0.31%	0.33%	0.35%	0.73%	0.73%
DRIFT RALIUS		7	92.69%	0.15%	0.24%	0.26%	0.27%	0.27%	0.25%	0.22%	0.20%	0.25%	0.26%	0.28%	0.28%	0.29%	0.28%	0.28%	0.26%	0.26%	0.26%	0.25%	0.55%	0.55%
ã		9	91.63%	0.12%	0.20%	0.20%	0.20%	0.19%	0.16%	0.20%	0.25%	0.26%	0.26%	0.28%	0.28%	0.29%	0.29%	0.29%	0.27%	0.27%	0.26%	0.23%	0.47%	0.47%
		5	92.28%	0.07%	0.11%	0.11%	0.10%	0.09%	0.18%	0.24%	0.25%	0.26%	0.26%	0.27%	0.28%	0.29%	0.29%	0.29%	0.27%	0.26%	0.25%	0.23%	0.43%	0.43%
		4	91.61%	0.06%	0.07%	0.06%	0.05%	0.17%	0.21%	0.24%	0.24%	0.24%	0.24%	0.26%	0.26%	0.28%	0.28%	0.28%	0.26%	0.25%	0.24%	0.21%	0.39%	•
		3	90.71%	0.03%	0.04%	0.03%	0.15%	0.20%	0.21%	0.22%	0.22%	0.23%	0.23%	0.24%	0.24%	0.26%	0.26%	0.26%	0.24%	0.23%	0.21%	0.19%	0.33%	0.33%
		2	89.40%	0.02%	0.03%	0.14%	0.18%	0.20%	0.20%	0.21%	0.21%	0.21%	0.21%	0.22%	0.22%	0.24%	0.24%	0.24%	0.22%	0.21%	0.19%	0.17%	0.32%	0.32%
		-	87.69%	0.02%	0.14%	0.18%	0.19%	0.20%	0.19%	0.20%	0.19%	0.19%	0.19%	0.20%	0.20%	0.21%	0.21%	0.21%	0.20%	0.19%	0.17%	0.17%	0.32%	0.32%
	EARTHQUAKE DATA: EQ 5	UNCONTROLLED BUILDING		0.63%	0.99%	1.08%	1.05%	1.05%	1.00%	0.94%	1.01%	1.14%	1.22%	1.35%	1.36%	1.46%	1.51%	1.53%	1.41%	1.31%	1.30%	1.39%	1.60%	1.60%
	EARTHQU	STORY	ISOLATOR FLOOR	1	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	MAX DRIFT RATIO

Table A2.5 Drift ratios after optimization for EQ5 data

Table A2.6 Drift ratios after optimization for EQ6 data

							DR	DRIFT RATIOS	OS													
EARTHC	EARTHQUAKE DATA: EQ 6									ISOLA	ISOLATOR LEVEL	EL										
STORY	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		86.60%	84.20%	78.98%	73.29%	73.39%	71.19% 7	72.53% 7	78.50% (66.38% (50.37% 5	56.77% 4	49.86% 4	11.90% 49	49.68% 4'	47.65% 44	44.43% 3	34.93% 3	35.18% 2	29.56%		
1	0.46%	0.01%	0.01%	0.02%	0.04%	0.05%	0.06%	0.09% 0	0.12%	0.13%	0.12%	0.10%	0.08% (0.09% 0	0 %60.0	.07% 0	0.06% (0.07% (0.08% 0	%60.0		
2	0.72%	0.14%	0.02%	0.03%	0.05%	0.07%	0.10%	0.15% 0	0.20%	0.23%	0.22%).18%	0.15% ().16% 0	0.16% 0	0.12% 0	0.12% (.12% (0.14% 0	0.16%		
3	0.81%	0.18%	0.14%	0.02%	0.04%	0.06%	0.10%	0.16% 0).23%	0.27%	0.26%	.23%	.19% (0.20% 0	20% 0	0.16% 0).16% (.14% (0.16% 0	0.19%		
4	0.82%	0.18%	0.18%	0.14%	0.03%	0.06%	0.10%	0.16% 0	0.25%	0.31%	0.30%	0.27%	-	Ũ	0.23% 0	0.19% 0	0.19% ().16% (0.20% 0	0.22%		
5	0.84%	0.19%	0.19%	0.19%	0.15%	0.04%	0.09%	0.16% 0).25%	0.33%	0.32%).29%	0.25% (0.25% 0	0.26% 0	0.21% 0	0.22% (0.18% (0.23% 0	0.26%		
9	0.84%	0.19%	0.20%	0.21%	0.19%	0.14%	0.07% (0.15% 0	0.25%	0.34%	0.33%	0.31%	0.27% (0.27% 0	0.27% 0	0.24% 0	0.24% (0.20% (0.26% 0	0.29%		
7	0.86%	0.19%	0.21%	0.23%	0.22%	0.19%	0.15% (0.13% 0	0.23%	0.33%	0.33%	0.31%	0.28% (0.28% 0	0.28% 0	0.26% 0	0.26% (0.22% (0.28% 0	0.32%		
8	0.84%	0.19%	0.21%	0.23%	0.23%	0.21%	0.18% (0.15% 0	0.21%	0.32%	0.32%	0.31%	-	0.28% 0	0.29% 0	0.27% 0	0.27% (0.24% (0.35%		
6	0.89%	0.18%	0.21%	0.23%	0.23%	0.22%	0.20%	0.19% 0	0.19%	0.28%	0.31%	0.30%	0.27% (0.28% 0	0.29% 0	0.28% 0	0.28% (0.25% (0.32% 0	0.37%		
10	0.91%	0.18%	0.21%	0.23%	0.23%	0.22%	0.20%	0.19% 0	0.23%	0.19%	0.28%	0.29%	0.26% (0.28% 0	0.29% 0	0.29% 0	0.29% (0.26% (0.34% 0	.40%		
11	1.00%	0.18%	0.21%	0.24%	0.25%	0.24%	0.22%	0.21% 0	0.26%	0.26%	0.22%	0.27%	0.25% (0.27% 0	0.29% 0	0.29% 0	0.30% (0.27% (0.35% 0	.42%		
12	1.03%	0.19%	0.22%	0.24%	0.25%	0.24%	0.23%	0.21% 0	0.26%	0.28%	0.29%	0.20%	0.23% (0.26% 0	0.28% 0	0.30% 0	0.31% 0	0.28% (0.37% 0	.43%		
13	1.10%	0.19%	0.23%	0.25%	0.26%	0.26%	0.24%	0.22% 0	0.28%	0.29%	0.34%	0.30%	0.35% (0.24% 0	0.27% 0	0.30% 0	0.31% (0.29% (0.37% 0	0.45%		
14	1.11%	0.20%	0.23%	0.26%	0.27%	0.26%	0.25%	0.22% 0	0.28%	0.29%	0.35%	0.35%	0.54% (0.44% 0	0.26% 0	0.30% 0	0.31% 0	0.30% (0.38% 0	.46%		
15	1.10%	0.20%	0.24%	0.27%	0.27%	0.26%	0.25%	0.22% 0	0.29%	0.29%	0.36%	0.39%	0.67% (0.76% 0	0.49% 0	0.29% 0	0.31% (0.30% (0.38% 0	0.46%		
16	1.03%	0.19%	0.23%	0.26%	0.26%	0.25%	0.23%	0.21% 0	0.27%	0.26%	0.34%	0.39%	0.74% (0.92% 0	0.73% 0	0.45% 0	0.30% (0.30% (0.38% 0	0.46%		
17	1.00%	0.19%	0.22%	0.26%	0.26%	0.24%	0.23%	0.20% 0	0.26%	0.25%	0.32%	0.40%	0.83%	1.08% 0	0.91% 0	0.68% 0	0.47% (0.29% (0.38% 0	0.46%		
18	0.97%	0.19%	0.22%	0.25%	0.25%	0.23%	0.22%	0.19% 0	0.24%	0.25%	0.33%	0.38%	0.87%	1.16% 1	1.03% 0	0.78% 0	0.61% (0.49% (0.37% 0	0.46%		
19	0.90%	0.18%	0.20%	0.23%	0.23%	0.21%	0.20%	0.17% 0	0.23%	0.24%	0.31%	0.35%	0.84%	1.14% 1	1.07% 0	0.82% 0	0.66% (0.65% (0.49% 0	0.45%		
20	1.12%	0.26%	0.27%	0.32%	0.31%	0.30%			0.41%	0.55%			1.38%				1.34%]	1.56%]	1.30% 0	0.81%		LOCATION
MAX DRIFT RATIO	1.12%	0.26%	0.27%	0.32%	0.31%	0.30%	0.30%	0.30% 0.30%	0.41%	•	•	0.59%	•	•	1.85% 1	1.41% 1	•	1.56% 1	1.30% C		0.26%	-

	DRIFT RATIOS	DRIFT RATIOS	DRIFT RATIOS	DRIFT RATIOS	RET RATIOS	IOS		TIOSI	ISOLATOR LEVEL	VEL							
9	5 6	5 6	9		7		8	6	10	11	12	13	14	15	16	17	18
63.34% 60.11% 55.73% 53.18% 52.48% 52.80% 3	55.73% 53.18% 52.48%	53.18% 52.48%	52.48%		52.80%		53.58%	62.10%	59.84%	59.69%	48.20%	41.04%	43.66%	42.40% 4	42.72% 3	39.69% 3	30.72% 23.63%
0.03% 0.04% 0.04%	0.03% 0.04% 0.04%	0.04%	0.04%		0.05%		0.05%	0.06%	0.07%	0.06%	0.06%	0.08%	0.07%	0.07%	0.06%	0.06% 0	0.07% 0
0.02% $0.02%$ $0.04%$ $0.06%$ $0.07%$ $0.09%$	0.04% 0.06% 0.07% 0	0.06% 0.07%	0.07%		0.09%		0.09%	0.11%	0.13%	0.11%	0.11%	0.15%	0.14%	0.13%	0.11%	0.11% 0	0.13% 0.14%
0.11% 0.02% 0.04% 0.06% 0.08% 0.10%	0.04% 0.06% 0.08% 0	0.06% 0.08% (0.08%	Ĭ	0.10%		0.10%	0.12%	0.15%	0.13%	0.14%	0.19%	0.18%	0.17%	0.14%	0.14% 0	0.15% 0.16%
0.14% 0.11% 0.03% 0.06% 0.08% 0.11%	0.03% 0.06% 0.08%	0.06% 0.08%	0.08%		0.11%		0.11%	0.13%	0.17%	0.15%	0.16%	0.22%	0.22%	0.20%	0.17%	0.18% 0	0.18% 0
0.11% 0.05% 0.08%	0.11% 0.05% 0.08%	0.05% 0.08%	0.08%	-	0.11%		0.12%	0.14%	0.18%	0.16%	0.18%	0.25%	0.25%	0.23%	0.19%	0.21% 0	0.21% 0.21%
0.15% 0.15% 0.14% 0.11% 0.07% 0.10%	0.14% 0.11% 0.07%	0.11% 0.07%	0.07%		0.10%		0.12%	0.14%	0.19%	0.17%	0.19%	0.27%	0.28%	0.25%	0.22%	0.24% 0	0.25% 0
0.15% 0.15% 0.12%	0.15% 0.15% 0.12%	0.15% 0.12%	0.12%		0.10%		0.12%	0.13%	0.19%	0.17%	0.19%	0.28%	0.31%	0.27%	0.25%	0.26% 0	0.28% 0.27%
0.16% 0.16% 0.15% 0.15% 0.15% 0.12%	0.15% 0.15% 0.15%	0.15% 0.15%	0.15%		0.12%		0.11%	0.13%	0.18%	0.17%	0.20%	0.29%	0.32%	0.30%	0.27%	0.29% 0	0.30% 0.30%
0.15% 0.15% 0.15%	0.15% 0.15% 0.15%	0.15% 0.15%	0.15%		0.15%		0.14%	0.13%	0.17%	0.16%	0.20%	0.29%	0.34%	0.32%	0.30%	0.31% 0	0.33% 0.34%
0.15%	0.14% 0.15% 0.15%	0.15% 0.15%	0.15%		0.15%		0.16%	0.18%	0.16%	0.16%	0.20%	0.29%	0.34%	0.33%	0.31%		
0.15% 0.16%	0.15% 0.16% 0.16%	0.16% 0.16%	0.16%		0.16%		0.18%	0.22%	0.20%	0.14%	0.20%	0.29%	0.35%	0.34%	0.33%	0.34% 0	0.36% 0.39%
0.15% 0.16% 0.16%	0.15% 0.16% 0.16%	0.16% 0.16%	0.16%		0.16%		0.17%	0.23%	0.23%	0.20%	0.19%	0.28%	0.35%	0.34%	0.34%	0.35% 0	0.38% 0
0.15% 0.17% 0.17%	0.15% 0.17% 0.17%	0.17% 0.17%	0.17%		0.16%		0.18%	0.24%	0.27%	0.26%	0.28%	0.27%	0.34%	0.34%		0.36% 0	
0.16% $0.15%$ $0.15%$ $0.17%$ $0.17%$ $0.16%$	0.15% 0.17% 0.17%	0.17% 0.17%	0.17%		0.16%		0.19%	0.24%	0.28%	0.28%	0.38%	0.35%	0.33%	0.34%	0.35%	0.36% 0	0.39% 0.44%
0.16% 0.17% 0.17%	0.16% 0.17% 0.17%	0.17% 0.17%	0.17%		0.15%		0.19%	0.23%	0.27%	0.29%	0.42%	0.53%	0.49%	0.33%	0.35%	0.36% 0	
0.15% 0.16% 0.15%	0.15% 0.16% 0.15%	0.16% 0.15%	0.15%		0.14%		0.16%	0.22%	0.25%	0.27%	0.46%	0.65%	0.67%	0.47%	0.34%	0.36% 0	0.40% 0.45%
0.15% 0.14% 0.14% 0.15% 0.15% 0.15%	0.14% 0.15% 0.15%	0.15% 0.15%	0.15%		0.15%		0.18%	0.24%	0.25%	0.27%	0.53%	0.78%	0.76%	0.64%	0.52%	0.35% 0	0.40% 0.45%
0.14% $0.14%$ $0.14%$ $0.15%$ $0.16%$ $0.16%$	0.14% 0.15% 0.16%	0.15% 0.16%	0.16%		0.16%		0.21%	0.29%	0.30%	0.26%	0.56%	0.85%	0.77%	0.66%	0.70%	0.55% 0	0.38% 0.45%
0.13% 0.13% 0.12% 0.14% 0.17% 0.18%	0.12% 0.14% 0.17%	0.14% $0.17%$	0.17%		0.18%		0.21%	0.33%	0.34%	0.27%	0.53%	0.83%	0.73%	0.60%	0.72%	0.74% 0	0.44% 0.44%
	0.20% 0.25% 0.31%	0.25% 0.31%	0.31%		0.35%		0.40%	0.65%	0.72%	0.53%	0.77%	1.29%	1.10%	1.01%	1.19%	1.37%]	1.11% 0.72%
0.200 0.350 0.210/															•	•	

Table A2.7 Drift ratios after optimization for EQ7 data

Table A2.8 Drift ratios after optimization for EQ8 data

EARTHOUAKE DATA: EO 8							DKI	DRIFT RATIOS	~	ISOLAT	ISOLATOR LEVEL	L										
BUILDING 1 2 3	4	4	4		5				8	9	10				14	15	16	17		19		
86.13% 82.41% 77.82% 73.62% 69.84	82.41% 77.82% 73.62%	77.82% 73.62%	73.62%		69.84	-	66.17% 60	50.31% 50.45%		45.45% 44	44.50% 42	12.70% 35	35.95% 20	%	26.80% 2/	%	27.32% 2	27.81% 2	27.99%	28.58%		
9.69E-05 0.01% 0.02%	9.69E-05 0.01% 0.02%	5 0.01% 0.02%	0.02%		0.0			0.03% 0.0	0.03% 0.	0.04% 0.	Ŭ	0.03% 0.	0.04% 0	0.04% 0.			0.05%	0.06%	0.07%	0.07%		
0.79% 0.13% 0.02% 0.02% 0.02% 0.0	0.02% 0.02% 0.02% 0	0.02% 0.02%	0.02%		0.0	0.03%	0.04% 0.	0.05% 0.0	0.06% 0.0	0.06% 0.	0.06% 0.	0.06% 0.	0.07% 0	0.08% 0.	0.08% 0	0.09%	0.09%	0.12%	0.13%	0.14%		
0.89% $0.17%$ $0.14%$ $0.02%$ $0.02%$ 0.0	0.14% 0.02% 0.02% (0.02% 0.02% (0.02% (Ĭ	0.0	.03%	0.04% 0.	0.05% 0.0	0.07% 0.0	0.07% 0.	0.07% 0.	0.07% 0.	0.09% 0	0.09% 0.	0.10% 0	.11%).12%	0.15%	0.16%	0.18%		
0.91% 0.18% 0.17% 0.13% 0.03% 0.0	0.17% 0.13% 0.03% (0.13% 0.03% (0.03% (Č	0.0	0.03%	0.04% 0.	0.06% 0.0	0.07% 0.0	0.08% 0.	0.08% 0.	0.08% 0.	0.10% 0	0.11% 0.	0.11% 0	0.13%	0.14%	0.18%	0.19%	0.22%		
0.95% 0.19% 0.18% 0.17% 0.13% 0.0	0.18% 0.17% 0.13% (0.17% 0.13% (0.13% (Ĩ	0.0	0.03%	0.04% 0.	0.06% 0.0	0.07% 0.0	0.08% 0.	0.08% 0.0	0 %60.0	0.11% 0	Ū	12% 0	.14%	0.16%	0.20%	0.22%	0.25%		
0.96% 0.19% 0.19% 0.18% 0.16% 0.1	0.19% 0.18% 0.16% (0.18% 0.16% (0.16% (Ĭ	0.1	.13%	0.04% 0.	0.06% 0.0	0.07% 0.0	0.08% 0.	0.09% 0.	0.10% 0.	0.12% 0	0.13% 0.	0.13% 0).15% (0.17%	0.22%	0.25%	0.27%		
1.00% $0.20%$ $0.20%$ $0.19%$ $0.18%$ $0.16%$	0.20% 0.19% 0.18% (0.19% 0.18% (0.18% (_	0.16			_		0.08% 0.	0.09% 0.			-		0.16% (0.19%	0.24%	0.27%	0.30%		
0.99% $0.20%$ $0.19%$ $0.18%$ $0.18%$ 0.17	0.19% 0.18% 0.18%	0.18% 0.18%	0.18%		0.17			0.12% 0.0	0.07% 0.0	0.08% 0.	0.09% 0.			0.14% 0.	Ĩ	0.16%	0.20%	0.25%	0.28%	0.32%		
	0.19% 0.18% 0.17%	0.18% 0.17%	0.17%		0.17				0.14% 0.	0.07% 0.	0.09% 0.			-			0.21%	0.26%		0.34%		
0.17%	0.19% 0.18% 0.17%	0.18% 0.17%	0.17%	-	0.16%									-				0.26%		0.36%		
0.20% 0.19% 0.18% 0.17%	0.19% 0.18% 0.17%	0.18% 0.17%	0.17%	-	0.17			0.16% 0.1		0.19% 0.	0.16% 0.	0.10% 0.	0.14% 0	-			0.24%	0.27%		0.38%		
0.17%	0.19% 0.18% 0.17%	0.18% 0.17%	0.17%	-	0.1				0.19% 0.	0.20% 0.				-			0.24%			0.39%		
0.19% 0.19% 0.18% 0.17%	0.19% 0.18% 0.17%	0.18% 0.17%	0.17%		0.17			0.17% 0.20%				0.22% 0.	0.25% 0	0.15% 0.	0.17% 0	0.20%	0.25%	0.29%	0.34%	0.41%		
0.19% 0.18% 0.18% 0.17%	0.18% 0.18% 0.17%	0.18% 0.17%	0.17%	_	0.13		0.17% 0.	0.17% 0.1	0.19% 0.	0.21% 0.	0.23% 0.		0.30% 0			0.20%	0.25%	0.30%	0.35%	0.41%		
0.92% 0.18% 0.18% 0.17% 0.16% 0.16%	0.18% 0.17% 0.16%	0.17% 0.16%	0.16%		0.16%		0.17% 0.	0.17% 0.1	0.19% 0.	0.21% 0.			0.31% 0		0.32% 0	0.19%	0.25%	0.30%	0.36%	0.42%		
0.16% 0.16% 0.15%	0.16% 0.16% 0.15%	0.16% 0.15%	0.15%		0.15		0.15% 0.	0.15% 0.17%		0.21% 0.	0.23% 0.			0.35% 0.			0.25%		0.36%	0.42%		
0.15% 0.15% 0.15% 0.15%	0.15% 0.15% 0.15%	0.15% 0.15%	0.15%		0.14										0.45% 0		0.46%	0.30%	0.36%	0.42%		
	0.14% 0.14% 0.14%	0.14% 0.14%	0.14%		0.13			0.15% 0.1	0.16% 0.2	0.22% 0.	0.23% 0.					0.48%	0.60%	0.47%	0.36%	0.42%		
0.12%	0.13% 0.13% 0.12%	0.13% 0.12%	0.12%		0	0.12%	0.13% 0.			0.21% 0.							0.61%		0.45%	0.41%	l	
0.18% $0.16%$ $0.16%$ $0.16%$	0.16% 0.16% 0.16%	0.16% 0.16%	0.16%		0			0.22% 0.31%			0.46% 0.			0.67% 0.			0.96%	%96.0		0.83%		LOCATION
0.20% 0.19%	0.20% 0.19% 0.18%	0.19% 0.18%	0.18%	•	0.17%	•	0.19% 0	•	•	•	•	•	•	•	•	•	•	•	0.93%		0.17%	s

EARTHQUA STORY U ISOLATOR FLOOR 1 3	EARTHQUAKE DATA: EQ 9 RY UNCONTROLLED BUILDING 2 FLOOR						DRIFT	DRIFT RATIOS													
	NCONTROLLED BUILDING									ISOLATOR LEVEL	LEVEL										
1 2 3				3 4		5	6 10	7 2007 00		00 /061 20	10 1			3 14	1 15 40/ 32 310/						
3 5	0.40%	0.07% 0.0	0.01% 0.01	01 %0/.00		%CU 0	1 0/10.001	%60.66 %9C.101 %/C.C01 %000 %000 %000		0 0/01/00	0.05% 0.06%	0/00.01 0/0%	%010 %99 %010 %99			% 0 0 %	% 0.06%	%CC.1+ 0	%00.cc 0	_	
3	0.64%																				
	0.73%		Ū									2% 0.13%		2% 0.12%	% 0.13%		6 0.13%	0.16%			
4	0.76%		–																	1	
5	0.80%		-											5% 0.16%	% 0.17%						
6	0.81%										0.14% 0.16%										
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	0/11-T	•	0/17:0	0.000	10700	0.02.0	10000	•		0/1/0	0.000	100000	1 0/ CCT	0/ 07-7			1 N + C - 1	.T _ 0/0C	0/07	0/ /	

EARTHOU	EARTHOUAKE DATA: EO I						STOR	STORY SHEAR[tf]	E	ISOLAT	ISOLATOR LEVEL	1									
STORY	UNCONTROLLED BUILDING	_	5	3	4	5	9	2	~	6	10 1	1	13]4	15	16	17	18	19		
ISOLATOR FLOOR		1,766 1	1,650	1,514	1,374	1,225	1,189	1,125	1,149 1	1,208 1,	,156 1,	1,151 1,7	1,770 1,809	09 2,132	32 2,206	06 2,649	49 2,98/	4 2,665	5 2,113		
1	5,308	2,579 3		5,175	7,416	6,994	7,884 1	0,463 1	1,265 14	14,934 9,	9,471 9,	9,294 8,0	3,035 7,834		~	36 8,818	18 10,514	4 13,070	14,918		
2	4,713	1,651 2	2,807	4,022	6,701	6,845	7,384 1	0,569 1	0,792 14	14,822 9,	9,473 9,	9,254 8,2	3,201 7,645	45 8,648	48 8,304	04 8,764	64 10,272	2 12,789	14,915		
3	4,579	1,542 1		2,706	4,876	5,674	6,314	9,391	9,850 12	12,951 8,	8,460 8,5	8,213 7,4	7,484 6,761	51 7,818	18 7,473		7,815 9,303	3 11,155	5 13,456		
4	4,498		,440	1,389	3,105	4,409	5,456	8,483	9,406 11	11,504 7,	7,941 7,	7,546 7,0	7,035 6,092	92 7,135	35 6,878	78 7,285	85 8,626	6 10,052	12,257		
5	4,399		1,346	1,284	1,293	2,925	4,150	6,839	8,468 9	9,669 7,	7,174 6,	6,628 6,3	6,366 5,756	56 6,251	51 6,022	22 6,645	45 7,786	6 9,093			
9	4,140	1,254 1	1,260	1,210	1,220	1,187	2,773	4,870	6,984 8	8,285 6,	6,686 5,	5,729 5,621	21 5,358	58 5,273	73 5,111	11 6,146	46 7,281	1 8,226	9,599	-	
7	3,754	1,173 1		1,154	1,160	1,162	1,100	3,045	4,929 6	6,580 6,	6,282 5,	5,067 4,911	11 4,901	01 4,975	75 4,488	88 5,397	97 6,856	6 7,603	8,821		
8	3,427	1,104 1		1,109	1,116	1,144	1,098	1,035	2,960 4	4,696 5,	5,497 4,	4,721 4,401	01 4,979	79 4,937	37 4,159	59 4,621	21 6,167	7 7,132	8,294		
6	3,225	1,052 1	1,088	1,075	1,090	1,128	1,093	1,020	,025 2	2,942 4,	4,110 4,5	4,263 4,1	4,144 5,068	58 4,940	40 4,167	67 5,050	50 6,599	9 7,583	\$ 8,506		
10	3,247		,066	1,052	1,071	1,112	1,068	987	111 1	1,144 2,	2,514 3,	3,274 3,7	3,794 4,957	57 4,891	91 4,412	12 5,311	11 6,923	3 7,929	8,727		
11	3,431	1,022 1		1,039	1,050	1,088	1,025	937	975 1	,109 1,	1,057 2,	2,307 3,3	3,334 4,479	79 4,662	62 4,521	21 5,416	16 7,122	2 8,104	4 8,791		
12	3,616	1,014 1	,043	1,024	1,022	1,042	965	873	915 1	,052 1,	,064 1,0	1,065 2,5	2,985 3,645	45 4,145	45 4,390	90 5,375	75 7,272	2 8,226	5 8,733		
13	3,726		1,026	966	985	970	886	798	862 1	,011 1,	,077 1,0	1,042 1,6	1,607 3,099	99 3,352	52 3,986	86 5,232	32 7,375	5 8,381			
14	3,700		992	951	935	878	818	770	858 1	,027 1,	,152 1,	,245 1,7	1,710 1,652		15 3,262	62 4,931		1 8,621			
15	3,505	933	934	882	868	825	847	757	874	980 1,	,177 1,	,348 1,7	1,791 1,783		1,865 3,161	61 4,272	72 6,831	1 8,590	9,032		
16	3,084	863	848	787	778	740	797	690	816	892 1,	,047 1,	1,342 1,7	1,738 1,899	99 1,864		1,923 3,805	05 5,880	0 8,092	9,066		
17	2,687		732	667	664	627	676	622	662	733	865 1,	,239 1,6	1,664 1,940		1,862 1,8	1,848 2,104	04 4,388	8 6,810	8,385		
18	2,519	624	588	527	528	485	506	504	632	592	791 1,0	,044 1,4	,415 1,769		1,745 1,7	1,798 1,751	51 1,982	2 4,889	7,020	_	
19	2,040	449	413	367	368	344	360	429	566	601	853	850 1,1	1,173 1,444	44 1,522		,504 1,519	19 1,728	8 1,980	4,758	ľ	
20	1,227	253	228	201	200	236	238	285	386	438	622	595 7	798 9.	939 9	960 9	932 9	993 1,275	5 1,185	11111		LOCATION
MAX STORY SHEAR	5,308	2,579 3	3,362	5,175	7,416	6,994	7,884 1	10,569 1	1,265 14	14,934 9,	9,473 9,	9,294 8,2	8,201 7,834	34 8,648	48 8,304	04 8,818	18 10,514	4 13,070	14,918	2,579	-

Table A2.13 Story shears after ontimization for EO1 data

בעב uala 1 able A2.14 Story snears after optimization for

		18 19	1,704 1,421	6,834 7,673	6,972 7,862	6,519 7,408	6,301 7,217	6,034 6,980	5,725 6,700	5,378 6,377	5,009 6,018	4,629 5,627	4,278 5,219	4,047 4,927	3,909 4,695	3,751 4,436	3,548 4,135	3,286 3,770	2,967 3,338	2,579 2,840	2,209 2,451	1,196 2,120	
		17	7 1,961	0 5,984	0 6,072	7 5,638	5 5,408	4 5,140	1 4,847	3 4,537	5 4,236	5 3,991	9 3,833	5 3,708	2 3,564	1 3,377	5 3,141	0 2,847	3 2,501	8 2,286	2 1,440	5 937	
		16	9 2,177	5 5,230	4,	2 4,877	2 4,665	7 4,434	3 4,191	2 3,953	1 3,755	1 3,596	3 3,439	3 3,265	4 3,062	0 2,821	0 2,545	0 2,390	8 2,513	3 1,748	2 1,352	9 946	
		15	9 2,199	3 4,505	8 4,538	7 4,182	8 4,002	7 3,817	3 3,643	8 3,482	1 3,321	4 3,141	2 2,933	0 2,693	0 2,424	9 2,210	0 2,180	7 2,480	1 1,918	2 1,653	6 1,342	5 959	
		14	34 2,135	6 4,453	1 4,498	60 4,157	37978	2 3,787	12 3,583	52 3,378	5 3,191	5 3,014	1 2,832	4 2,620	4 2,460	3 2,309	9 2,410	1 1,947	1,731	1,462	5 1,146	0 805	
		13	40 1,984	00 4,236	25 4,271	50 3,950	16 3,787	36 3,612	56 3,432	51 3,252	53 3,095	30 2,955	33 2,811	03 2,644	00 2,454	17 2,283	03 1,809	55 1,621	33 1,502	87 1,333	51 1,115	596 830	
		12	,269 1,840	57 3,500	81 3,525	47 3,250	56 3,116	81 2,986	2,668 2,866	94 2,761	,983 2,653	,693 2,530	,490 2,383	,557 2,203	1,139 2,100	,024 1,717	910 1,603	788 1,465	705 1,293	609 1,087	498 851	376 59	
	R LEVE	11	,261 1,2	3,400 3,757	3,430 3,781	3,150 3,447	2,972 3,256	2,751 2,981	2,578 2,6	2,345 2,294	2,031 1,9	,642 1,6	,596 1,4	,194 1,5	,116 1,1	,020 1,0	911 9	823 7	760 7	682 6	579 4	438 3	
	ISOLATOR LEVEL	10	,249 1,2	2,638 3,4	2,597 3,4	2,348 3,1	2,306 2,5	2,220 2,7	2,088 2,5	,909 2,3	,690 2,0	,522 1,6	1,185 1,5	1,128 1,1	,063 1,1	989 1,0	6 116	827 8	734 7	628 6	511 5	381 4	
Ŧ		8 9	,198 1,	,800 2,0	2,686 2,	309 2,	2,051 2,3	,947 2.;	,795 2,0	,593 1,6	1,468 1,	1,126 1.	,054 1,	982 1,	906 1,0		743	665	585	504	408	290	
STORY SHEAR[tf]		7 8	,392 1,	,305 2,	2,347 2,	2,162 2,	2,016 2,	,812 1,	,551 1,	,589 1,	,305 1,	,217 1,	,127 1,	,035	943		754	655	554	448	340	238	
STORY		9	,511 1	,773 2	,790 2	,607 2	,580 2	,532 1	,716 1	,432 1	,351 1	,268 1	,182 1	,092 1	,000	903	804	700	592	479	363	249	
		5	1,685 1	1,748 1	1,755 1	1,712 1	1,703 1	1,925 1	1,599	l,514 I	1,430 1	1,345 1	1,256 1	1,164	1,068 1	967	863	753	637	517	395	270	
		4	1,856	1,884	2,011	1,871	2,229	1,758	1,661	1,564	1,466	1,366	1,266	1,163	1,071	866	914	817	708	585	452	307	
		3	1,985	2,002	1,996	2,398	1,889	1,794	1,699	1,605	1,510	1,412	1,312	1,237	1,171	1,093	1,002	896	776	641	495	336	
		2	2,210	2,218	2,828	2,109	2,006	1,901	1,814	1,734	1,653	1,567	1,474	1,375	1,273	1,194	1,099	987	858	711	550	373	
		-	2,428	2,907	2,338	2,247	2,154	2,058	1,959	1,856	1,750	1,674	1,595	1,509	1,415	1,321	1,221	1,100	959	798	619	422	
	EARTHQUAKE DATA: EQ 2	UNCONTROLLED BUILDING		6,401	6,335	6,247	6,132	5,989	5,817	5,615	5,383	5,120	4,826	4,505	4,161	3,788	3,398	2,983	2,548	2,087	1,608	1,100	
	EARTHQU	STORY	ISOLATOR FLOOR	-	2	3	4	5	9	7	8	6	10	=	12	13	14	15	16	17	18	19	

		19	83 2,000	73 8,800	47 8,994			87 7,647			Ĩ			_		89 6,292		92 5,836		01 4,456	3,932 3,486	,998 3,074	1,075 1,139 LOCATION	
		18	0 2,88	0 10,172	Ξ	_	4 9,815	5 9,487	7 9,053	_	2 7,903	7 7,196	8 6,459	0 6,050	5,834	- 1	3 5,932	3 5,592		9 4,001		-	_	
		17	8 3,98(1 11,990	5 12,501	4 11,984	8 11,814	4 11,495	0 11,027	3 10,424	4 9,712	3 8,967	9 8,288	5 7,600	4 6,785	3 5,762	6 5,183	7 4,643	3 4,156	3 5,539	0 2,943	0 1,884	1 1,178	
		16	5 4,648	3 14,40	5 14,975	2 14,274	2 13,978	8 13,514	0 12,930	4 12,263	1 11,554	1 10,803	1 9,915	8,825	1 7,494	3 5,893	3 4,676	3,897	3 6,863	5 3,653	3 2,790	9 2,430	2 1,64	
		15	4,066	16,663	16,856		15,252	14,868	14,430	13,884	13,151	12,151	10,864	9,348	7,871		4,133	6,795	3,453	1 3,025			1,622	
		14	3,290	17,106	17,612		16,140	15,502	14,716	13,838	12,889	11,828	10,596	9,145	7,459		6,641	3,503	4,463	5,124	5,239		2,949	
		13	2,525	20,103	20,704	19,426	18,749	17,839	16,686	15,381	13,902	12,132	10,143	8,301	6,374	6,408	3,217	4,703	5,882	6,351	5,982	5,132	3,291	
		12	2,883	21,461	22,064	20,783	20,137	19,192	17,934	16,331	14,400	12,155	9,633	6,858	5,918	2,164	2,270	2,840	3,299	3,664	3,556	2,882	1,861	
	JEVEL.	Ξ	2,285	18,293	18,329	16,666	15,690	14,358	12,897	11,172	9,211	6,979	4,778	3,861	1,651	1,838	2,036	2,147	2,165	2,079	1,853	1,453	903	
L UOT 1	ISULATOR LEVEL	10	2,457	15,929	16,141	14,855	14,016	12,892	11,463	9,704	7,618	5,172	3,857	2,006	1,598	1,695	1,887	2,020	2,018	1,866	1,570	1,152	689	
Car	2	6	2,325	17,566	17,706	16,065	14,974	13,262	11,250	8,814	6,084	4,217	2,240	2,252	2,252	2,176	1,986	1,674	1,652	1,610	1,421	1,068	674	
AR(tf)		8	2,121	10,372	9,756	8,177	7,210	5,971	4,656	3,413	2,996	1,967	2,035	2,122	2,167	2,146	2,046	1,866	1,626	1,359	1,067	730	395	
STORY SHEAR[tf]		7	1,978	8,409	7,998	6,707	6,024	5,187	4,126	2,823	1,930	1,875	1,804	1,723	1,643	1,567	1,441	1,263	1,050	891	714	533	328	
STC		9	1,893	779,T	7,486	6,414	5,461	4,193	2,892	1,897	1,881	1,857	1,811	1,729	1,611	1,460	1,292	1,116	943	775	695	559	345	
		5	1,893	6,699	6,057	4,670	3,651	2,668	1,890	1,909	1,896	1,848	1,770	1,670	1,551	1,413	1,271	1,126	696	161	713	563	338	
		4	1,962	4,853	4,098	3,035	2,756	1,901	1,935	1,953	1,941	1,895	1,819	1,721	1,612	1,498	1,373	1,225	1,055	865	663	545	360	•
		3	1,991	3,847	2,974	2,690	1,904	1,900	1,906	1,900	1,871	1,816	1,742	1,662	1,582	1,496	1,391	1,258	1,094	905	669	570	367	•
		2	1,981	2,731	2,781	1,903	1,839	1,806	1,779	1,740	1,681	1,606	1,525	1,454	1,397	1,339	1,261	1,154	1,014	846	656	495	312	
		-	1,970	2,560	1,870	1,793	1,737	1,697	1,658	1,606	1,534	1,438	1,319	1,228	1,188	1,152	1,099	1,019	908	766	600	445	275	
	UANE DATA: EQ 3	UNCONTROLLED BUILDING		8,674	8,652	8,639	8,552	8,311	7,863	7,180	6,293	5,834	5,467	5,176	5,135	5,126	5,491	5,843	5,886	5,591	4,917	3,778	2,193	
EA DTHOI	EAKIHU	STORY	ISOLATOR FLOOR	_	2	3	4	5	9	7	8	6	10	=	12	13	14	15	16	17	18	19	20	

Table A2.15 Story shears after optimization for EQ3 data

Table A2.16 Story shears after optimization for EQ4 data

							STC	STORY SHEAR[tf]	ur (ef)													
EARTHQ	EARTHQUAKE DATA: EQ 4									ISOL	ISOLATOR LEVEL	EVEL										
STORY	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	II	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		2,120	1,987	1,884	1,794	1,707	1,620	1,536	1,517	1,888	1,775	1,912	2,620	3,059	3,230	3,231	3,302	3,444	3,172	2,449		
_	6,970	2,621	2,396	2,855	3,871	5,486	6,356	7,108	7,556	8,705	10,006	10,656	8,990	8,298	9,085	10,219	10,859	11,007	1,204	1,079		
2	6,882	1,981	2,652	2,410	3,271	4,925	5,838	6,696	7,267	8,675	10,106	10,915	9,244	8,089	8,858	9,993	10,724	0,913	1,163	1,003		
3	6,768	1,853	1,844	2,408	2,588	3,716	4,667	5,552	6,272	7,734	9,232	10,098	8,657	7,668	7,823	8,912	9,617	9,875	0,118	9,980		
4	6,628	1,736	1,708	1,729	2,429	2,843	3,741	4,740	5,630	7,155	8,575	9,589	8,310	7,504	7,816	8,273	8,974	9,280	9,545	9,391		
5	6,463	1,638	1,592	1,591	1,649	2,264	2,870	3,679	4,984	6,623	7,703	8,802	7,821	7,259	1,771	7,773	8,363	8,673	8,923	8,714		
9	6,272	1,556	1,499	1,477	1,531	1,588	2,268	2,924	4,226	5,881	6,756	7,854	7,170	7,115	7,561	7,907	7,903	8,149	8,327	8,043		
7	6,051	1,487	1,425	1,396	1,439	1,490	1,512	2,322	3,319	4,938	5,876	6,701	6,496	6,865	7,262	7,810	7,821	7,795	7,797	7,417		
8	5,800	1,426	1,362	1,333	1,365	1,405	1,413	1,435	2,581	3,771	4,808	5,351	5,934	6,513	6,913	7,578	7,828	7,509	7,405	7,026		
6	5,521	1,370	1,305	1,276	1,299	1,324	1,320	1,346	1,428	2,845	3,631	4,436	5,263	6,018	6,672	7,218	7,701	7,635	7,168	6,784		
10	5,212	1,313	1,247	1,219	1,235	1,242	1,227	1,264	1,364	1,748	2,860	3,374	4,451	5,372	6,250	7,013	7,338	7,589	7,411	6,847		
П	4,874	1,252	1,185	1,159	1,169	1,158	1,135	1,186	1,297	1,638	1,606	3,004	3,486	4,575	5,664	6,623	7,105	7,276	7,413	7,131		
12	4,511	1,182	1,117	1,093	1,097	1,072	1,048	1,110	1,221	1,509	1,515	1,724	3,797	4,019	4,872	6,040	6,710	6,769	7,190	7,165		
13	4,117	1,101	1,039	1,021	1,021	984	965	1,033	1,129	1,342	1,437	1,565	2,289	4,268	4,222	5,200	6,096	6,345	6,701	6,953		
14	3,702	1,009	953	942	940	668	881	944	1,014	1,131	1,326	1,412	1,996	2,708	4,608	4,186	5,270	5,799	6,077	6,489		
15	3,612	902	855	854	852	814	800	836	950	1,001	1,191	1,271	1,731	2,461	2,941	4,842	4,184	4,994	5,538	5,956		
16	3,436	780	744	754	753	722	720	732	922	902	1,041	1,120	1,505	2,253	2,729	2,967	5,057	4,386	5,087	5,546		
17	3,183	645	622	640	641	616	623	637	832	826	886	949	1,274	1,997	2,464	2,653	2,816	5,108	4,649	4,935		
18	2,826	499	487	510	514	493	498	516	670	712	713	922	1,109	1,706	2,095	2,212	2,291	2,678	4,832	4,398		
19	2,222	340	337	359	365	349	346	358	442	732	737	970	1,078	1,398	1,696	1,626	1,666	2,082	2,342	3,905	l	
20	1,320	183	185	200	205	196	188	184	252	518	510	665	750	914	1,125	1,038	967	1,365	1,357	1,230	Iζ	LOCATION
MAX STORY SHEAR	6 970	2.621	2.652	2 855	3 871	5 486	6 356	7 100	7 556	0 705	10106	10.015	10,044	0.000	2000	10,10	020 01	2001		0101		-

							STC	STORY SHEAR[tf]	AR(tf)													
EARTHQ	EARTHQUAKE DATA: EQ 5									ISOL	ISOLATOR LEVEL	EVEL										
STORY	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,423	1,453	1,477	1,494	1,507	1,495	1,515	1,762	2,026	1,925	2,043	2,236	2,619	2,936	3,283	3,646	3,589	3,162	2,675		
1	8,082	2,233	3,485	5,313	8,078	9,888	16,026	18,405	21,148	18,076	19,301	19,268	13,859	15,964	14,801	14,598	19,012	18,154	14,774	17,095		
2	8,088	1,375		3,709	6,573	8,920	15,153	17,756	21,106	18,892	19,724	19,862	13,618	15,572	14,473	14,320	18,576	18,452	14,509	17,010		
3	7,861	1,336	1,379		4,105	6,744	12,483	15,023	18,884	17,891	18,390	18,579	12,769	13,766	12,762	12,962	16,016	16,933	12,741	15,192		
4	7,356	1,296			2,703	5,002	10,028	12,941	17,171	17,311	17,549	17,814	12,662	12,757	12,154	11,936	14,185	15,618	12,222	14,461		
5	6,962	1,248	1,253	1,362	1,464	2,984	6,926	10,050	14,834	16,031	16,427	16,726	12,208	11,797	11,397	10,611	11,816	13,838	11,130	13,628		
6	6,351	1,187	1,196		1,418	1,491	3,655	7,188	12,031	14,236	14,920	15,340	11,412	11,195	10,474	9,278	9,586	11,728	10,034	12,504		
7	5,563	1,108	1,148		1,376	1,460	1,500	3,924	8,616	11,695	12,941	13,772	10,311	10,778	10,173	8,469	7,921	9,667	9,410	10,995		
8	5,479	1,014	1,107	1,214	1,333	1,431	1,481	1,518	4,784	8,494	10,428	11,923	9,315	10,590	10,424	8,719	6,546	7,884	8,565	9,477		
6	6,089	971	1,072	1,177	1,287	1,395	1,459	1,493	1,733	4,483	7,418	9,480	8,588	10,230	10,406	9,295	6,970	6,832	7,695	8,553		
10	6,445	941	1,042	1,144	1,244	1,347	1,425	1,457	1,676	1,894	4,428	6,505	7,464	9,371	10,080	9,639	8,399	7,501	7,524	7,685		
Π	6,503	913	1,014	1,112	1,203	1,291	1,373	1,406	1,598	1,774	1,929	4,503	5,815	7,950	9,237	9,595	9,302	8,486	8,528	8,653		
12	6,239	882	982	1,076	1,158	1,225	1,299	1,333	1,477	1,748	1,997	1,869	4,566	6,069	7,777	9,048	9,556	9,641	9,141	9,654		
13	6,134	844	941	1,030	1,103	1,144	1,203	1,232	1,310	1,753	1,957	1,718	2,075	5,122	5,726	7,770	9,401	10,084	9,329	10,198		
14	5,931	161	885	970	1,034	1,047	1,096	1,109	1,113	1,590	1,795	1,573	2,090	2,666	5,424	5,909	8,622	9,765	9,082	10,301		
15	5,518	719	808		945	950	1,000	983	1,034	1,291	1,476	1,411	2,138	2,752	2,639	5,303	6,946	8,725	8,380	9,976		
16	4,802	625	706	778	827	847	896	849	955	1,146	1,192	1,211	2,184	2,976	2,662	2,626	5,293	7,026	7,223	9,175		
17	3,835	512	582	644	681	726	771	734	848	166	1,270	983	2,177	3,209	2,705	2,448	2,879	4,865	5,674	7,834		
18	3,162	429	443	491	515	583	619	709	838	873	1,413	950	2,239	3,189	2,775	2,475	2,961	2,640	4,372	6,077		
19	2,865	383	376	381	437	477	530	667	738	1,064	1,486	924	1,908	2,696	2,719	2,276	2,766	2,458	2,133	4,000	l	
20	1,978	254	252	267	310	326	357	464	533	748	947	624	1,238	1,774	1,858	1,536	1,705	1,924	1,287	1,262	Г	LOCATION
MAX STORY SHEAR	8,088	2,233	3,485	5,313	8,078	9,888	16,026	18,405	21,148	18,892	19,724	19,862	13,859	15,964	14,801	14,598	19,012	18,452	14,774	17,095	2,233	1

Table A2.17 Story shears after optimization for EQ5 data

Table A2.18 Story shears after optimization for EQ6 data

							STO	STORY SHEAR[tf]	RIff													
EARTHQ	EARTHQUAKE DATA: EQ 6									VIOSI	ISOLATOR LEVEL	VEL										
STORY	UNCONTROLLED BUILDING	1	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,404	1,362	1,278	1,193	1,195	1,164	1,183	1,472	1,508	1,345	1,287	1,930	2,090	2,635	2,570	2,743	2,372	2,138	1,616		
-	5,962	1,579	1,957	3,477	5,263	6,669	8,497	11,323	13,851	14,871 1	3,095	10,283	7,887	9,514	9,452	6,756	7,394	8,744	9,952 1	0,682		
2	5,848	1,339	1,716	2,448	4,244	5,922	7,787	10,925	13,676	15,143 1	3,510	10,859	8,344	9,585	9,592	6,918	7,299	8,695 10	0,040 1	0,985		
3	5,703	1,277	1,307	1,595	2,669	4,321	6,179	9,232	12,252	13,841 1	12,691	10,409	8,262	8,799	8,883	6,487	6,533	7,752	9,163 1	0,250		
4	5,527	1,216	1,258	1,257	1,690	3,028	4,833	7,965	11,062	12,965 1	2,118	10,167	8,247	8,389	8,475	6,277	6,034	7,167 \$	8,649	9,865		
5	5,320	1,156	1,216	1,246	1,204	1,666	3,228	6,132	9,481	11,958 1	1,227	9,686	8,023	7,875	7,970	6,019	5,655	5,404	070,7	9,307		
9	5,085	1,100	1,181	1,241	1,209	1,129	1,857	4,298	7,562	10,532 1	0,017	8,943	7,585	7,312	7,381	5,825	5,382	5,768	7,199	8,639		
7	4,822	1,047	1,150	1,233	1,209	1,117	1,086	2,222	5,232	8,532	8,481	7,936	6,922	6,681	6,721	5,718	5,081	5,034	6,198	7,697		
8	4,535	995	1,118	1,217	1,200	1,113	1,035	1,114	2,707	6,047	6,661	6,708	6,057	5,982	6,121	5,508	4,753	4,246	5,177	6,604		
6	4,554	941	1,079	1,188	1,181	1,106	1,015	1,053	1,367	3,119	4,593	5,271	5,064	5,214	5,533	5,169	4,411	3,811 4	4,760	5,344		
10	4,599	881	1,031	1,144	1,152	1,093	1,011	1,000	1,279	1,405	3,045	3,729	4,021	4,387	4,806	4,690	4,166	3,917	4,644	5,207		
11	4,600	817	970	1,086	1,112	1,071	1,001	955	1,213	1,339	1,386	2,587	3,164	3,572	3,936	4,073	4,083	4,062	4,544	5,196		
12	4,530	782	917	1,016	1,062	1,038	979	915	1,165	1,287	1,422	1,175	2,986	2,920	3,327	3,617	4,171	4,405	4,655	5,121		
13	4,369	754	880	978	1,011	994	942	871	1,121	1,223	1,425	1,270	1,865	3,680	2,718	3,182	4,098	4,534	4,940	5,184		
14	4,105	710	832	940	964	937	889	815	1,061	1,130	1,381	1,350	2,228	2,498	4,054	2,696	3,784	4,407	5,125	5,503		
15	3,731	657	171	886	868	864	819	741	975	1,005	1,283	1,382	2,488	3,020	2,632	3,542	3,158	3,976	4,970	5,485		
16	3,265	598	693	810	810	771	729	649	857	856	1,133	1,320	2,595	3,337	2,762	2,221	3,319	3,244	4,507	5,197		
17	2,763	523	596	706	698	656	620	540	711	704	937	1,163	2,523	3,368	2,822	2,172	2,045	2,955	3,669	4,557		
18	2,275	432	480	574	561	527	511	423	602	607	789	939	2,247	3,057	2,718	2,048	1,634	1,822	2,816	3,638		
19	1,944	318	347	409	396	379	372	332	454	575	712	695	1,739	2,385	2,283	1,723	1,457	1,579	1,473	2,732	l	
20	1,337	189	202	229	221	216	217	223	336	417	483	467	1,110	1,441	1,472	1,120	976	1,125	1,048	873	2	LOCATION
MAX STORY SHEAR	5,962	1,579	1,957	3,477	5,263	6,669	8,497	11,323	13,851	15,143 1	13,510	0,859	8,344	9,585	9,592	6,918	7,394	8,744 10	0,040 1	10,985 1	1,579	1

							STORY	STORY SHEAR[tf]	5												
EARTHQUAKE DATA: EQ 7	_									ISOLATO	ISOLATOR LEVEL										
UNCONTROLLED BUILDING	DNIC	1	2 3	4	5	9	7	8	9	10	11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR	-	,122 1	,060 1,0	,020 9	967 9.	937 9	929 9	933 1,(088 1,	,416 1,33	37 1,335	5 1,89	1 2,063	2,437	2,394	2,679	2,563	1,972	1,413		
5,	5,039 1	,417 1		2,551 4,1	,163 5,0	,010 5,4	,410 5,8	,881 6,0	,068 7,	,511 8,2	;,274 7,043	3 6,591	1 7,630	7,382	7,320	6;099	6,695	8,293	8,814		
5,	5,005 1	,055 1.	_	,979 3,6	,666 4,7	,713 5,4	,438 5,9	5,904 5,9	,966 7,	,404 8,414	14 7,140	0 6,724	æ	7,554	7,457	6,193	6,711	8,312	8,894		
4,	4,943	995 1	-	504 2,6	2,610 3,8	,824 4,7	,795 5,3	,303 5,3	,353 6,	5,488 7,6	,674 6,447	7 6,210	0 7,801	7,065	6,916	5,740	6,128	7,448	8,069		
4,	4,792	942	972	981 1,6	,679 2,947	4	,143 4,8	1,873 4,8	1,866 5,	5,850 7,0	,072 5,990	0 5,888	8 7,709	6,866	6,610	5,560	5,776	6,784	7,494		
4,	4,532	895	•	944 9	922 1,7	m	,181 4,1	1,140 4,2	,249 4,	1,964 6,3	6,345 5,473	3 5,462		6,846	6,381	5,302	5,363	5,995	6,753		
4,	4,252	855		908 8	884 8	894 1,9	,941 3,1	3,180 3,5	3,562 4;	4,281 5,6	5,659 4,874	4 4,958	8 7,143	6,802	6,027	5,043	5,177	5,283	6,027		
4,	4,016	835	870 8	872 8	845 8	865 8	880 1,9	.961 2,7	2,780 3,	,584 4,8	1,898 4,238	8 4,404	4 6,680	6,654	5,649	4,931	5,036	5,169	5,537		
.э,	3,981	823			803 8	831 8	850 8	875 1,9	925 2,	2,779 3,9	,910 3,641	1 4,031	1 6,132	6,384	5,424	4,836	4,949	5,101	5,264		
3,	3,856	805		791 7	759 7	796 8	822 8	832 9	992 2,	2,323 2,701	01 3,078	8 3,613	3 5,537	6,015	5,387	4,859	4,890	5,192	4,991		
ι, Έ	3,827	780		745 7					924 1,	,324 2,436	36 2,356	6 3,076	6 4,880	5,552	5,213	4,845	4,727	5,140	5,090		
3,	3,744	747		695 6	661 7.	721 7	747 7	741 8	859 1,	,245 1,2	,230 2,159	9 2,433	3 4,092	4,990	4,899	4,783	4,621	4,936	5,225		
3,	3,529	707		640 6	628 6	683 7	700 6	689 8	807 1,	,160 1,1	,176 1,180	0 2,536	6 3,224	4,305	4,463	4,648	4,469	4,644	5,236		
ι, Υ	3,166	629						633 7	796 1,	,058 1,2	,219 1,113	3 1,689	9 3,418	3,481	3,905	4,401	4,372	4,461	5,174		
2,	2,789	602		531 5	558 6	601 5	593 5	585	160	967 1,1	,173 1,088	8 1,619	9 2,012	3,789	3,360	4,012	4,129	4,630	5,049		
2,	2,476	544		476 5	509 5	549 5	540 5	538 (664	847 1,0	,032 1,017	7 1,566	6 2,153	2,525	3,215	3,469	3,690	4,485	4,839		
2,	2,186	487	457 4	414 4	450 4	486 4	475 4	491 5	545	726 8	835 909	9 1,585		2,526	2,200	3,712	3,163	4,033	4,726		
1,	1,937	418	389	375 3	381 4	411 3	399 4	442	522	684 6	699 781	1 1,607	7 2,439	2,369	2,033	2,362	3,764	3,229	4,229		
1,	,757	336	309	320 3	303 3.	334 3	381 4	408 5	515	746 7	722 638	8 1,433	3 2,253	2,013	1,695	2,044	2,119	3,166	3,397		
1,	1,417	239	231	240 2	226 2	279 3	351 3	389 4	473	728 7	790 582	2 1,051	1 1,756	1,482	1,190	1,581	1,712	1,496	2,374	l	
	869	137	139	143 I	147 1	183 2	230 2	262 3	328	494 5	520 378	8 627	7 1,014	856	170	940	1,083	863	715	Т	LOCATION
MAX STORY SHEAR 5.	5.039 1	417 1	732 2.	2.551 41	163 5 010		5 438 5 9	5 004 61	6 068 7	511 8 414	14 7 7 140	ACT 2 0	0 041	7 554	L3V L	6 102	112 2	0 212	0.004		-

Table A2.19 Story shears after optimization for EQ7 data

Table A2.20 Story shears after optimization for EQ8 data

							STO	STORY SHEAR[tf]	AR [tf]													
EARTHQ	EARTHQUAKE DATA: EQ 8									TOSI	ISOLATOR LEVEL	CVEL										
STORY	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,395	1,333	1,260	1,198	1,145	1,097	1,022	1,045	1,109	1,097	1,071	1,585	1,598	1,817	1,704	2,046	2,067	1,863	1,583		
1	6,398	1,640	1,305	1,583	2,396	2,548	2,954	3,434	3,921	4,085	4,051	3,893	4,918	4,786	4,928	5,024	5,082	6,296	6,830	7,532		
2	6,311	1,325		1,292	2,109	2,459	2,834	3,436	3,937	4,139	4,082	3,827	4,859	4,813	4,958	5,131	5,110	6,398	6,913	7,717		
3	6,228	1,255	1,259	1,523	1,499	2,006	2,359	3,023	3,550	3,748	3,705	3,427	4,293	4,386	4,497	4,752	4,680	5,930	6,442	7,261		
4	6,117	1,184	1,186	1,185	1,496	1,564	1,886	2,680	3,223	3,468	3,415	3,205	3,867	4,100	4,176	4,514	4,433	5,684	6,174	7,037		
5	5,970	1,139	1,136	1,123	1,117	1,385	1,506	2,154	2,774	3,037	3,040	2,994	3,380	3,742	3,790	4,209	4,220	5,382	5,881	6,731		
9	5,788	1,106	1,100	1,075	1,053	1,058	1,364	1,719	2,195	2,547	2,597	2,826	3,076	3,352	3,444	3,840	3,992	5,055	5,531	6,354		
7	5,569	1,070	1,061	1,027	7997	978	994	1,337	1,768	1,975	2,299	2,650	2,967	2,959	3,089	3,439	3,705	4,690	5,140	5,865		
8	5,314	1,029	1,018	979	945	915	006	925	1,435	1,624	2,067	2,405	2,840	2,703	2,738	3,028	3,441	4,312	4,712	5,362		
6	5,028	981	969	929	892	864	850	835	666	1,504	1,747	2,045	2,639	2,629	2,656	2,764	3,252	3,930	4,368	4,898		
10	4,724	928	914		838	816	810	785	950	1,027	1,498	1,617	2,332	2,539	2,602	2,798	3,156	3,689	4,142	4,826		
Π	4,410	868	854	817	782	764	766	744	898	968	1,008	1,458	1,960	2,347	2,530	2,802	3,131	3,538	4,074	4,797		
12	4,084	802	789	755	724	709	719	706	842	911	978	966	2,041	2,044	2,382	2,730	3,058	3,432	3,956	4,725		
13	3,746	729	718	689	663	654	668	663	<i>6LL</i>	851	938	933	1,378	2,007	2,124	2,549	2,923	3,342	3,840	4,624		
14	3,396	652	644	620	598	593	611	612	710	784	886	867	1,201	1,449	2,252	2,265	2,724	3,182	3,710	4,411		
15	3,013	568	564	547	530	526	547	552	633	719	820	782	1,135	1,341	1,673	2,171	2,459	2,942	3,517	4,084		
16	2,595	480	480	469	457	454	474	485	549	684	743	706	1,022	1,238	1,580	1,588	2,570	2,623	3,242	3,641		
17	2,141	388	392	385	378	375	391	414	464	630	652	613	884	1,147	1,416	1,459	1,866	2,507	2,867	3,087		
18	1,665	297	301	298	292	290	313	329	366	540	540	495	718	1,041	1,192	1,262	1,629	1,741	2,508	2,513		
19	1,155	206	204	203	199	202	232	244	322	405	515	407	561	826	888	975	1,255	1,332	1,309	2,101	l	
20	637	125	114	III	109	112	137	155	218	273	357	271	357	527	568	587	745	776	692	839	З	LOCATION
MAX STORY SHEAR	6,398	1,640	1,684	1.583	2,396	2,548	2,954	3,436	3,937	4,139	4,082	3,893	4,918	4,813	4,958	5,131	5,110	6,398	6,913	7,717 1.	1,583	e
																				ł		

		-					STO	STORY SHEAR[tf]	Rltf													
EARTHQUA	EARTHQUAKE DATA: EQ 9									ISOLAT	ISOLATOR LEVEI	EL										
STORY UI	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	9		11	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,730	1,762	-	1,798	1,779	1,738	1,695	1,780 2	2,043 1	1,714 1	1,795 1	1,888 2	2,096	2,124	2,181 2	2,309	2,419	2,363	2,333		
1	5,134	2,034	1,519	1,797	2,403	3,002	3,730	4,522	4,884 5	5,139 5	5,437 6	6,125 6	6,092	5,452	5,443	5,267 5	5,232 (6,046	7,004	8,225		
2	5,198		2,206	_	1,942	2,628	3,391	4,278	4,727 5			Ĩ		5,451	5,437		5,209 (6,059	6,983	8,331		
3	5,230			~	1,539	1,924	2,670	3,573	1	~	4,883 5		-	5,018		7	4,755	5,540	6,342	7,868		
4	5,203			-	2,074	1,595	2,116	3,157	3,884 4	4,325 4	4,552 5	5,402 5	5,470 4			4,771 4	4,497	5,244	6,012	7,795		
5	5,111				1,736	2,015	1,644	2,592			4,145 5			4,526	4,445	4,583 4	4,269 4	4,902	5,675	7,705		
9	4,955	1,740			1,671	1,704	2,009	1,961		3,204 3	3,837 4	4,583 4	4,809 4			4,375 4	4,245	4,535	5,325	7,597		
7	4,748	1,715	5 1,675	1,624	1,600	1,624	1,657	1,984		2,669 3		4,085 4	4,384 2		3,927		4,199 4	4,255	5,162	7,458		
8	4,504		-	1,565	1,522	1,538	1,572	1,613	2,172 2		2,987 3	_				4,013 4	4,118 4	4,214	5,106	7,290		
6	4,230	1,625	-	1,495	1,438	1,445	1,482	1,528		2,516 2	2,472 2		3,322 3				4,006 4	4,189	5,065	7,087		
10	3,930	1,559	-	1,414	1,347	1,346	1,386	1,435			2,218 2	2,452 2	2,898 3					4,123	5,035	6,862		
П	3,612		-	1,324	1,249	1,241	1,284	1,335	1,445 1		1,659 2	2,305 2	2,444	3,288	3,731	3,770 3	3,827	4,009	4,978	6,636		
12	3,298	1,381	-	1,223	1,145	1,131	1,177	1,230	1,332 1	1,584 1	1,601 1	1,602 2	2,704	2,865	3,433	3,583 3	3,727	3,847	4,869	6,419		
13	3,014		-	1,113	1,035	1,016	1,063	1,118		[1,521 1	1,507 1			3,010	3,303 3	3,562	3,623	4,681	6,173		
14	2,759		-	995	920	868	946	1,000	1,093 1	1,302 1	1,406 1	1,415 1	1,752			2,915 3	3,324	3,320	4,398	5,859		
15	2,499	1,005		867	799	775	825	873	960 1	,119 1	1,252 1	1,290 1		1,781	1,916	2,896 3	3,009	2,967	4,014	5,452		
16	2,221	853		732	673	710	700	738	817	924 1	1,057 1	1,116 1	1,698	1,926	2,012		3,067	2,723	3,523	4,935		
17	1,925	689		591	566	644	599	597	999	764	829	903 1	1,575 2			1,719 1	1,802	3,280	3,099	4,307		
18	1,606	550) 484	447	477	538	494	483	510	631	603	687 1	1,493	1,917	1,954	1,619 1	1,579	2,077	3,428	3,764		
19	1,245	437	7 368	321	348	390	360	348	361		478	583 1	1,239	1,552	1,575	1,298 1	1,329	1,622	1,840	3,415	ļ	
20	742	268	742 268 228	194	202	218	214	204			326			954			870	994	1,133	1,215	Ţ	LOCATION
MAX STORY SHEAR	5,230	2,034	1 2,206	2,116	2,403	3,002	3,730	4,522	4,884 5	5,165 5		6,192 6	6,173 5	•	5,443	5,324 5	5,232 (6,059	7,004	8,331 2	2,034	-

Table A2.21 Story shears after optimization for EQ9 data

Table A2.22 Story shears after optimization for EQ10 data

							STC	STORY SHEAR[tf]	LR [tf]													
EARTHQU	EARTHQUAKE DATA: EQ 10									ISOL	ISOLATOR LEVEL	CVEL										
STORY	UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	Π	12	13	14	15	16	17	18	19		
ISOLATOR FLOOR		1,740	1,528	1,330	1,188	1,158	1,149	1,139	1,301	1,301	1,233	1,203	1,718	2,399	3,068	3,270	3,331	3,069	2,490	1,915		
-	6,883	2,033	1,635	2,873	4,208	5,650	8,489	9,115	9,660	8,836	9,784	8,745	7,544	8,842	8,900	10,251	10,638	10,547	9,238	9,806		
2	6,819	1,648	1,934	2,101	3,466	5,059	8,057	8,981	9,720	9,186	9,713	8,894	7,617	8,962	9,038	10,168	10,684	10,786	9,473	10,081		
3	6,726	1,563	1,463		2,259	3,754	6,664	7,780	8,774	8,580	8,735	8,198	7,045	8,246	8,418	9,059	9,666	9,976	8,857	9,379		
4	6,602	1,476	1,400	1,281	1,497	2,767	5,373	6,834	7,960	8,139	8,052	7,813	6,725	7,832	8,077	8,308	8,969	9,427	8,550	8,936		
5	6,443	1,384	1,339	1,230	1,134	1,561	3,746	5,399	6,863	7,386	7,189	7,285	6,326	7,277	7,637	7,349	8,068	8,722	8,103	8,302		
9	6,252	1,291	1,275	1,179	1,082	1,096	1,902	3,850	5,505	6,409	6,205	6,699	5,855	6,665	7,100	6,363	7,107	7,906	7,584	7,693		
7	6,027	1,196	1,207	1,126	1,029	1,036	1,087	1,926	3,867	5,151	5,043	5,914	5,296	6,130	6,523	5,376	6,121	7,001	7,004	7,071		
8	5,769	1,100	1,135	1,071	974	166	1,032	1,112	2,293	3,669	3,899	5,049	4,689	5,539	6,082	4,947	5,362	6,180	6,489	6,407		
6	5,480	1,001	1,061	1,014	916	942	982	1,080	1,232	2,269	2,901	4,106	4,134	4,901	5,499	4,803	5,406	5,796	6,136	5,886		
10	5,159	902	984	954	868	890	933	1,042	1,168	1,244	2,234	3,071	3,477	4,322	4,752	5,094	5,711	5,803	5,982	5,828		
Ξ	4,809	844	904	168	820	834	882	966	1,104	1,188	1,192	2,332	2,757	3,629	4,147	5,245	6,065	6,078	6,003	5,964		
12	4,617	789	821	826	765	774	829	943	1,041	1,123	1,200	1,210	2,970	2,902	3,955	5,202	6,266	6,456	6,142	6,177		
13	4,834	728	736	756	704	710	171	883	970	1,043	1,178	1,220	1,770	3,651	3,516	4,870	6,200	6,686	6,334	6,448		
14	4,922	660	650	682	637	642	706	815	890	1,029	1,093	1,185	1,785	2,403	4,346	4,234	5,792	6,592	6,405	6,651		
15	4,808	586	567	602	564	568	633	737	800	960	956	1,103	2,098	2,408	2,923	4,119	4,983	6,136	6,191	6,668		
16	4,408	519	495	516	484	488	550	646	969	786	806	1,065	2,353	2,369	2,849	2,748	3,945	5,248	5,667	6,361		
17	3,707	493	469	424	397	402	458	541	585	682	744	1,114	2,372	2,471	2,588	2,477	2,572	4,032	4,750	5,705		
18	3,125	435	424	393	333	318	357	423	533	628	795	1,120	2,154	2,374	2,431	2,043	2,046	2,423	3,554	4,724		
19	2,374	336	337	323		259	285	324	428	638	731	1,039	1,725	1,998	1,990	1,645	1,783	1,786	1,760	3,251		
20	1,363	205	213	212	190	157	175	204	301	453	490	692	1,119	1,315	1,189	1,104	1,152	1,203	1,150	1,149	2	LOCATION
MAX STORY SHEAR	6.883	2.033	1.934	2.873		5.650	8.489	9.115	9.720	9.186	9.784	8.894	7.617	8.962	9.038	10.251	10.684	10.786	9.473	10.081	1.934	2
NUCLE INDICIOUS		ccn,2	FCC,1	610,2	'	v.v.	0,407	7,117	7,140	7,100	7,/01	0,071	1.0.1	0,704	000,6	10,401	10,001	10,/00	1	C11.2	10,001	10,001

						STO	STORY SHEAR[tf]	RII												
EARTHQUAKE DATA: EQ 11									10SI	ISOLATOR LEVEL	VEL									
STORY UNCONTROLLED BUILDING	-	2	3	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	
ISOLATOR FLOOR	1,064	1,088	1,118	1,127	1,206	1,359	1,711	2,011	2,291	1,718	1,542	1,909	2,282	2,606	2,450 2	2,698 2	2,843 2	2,818	2,219	
6,498	3,531	6,469	11,931	18,125	18,332	17,007	25,961	22,768 2	23,350	19,012	9,197 1	18,784 1	8,794 1	6,239 1	5,602 17	7,652 24	24,368 30	(4	5,853	
2 6,359	1,007	3,967	9,191	15,880	18,176	16,567	25,371	22,872 2	23,728	19,675	8,289 1	18,562 1	8,491	6,344 1	5,334 17	7,468 23	23,065 30	30,484 20	26,493	
6,305	968	1,050	4,690	11,384	15,213	14,429	22,396	20,662 2	21,660	18,373	15,070 1	5,833 1	6,701 1	4,955 1	3,718 15	15,455 19	9,120 26	26,899 2/	24,653	
6,290	945	1,038	1,088	6,237	11,678	11,969	20,304	19,087 2	20,331	17,393					2,464 14	14,036 16	16,438 24		22,847	
5 6,242	940	1,039	1,087	1,117	6,234	8,525	16,622	16,691	19,540	15,820	12,903 1	1,100 1	12,075 1	2,496 1	1,570 12	12,133 14	14,098 20	20,919 20	20,821	
6,025	940	1,042	1,089	1,120	1,198	4,744	12,305	13,696	18,103	13,754	1,710 1	_	9,984 1	0,443 10	0,443 10	0,184 12	2,319 17	17,673 18	18,758	
7 5,563	935	1,037	1,079	1,113	1,204	1,348	6,632	10,029	15,356	11,462	0,394	9,275		8,869	8,687 9	9,208 10	10,020 14		16,155	
4,982	606	1,012	1,049	1,078	1,185	1,334	1,667	5,436	11,316	10,106	0,100			8,548	7,569 8	8,370 9	9,064 11	1,269 12	12,907	
4,990	865	971	1,000	1,015	1,130	1,285	1,649	1,881	5,963	7,675	9,642				7,403 7	7,665 8	8,513 8		10,613	
0 4,889	810	919		934	1,044	1,205	1,588	1,770	2,031	5,281	7,863	_	-		8,399 7	7,126 7	7,667 8	8,660 10	0,070	
1 4,533	767	878	901	865	945	1,120	1,498	1,673	1,897	1,623		7,452	9,491		8,785 8	8,125 7	7,908 8	8,660 10	10,446	
2 4,334	742	851	863	830	844	1,042	1,405	1,604	1,847	1,813	1,374	4,848		8,971	8,496 8	8,629 8	8,834 9	9,975	9,914	
3 4,157	725	825	821	784	741	950	1,291	1,523	1,837	1,949	1,473		5,530	7,050	7,597 8	8,462 10	10,010 11	1,126 10	899'01	
4 3,701	695	<i>6LL</i>	759	728	683	826	1,111	1,379	1,762	1,925	1,488	1,900		5,389	6,502 7	7,841 10	10,343 12	12,352 12	2,797	
5 3,499	641	703	999	629	617	668	853	1,148	1,529	1,693	1,382	2,085	2,461	2,720	4,974 6	6,376 9	9,544 12	12,458 13	13,737	
6 3,166	560	598	547	574	541	625	649	919	1,182	1,255	1,270				2,352 5	5,296 7			13,599	
7 2,693	458	473	477	477	465	593	709	743	835	827	1,029	2,140		_	.,	2,477 5.	5,586 9	9,022 12	12,037	
18 2,657	378	388	408	399	387	513	676	703	834	861	982	1,904	2,543	2,414	1,980 2	2,402 2	2,738 6	6,012	9,203	
19 2,813	286	295	311	331	351	432	557	632	966	1,075	867	1,709	2,050	1,927	1,718 2	2,042 2	2,632 2	2,254	5,813	
20 2,045	193	205	212	221	247	319	408	541	0/17	743	632	1,138	1,287	1,271	1,206 1	1,491 1	1,988 2	2,000	1,932	LOCATION
MAX STORY SHEAR	3 531	6469	11 031	18 175	10 227	17 007	190 50	22 072 00	2770	10 675	10107	1 101 0	0 704	1 1 1 2 7 7 1	21 009 21	17 657 74	00 000 00	102.00	0 00 70	2 521

Table A2.23 Story shears after optimization for EQ11 data

Table A2.24 Story shears after optimization for EQ12 data

		18 19	15 2,902 2,298	15 8,315 8,191	52 8,666 8,362	8,206	7,949	7,570	01 7,103 6,850	6,514	20 5,928 6,098	36 5,667 5,849	5,378	5,341	34 5,423 5,576	5,393	72 5,227 5,852	39 4,832 5,730	76 4,249 5,337	1 3,414 4,659	78 3,726 3,765	23 1,726 2,881	
		17	28 3,235	55 9,145	80 9,452	95 8,902	77 8,592	9,310 8,146	40 7,591	8,187 6,949	7,633 6,320	7,042 5,786	5,325 5,381	5,431 5,192	40 5,084	4,510 4,854	3,937 4,472	3,174 3,889	5,324 3,176	2,785 4,611	2,230 2,478	,648 1,723	
		15 16	3,103 3,328	1,698 10,655	1,921 10,980	1,090 10,295	0,676 9,877	0,509 9,3	0,220 8,640				7,343 6,3	6,142 5,4	4,785 4,940	4,042 4,5	3,188 3,5	5,446 3,1	2,817 5,3	2,554 2,7	2,190 2,2	1,755 1,6	
		14 1	2,986 3,	2,265 11,	2,556 11,	-	1,382 10	0,917 10,	0,351 10		8,877 9,	7,886 8.	6,669 7,	5,276 6,	3,926 4.	3,098 4,	5,424 3,	2,899 5.	2,917 2,	3,165 2,	3,101 2	2,623 1,	
		13	2,572	13,318 1	13,473 13	_	11,836 1	11,120 10	10,337 10		8,382	7,400	6,220	4,779	3,310	4,882	2,515	2,760	3,311	3,569	3,428	2,818	
		12	1,956	13,781	13,787	12,576	11,843	11,023	10,147	9,288	8,247	6,980	5,508	3,951	4,120	2,005	2,038	2,184	2,486	2,554	2,330	1,914	
	EVEL	II	1,178	14,220	14,068	12,593	11,711	10,545	9,344	8,013	6,666	5,225	3,776	2,855	1,140	1,237	1,262	1,274	1,258	1,213	1,105	895	
	ISOLATOR LEVEL	10	1,177	11,945	12,101	11,160	10,532	9,711	8,746	7,541	5,979	4,038	2,853	1,208	1,336	1,411	1,408	1,326	1,175	1,178	1,088	906	
	ISO	6	1,160	12,132	11,966	10,652	9,884	8,788	7,572	5,975	4,212	2,522	3 1,139	1,234	1,316	1,354	1,328	1,240	5 1,196	1,189	1,078	853	
HEAR[tf]		8	0 1,094	0 11,901	5 11,301	9 9,644	0 8,373	8 6,898	2 5,350	6 3,611	3 2,250	5 1,042	66 998	966 0	6 1,027	8 1,070	1 1,062	1 1,064	6 1,055	610 L	6 832	9 663	
STORY SHEAR[tf]		7	,036 1,010	5,267 7,910	,535 7,275	1,255 6,009	,240 5,110	2,087 3,858	,495 2,662	955 1,716	900 923	862 865	820 816	799 760	879 856	924 908	921 901	863 831	746 786	712 75	615 656	449 479	
		5 6	,119 1,0	,463 6,2	,681 5,5	,312 4,2	2,222 3,2	,469 2,0	,042 1,4	983 9	941 9	910 8	880 8	848 7	881 8	887 9	860 9	797 8	694 7	639 7	540 6	382 4	
		4	,206 1,	1,596 5,	,620 4,	,168 3,	1,578 2,	,107 1,	,019 1,	949	868	885	868	874	877	854	802	720	648	583	484	351	
		3	1,314]	3,166 4	2,126 3	1,588 2	1,210	1,108	1,011	927	860	853	875	874	849	66L	729	664	651	598	505	371	
		2	1,368	1,715	1,728	1,261	1,154	1,050	961	916	894	867	856	831	786	727	672	605	605	567	486	361	
		-	1,414	1,669	1,307	1,213	1,145	1,091	1,045	1,004	996	930	893	852	808	758	700	633	556	521	452	339	
	EARTHQUAKE DATA: EQ 12	UNCONTROLLED BUILDING		6,811	6,742	6,648	6,524	6,369	6,185	5,969	5,722	5,442	5,132	4,793	4,429	4,034	3,920	4,221	4,276	4,053	3,538	2,717	
	EARTHQ	STORY	ISOLATOR FLOOR	-	2	3	4	5	9	7	8	6	10	П	12	13	14	15	16	17	18	19	