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# Influence of buffer layers on Ni thin film structure and graphene growth by CVD

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#### Abstract

Buffer and/or adhesive layers were used to decrease the dewetting of Ni thin film at graphene growth temperatures of around 900 °C. Depositing a thin buffer (Al<sub>2</sub>O<sub>3</sub>) layer onto SiO<sub>2</sub>/Si substrate significantly reduced the dewetting effect and surface roughness of Ni catalyst film. Thin adhesive (Cr) layers with or without Al<sub>2</sub>O<sub>3</sub> buffer layers increased the texturing in (1 1 1) orientation, which was promoted by growing at an elevated temperature (450 °C). The effects of pretreatment and growth temperature on crystal orientation, grain size and surface roughness of Ni film were analyzed. Our results indicated a large positive correlation coefficient between the film thickness and surface roughness for thinner and non-buffered films, and a negative correlation coefficient between the thickness and 900 °C -annealed film roughness for thicker and buffered films. The graphene coverage was greatly improved over the films grown with Al<sub>2</sub>O<sub>3</sub> and/or Cr layers. In summary, we suggest that growing high quality, large area, 1- or 2-layer graphene on polycrystalline Ni transition metal thin film is optimized by using Al<sub>2</sub>O<sub>3</sub> and/or Cr layers to reduce Ni dewetting, surface roughness, and groove depth while controlling grain size and texturing in (1 1 1) orientation by annealing at 900 °C.

Keywords: thin film dewetting, buffered growth, film pretreatment, CVD, graphene growth

S Online supplementary data available from stacks.iop.org/JPhysD/48/455302/mmedia

(Some figures may appear in colour only in the online journal)

## 1. Introduction

To obtain high-quality graphene, substantial efforts have been directed towards optimizing the chemical vapour deposition (CVD) conditions [1–3]; however, thin film, serving as both catalyst and support [4], has a pronounced effect on graphene growth, perhaps even overshadowing graphene growth conditions.

Compared to other widely used materials such as Cu, Pt, and Ir, graphitic layers grown on Ni substrate have been reported to possess a higher degree of crystallinity [5]. Additionally, particular studies have reported that graphene can easily grow on an (111) oriented Ni surface due to a reasonable lattice match [6–9] and to the lower energy existing at the interface than other crystallographic orientations [10, 11]. (It should be noted, however, that at least one study reports

that local binding variations can occur between graphene and the lattice-mismatched underlying metal, and yet not affect continuous graphene growth [12].) A further point of consideration is that Ni has higher dehydrogenation and carbon solubility at high temperatures than many other materials [13].

On a polycrystalline Ni surface, grain boundaries can interfere with carbon segregation, forming grooves with higher carbon concentration than for a less granular surface [3, 8, 14]. Multilayer graphene grows in these grooves, reducing precipitation uniformity [13, 15]. Thus, grain boundaries on polycrystalline Ni film can be detrimental to the mechanical and electrical properties of graphene [16, 17] and limit the graphene flake size [11, 18, 19].

Presenting a further complication, Ni grains tend to form clusters, and exposing the substrate surface to extreme temperatures results in Ni film dewetting. This effect is due to internal forces in the film being larger than those with a film and substrate, where excess energy is supplied by pretreatment [20-22] and the effect becomes more prominent (and increases surface roughness) with increasing temperature. To lessen the consequences of dewetting, thicker (>400 nm) Ni films have been used for graphene growth [23]. However, thicker films lead to more carbon solution in the film, which in turn leads to multilayer graphene growth. As an alternate counter measure, a buffer layer can be used to decrease the dewetting effect and reduce surface roughness; Al<sub>2</sub>O<sub>3</sub> has been widely used as a buffer layer on top of SiO<sub>2</sub> in the CVD growth of CNT and graphene [24-27]. Al<sub>2</sub>O<sub>3</sub> has high thermal conductivity and generally functions better than SiO<sub>2</sub> as a support layer for the hydrocarbon CVD process [28]. Additionally, Cr is a commonly used material that has a high oxidation tendency and increases the adherence of metal thin films onto substrate surfaces [19]. When used in conjunction with a metal, the  $Al_2O_3$ buffer prevents metal silicide formation between the substrate and the catalyst metal particles [29]. Moreover, metal on an oxide buffer layer exhibits much less mobility [30] due to increased adhesion [31] between the film and the substrate. Hence, to grow high-quality, large-area, and 1-2-layer graphene on polycrystalline Ni transition metal (TM) thin film is of fundamental importance to reduce Ni dewetting and the surface roughness and groove depth of Ni film, and to have the largest grain sizes and texturing in (111) orientation.

In this work, we investigated the importance of optimizing thin film properties for the CVD growth of graphene. Thin film properties, and hence graphene growth, were greatly enhanced by using a buffer ( $Al_2O_3$ ) and/or an adhesion layer (Cr). We demonstrated that reduced Ni dewetting and surface roughness and texturing in (111) orientation provided highquality, large-area graphene of 1–2 layers on polycrystalline Ni TM thin film.

# 2. Experimental details

Ni films with Al<sub>2</sub>O<sub>3</sub> and/or thin Cr layers were deposited on SiO<sub>2</sub>/Si wafers by magnetron sputtering. Cleaning and preparing the substrate prior to thin film deposition and graphene growth were carried out using an ultrasonic bath (details are given in the online supporting information) (stacks.iop.org/ JPhysD/48/455302/mmedia). The growth rates for various deposition powers were determined from the growth time and film thickness, measured both by cross-sectional SEM and a surface profiler. Ni films with and without an Al<sub>2</sub>O<sub>3</sub> and/or Cr buffer and adhesive layers were deposited over SiO<sub>2</sub>( $\mu$ m)/ Si and SiO<sub>2</sub>(230 nm)/Si substrates. Some samples were grown with substrate heating, which was accomplished using halogen heaters behind the substrate. All the films were grown under 9.95 sccm Ar flow.

For grain enlargement, the films were annealed at 800, 900, and 950 °C under 150 sccm Ar flow environmental pressure for 60 min. All the as-grown and annealed films were characterized by XRD, AFM, SEM, and surface profilometry. The XRD patterns were collected with a Philips X'Pert diffractometer with Cu K $\alpha$  radiation and analysed with X'pert HighScore Peak Search software. The crystal qualities were analysed by the peak intensity ratios from XRD  $\theta$ -2 $\theta$  measurements and grain sizes were calculated using Scherer's formula. The surface roughness determinations of the films were obtained from AFM surface topography measurements. SEM was used for topography and thickness measurements.

To grow graphene over films with various thicknesses, numerous growth parameters were applied using atmospheric pressure CVD (see the online supporting information) (stacks. iop.org/JPhysD/48/455302/mmedia). Ar and/or H<sub>2</sub> were introduced for 20 or 50 min before introducing CH<sub>4</sub>. A 20 or 50 min pretreatment process with respective 40 or 10 min carbon dissolution times was used. The growths were also carried out at 800, 900, and 950 °C. The heating rate was 28 °C min<sup>-1</sup>. The CVD process was terminated by stopping the CH<sub>4</sub> or CH<sub>4</sub>:H<sub>2</sub> flow and the temperature of the chamber was cooled at 1, 2, 3, 4, 5, 10, or 15 °C min<sup>-1</sup>.

Raman spectroscopy was used to identify the number of graphene layers on the Ni films as they were grown, without transferring to another substrate. An Ar-ion laser operating at 514.5 nm (2.41 eV) with a 600 groove  $mm^{-1}$  grating was used to obtain D, G, and G' bands.

#### 3. Results and discussion

#### 3.1. Scope of work

In this study, eighteen films (referenced as Ni1 through Ni18) with four different structures were grown and characterized (figure 1(a)). Initially, Ni films of various thicknesses were grown on SiO<sub>2</sub>/Si substrates. Later, buffer layers including Al<sub>2</sub>O<sub>3</sub>, Cr, and Cr/Al<sub>2</sub>O<sub>3</sub> were grown prior to the Ni film growth to improve the adherence of the films to the substrate at elevated temperatures. The growth parameters for the films are summarized in figure 1(b), along with the film thickness.

#### 3.2. Temperature

It has been reported that the number of layers and the size of CVD-grown graphene are limited by the grain size of crystalline Ni films obtained after thermal annealing [8, 32]. This theory was tested in the initial part of the study, during which Ni films grown on SiO<sub>2</sub>/Si substrates were studied. These films were also used later on to show the effect of the buffer layers. XRD  $\theta$ -2 $\theta$  scans of the as-grown, 800, and 900 °C -annealed Ni films indicated that increasing the pretreatment temperature favoured texture in (111) orientation (figure 2). Furthermore, the average crystallite sizes were increased with the increasing pretreatment temperature (figure 2 inset). Annealing at 800 °C was not sufficient to effectively disassociate the CH<sub>4</sub> to obtain enough carbon and drive it into the film to sustain graphene growth. Therefore, graphene growth was carried out at 900 °C or higher.

It is generally accepted that during pretreatment, thin film tends to decrease its excess energy by minimizing the interfacial surface area between itself and the substrate [33]. The surface roughness increases and parts of the substrate might



**Figure 1.** (a) Layer structures of Ni films with the sample numbers deposited on  $SiO_2/Si$ ; (\*) indicates that these films were deposited with substrate heating at 450 °C. (b) Composite plot of the dc/RF power, deposition time, and thickness of layers.



**Figure 2.** XRD  $\theta$ -2 $\theta$  scans of Ni1 samples. 2 $\theta$  positions and average grain size values of the as-grown (blue), 800 °C (red), and 900 °C (black) annealed samples are given inside the plot.

be exposed, depending on the film thickness and degree of dewetting. The granular structure of the films and the effects of annealing were analysed with SEM and AFM. Figure 3 shows SEM and AFM topographic images of a 230 nm thick Ni4 film ((a) and (b)) and a 400 nm thick Ni13 film ((c) and (d)) without buffer layers or with a  $Al_2O_3$  buffer layer (Ni11 (e) and (f)), annealed at 900 °C. The surface roughness values

are shown in figure 5. As can be clearly seen, the smoothest and least dewetted film is Ni11 with an  $Al_2O_3$  buffer layer (the average rms value of Ni11 is about 38.8 nm; Ni13 is about 72.9 nm). Dewetting also increased with the pretreatment temperature. (Note: to achieve a continuous film and texture in (111) orientation at temperatures of 900 °C or above,  $Al_2O_3$ buffer layers and/or Cr adhesive layers were deposited prior to the Ni film growth, as discussed below.)

# 3.3. Structure

Both substrate and buffer layers have characteristic peaks very close to the  $2\theta$  peak position of Ni (111). A simple calculation involving the atomic structure factor based on the FCC structure of Ni films yields a (111) peak position at  $2\theta = 44.49^{\circ}$  (see the online supporting information) (stacks.iop.org/JPhysD/48/455302/mmedia). Thermally grown SiO<sub>2</sub> is usually amorphous and has a broad peak centred at 43°. The NiO peak is at 43.3°, the Al<sub>2</sub>O<sub>3</sub> peak is at 43.9°, and the Cr peak is at 44.2°. In analysing the XRD  $\theta$ -2 $\theta$  measurement results of all the as-grown and annealed Ni films to calculate the grain sizes, the peaks appearing at this position were carefully fitted by considering all possible contributions from the substrate, buffer-adhesive layers, and NiO (figure 4).

All the as-grown Ni films were polycrystalline. The as-grown Ni1-6 films were grown along the (111) direction and a well-defined (111) peak appeared at  $44.50^{\circ}$ .



**Figure 3.** SEM micrographs (a), (c), and (e) and AFM topographic images (b), (d), and (f) of Ni4 (a) and (b), Ni13 (c) and (d) and Ni11 (e and f) films annealed at 900 °C. The scale bar on the SEM images indicates 10  $\mu$ m.

Among these layers, the film grown with the lowest power and least thickness had the greatest texturing in the (111) orientation.

The Ni7 film was grown with a  $30 \text{ nm Al}_2O_3$  buffer layer and the film 8 was grown with a  $60 \text{ nm Al}_2O_3$  buffer layer. The intensity ratios of the Ni (111) peak to other orientation were higher in the XRD measurements of the annealed Ni7 film compared to those of the Ni8 film. This was an indication of the thinner buffer more effectively favouring the (111) orientation of the Ni film (see the online supporting information) (stacks.iop.org/JPhysD/48/455302/mmedia).

To study the effects of Ni film thickness on crystal orientation, ~400 nm thick layers (Ni11-14) were grown. All four were grown on a SiO<sub>2</sub>/Si substrate; Ni11 and Ni12 also had an Al<sub>2</sub>O<sub>3</sub> buffer layer. The SiO<sub>2</sub> layer thickness was 1  $\mu$ m for Ni11 and Ni13 and 230 nm for Ni12 and Ni14. Annealing these samples increased texturing in the (220) direction for all four samples. There was a large strain in the as-grown samples, as indicated by the upshifts of the XRD peak positions of the samples with the annealing due to strain relief (see the online supporting information figure S2) (stacks.iop.org/ JPhysD/48/455302/mmedia). The strain was 52% and 44% for Ni11 and Ni13, respectively, and 38% and 31% for Ni12 and Ni 14, respectively. The buffer layer of Ni11 and Ni12 apparently further contributed to strain relief.

#### 3.4. Substrate heating

Some studies have reported an increase in texturing in the (111) orientation by heating the substrate during thin film deposition [34]. To study the effects of substrate heating on texture, two 100 nm thick Ni films (Ni9 and Ni10) were grown at a substrate temperature of 450 °C. These films, however, exhibited dominant texturing in the (200) orientation (see the online supporting information) (stacks.iop.org/JPhysD/48/455302/mmedia).

Ni17 and Ni18 were also deposited by substrate heating at 450 °C. Ni17 had Cr/Al<sub>2</sub>O<sub>3</sub> and Ni18 had a Cr buffer over the SiO<sub>2</sub>/Si substrate. Similar to Ni9-10, these as-grown films were predominantly oriented in the (200) direction as compared to the samples deposited under the same conditions but without substrate heating. Nevertheless, the non-buffered Ni9 and Ni10 films had lower intensity (111) peaks in contrast to the Ni17 and Ni18 films. Therefore, it can be concluded that the Cr buffer caused the Ni film to have (111) preferentially oriented grains. Moreover, when annealing on the samples with a Cr buffer was performed for 60 min, the intensity ratio of (111)/(200) further increased. When the Ni7, Ni8, Ni11, and Ni12 films were compared with the Ni15-18 films, it was seen that the contribution of the Cr layer was more than that of the  $Al_2O_3$  buffer layer in texturing Ni film in the (111) orientation.



**Figure 4.** Fitted XRD  $\theta$ -2 $\theta$  measurements of Ni18 (a) and Ni16 (b) films. The black line indicates the as-grown and the light blue line indicates annealing at 900 °C for 60 min.

The average grain sizes of the crystallites in the (111) orientation were calculated by using Scherer's formula. The average grain sizes for all the as-grown samples were roughly the same. The grain sizes increased with increasing the annealing temperature (see the online supporting information figure S4) (stacks.iop.org/JPhysD/48/455302/mmedia).

#### 3.5. Surface roughness

The surface roughness (root mean square, RMS values) of both the as-grown and annealed Ni films was obtained by averaging several AFM topography images for each sample. Figure 5 shows the comparison of the as-grown thickness to the as-grown roughness and roughness after 900 °C annealing of all the Ni films studied here. The film thickness was obtained by both surface profilometry and cross-sectional SEM. The thickness measurements obtained by both techniques were in very good agreement. A striking similarity between the thickness and as-grown roughness measurements was observed, even though they were obtained with different techniques. There was a large positive correlation between the thickness and as-grown film roughness (Pearson correlation coefficient of 0.671), particularly for Ni films 1-8, for which the positive correlation coefficient between the thickness and as-grown roughness RMS values was 0.982, and between the thickness and annealed film roughness was 0.884. On the other hand, there was a negative correlation coefficient between the thickness and annealed (900 °C) film roughness of -0.651 for films 9-18. That is, as the film thickness increased the annealed film roughness decreased even though the as-grown roughness increased. Therefore, it can be said that the annealed film roughness was inversely proportional to the thickness for the thicker film numbers 12-18 (see the online supporting information) (stacks.iop.org/JPhysD/48/455302/mmedia).

Figure 5 also clearly shows a contribution from the buffer layer and thickness on the Ni film properties. Upon inspecting the annealed samples with lower roughness RMS values, it was evident that those with an  $Al_2O_3$  buffer (Ni7, Ni8, Ni11, and Ni12 films) had a smoother surface compared to those without an  $Al_2O_3$  buffer (Ni films of 1–6, 13 and 14). (The Ni9 and Ni10 films were grown with substrate heating, and thus are not included in the discussion.)

No significant difference was observed between the asgrown roughness RMS values of thicker (about 400 nm) Ni films (11, 12, 13, and 14). However, when the Ni film thickness and roughness RMS values of the annealed samples were compared, it was evident that the thicker Ni films (13 and 14) had almost two times higher roughness than those with  $Al_2O_3$ buffer layers (11 and 12). In addition, increasing the Ni film thickness resulted in bigger Ni particles on the surface (figure 3), whereas the average crystallite size did not change significantly (see the online supporting information figure S4) (stacks.iop.org/JPhysD/48/455302/mmedia). Hence, it can be concluded that the  $Al_2O_3$  buffer was very effective in reducing the roughness of the Ni films at high temperatures (figure 5).

Sputtering power also had a strong influence on the asgrown film roughness. Films grown with a higher power but shorter time for a thickness of 400 nm (Ni15 through Ni18) had a substantially increased surface roughness (figure 5). The  $Al_2O_3$  buffer layer helped somewhat to decrease the surface roughness. On the other hand, annealing successfully reduced the roughness of the films to those of films grown with a lower power (figure 5).

In this study, all the AFM surface topography images were in very good agreement with the SEM surface morphology images (figure 3), although different locations were scanned over the surface. In addition, the columnar growth ( $T_d \ge 0.2$ – 0.3  $T_m$  [35],) of the Ni films was observed from the crosssectional SEM images. The films with approximately 100 nm thick Ni layers had a higher as-grown roughness when deposited with substrate heating at 450 °C (Ni films 9 and 10). Nevertheless, when we annealed these samples, roughness RMS values very close to those of the buffered films (Ni7 and 8) were achieved (figure 5).



**Figure 5.** The relation between the thickness and surface roughness (RMS) values of all the as-grown and annealed at 900  $^{\circ}$ C cases. The as-grown roughness is drawn at a different scale to help visual comparison.

#### 3.6. Raman spectroscopy

Graphene growth and characterization were carried out on the aforementioned eighteen Ni thin films using various CVD growth parameters. The growths were carried out in an atmospheric pressure CVD system (see online supporting information) (stacks.iop.org/JPhysD/48/455302/mmedia). Confocal Raman spectroscopy was used to assess the presence and the quality of the graphene. There are three prominent peaks in the Raman spectra of graphene: The G band, which is the only first order Raman scattering appearing at about 1585 cm<sup>-1</sup>; the D band appearing at about 1350 cm<sup>-1</sup>, which is induced by disorder; and the G' band (also called 2 D) at about  $2700 \text{ cm}^{-1}$ , achieved using laser excitation at 2.41 eV (514 nm wavelength). The number of graphene layers can be obtained from Raman measurements by comparing G-peak to G'-peak intensity  $(I_G/I_G)$  and full width at the half maximum (FWHM) value of the G' band (2D band) [36-38]. A large number of spectra were collected over a sample surface by manual focusing. Raman spectra were fit with Lorentzian functions to obtain peak position and FWHMs. In addition to the quality of fit (value of the coefficient of determination, or  $R^2$ ) and FWHMs of the fit, the intensity ratios of the G and G' bands  $(I_G/I_G)$  were also compared. A single-peak Lorentzian fit to the G' peak and  $I_{\rm G}/I_{\rm G} < 0.5$  indicates that the measurement is coming from mono-layer graphene and a two-peak Lorentzian fit points to bi-layer turbostratic graphene on the Ni film surface [39, 40].

A representative Raman spectrum of graphene growth (GRP20, graphene growth no. 20) on Ni1 film is shown in figure 6. For this measurement the G' band can be fit with a Lorentzian peak with a FWHM of  $28.9 \text{ cm}^{-1}$  ( $R^2 = 0.9982$ ). The same peak can also be fit by two Lorentzian peaks, but with FWHMs of  $24.2 \text{ cm}^{-1}$  and  $24.5 \text{ cm}^{-1}$  ( $R^2 = 0.9998$ ). For the GRP20 sample, the  $I_G/I_G$  ratio was about 0.30 and the FWHM of the G' band was  $29 \text{ cm}^{-1}$ . Although the Raman spectrum shows high-quality graphene, this kind of spectra was only available in sporadic areas of the sample. This is very probably due to the dewetting of the Ni film. When

we increased the CH<sub>4</sub> flow, the FWHMs of grown graphene layers decreased to a value of approximately  $28 \text{ cm}^{-1}$  with  $I_G/I_G$  ratio of about 0.34. Considering interlayer coupling and reported Raman measurements, these spectra may be assumed due to monolayer graphene [2, 38].

Among all the observed G' band Raman spectra, when the number of graphene layers was more than two, the FWHM values were greater than  $50 \text{ cm}^{-1}$  and the  $I_G/I_{G'}$  ratio was larger than 1. For these, the G' band was fitted by more than three Lorentzian peaks. On the other hand, for 1 to 2-layer graphene, with a FWHM  $< 50 \text{ cm}^{-1}$  and  $I_G/I_{G'} < 1$ , the G' band can be fitted by at most three Lorentzian peaks.

#### 3.7. CH<sub>4</sub> flow

To enlarge the grain sizes in polycrystalline Ni films and thus to obtain larger graphene flakes, growth temperatures of 900 and 950 °C were used. At these temperatures, we found that there was a certain minimum requirement on the CH<sub>4</sub> flow rate of 8 sccm, which led to the growth of 1-2 layer graphene with narrow G' band FWHMs and with small D peaks. Moreover, 1-2-layer graphene flakes were sparsely distributed over thinner films (~100nm) at 1-8 sccm CH<sub>4</sub> flow at 900 °C (an example of growth over Ni1 is given above). On the contrary, on thicker films (thickness  $\ge 160$  nm), 1–2 layers of graphene grew with 8 sccm  $CH_4$  flow; however, their G' peaks were broad with FWHMs of  $38-56 \text{ cm}^{-1}$  and the D and D' peak intensities were larger compared to those obtained on thinner films (figure 7). Therefore, the CH<sub>4</sub> flow was increased to 20-30 sccm for target 400 nm film thickness. Under a sufficiently high CH<sub>4</sub> flow, the growth temperature of 900 °C was enough to considerably suppress the D and D' intensity ratios. However, the D' peak, which is also related to defects, became noticeable around  $1610 \,\mathrm{cm}^{-1}$  for these growths (an example, GRP50, is given in figure 7).

Ni films with buffer and/or adhesive layers (Ni11 and Ni12) had lower roughness RMS values after annealing. This led to the successful growth of 1–2-layer graphene on these



**Figure 6.** (a) G' band Raman spectrum of a GRP20 sample grown on Ni1 film by method 3 (see the online supporting information, table S1) (stacks.iop.org/JPhysD/48/455302/mmedia). The green and blue lines are the components of the red line, which is the fitting result. (b) The same result fit with a single Lorentzian peak. (c) The whole range of the respective spectrum.



**Figure 7.** Raman spectrum of a GRP50 sample grown on a Ni5 substrate by method 4 (see the online supporting information, table S1) (stacks.iop.org/JPhysD/48/455302/mmedia). The green lines refer to the component of the red line, which is the calculated profile. The inset is the optical image of the area where the spectrum was collected and the red circle indicates the approximate position of the laser spot.

films. The large number of spectra collected over the surface by manual focusing confirms that a large portion of the surfaces were in fact covered by mostly 1-2 layer graphene.

#### 3.8. Graphene coverage

Graphene surface coverage with the film thickness and buffer layer was also studied. The SEM images of graphene growth (GRP23) carried over Ni4 film at 900 °C are shown in figures 8(a) and (b). Ni4 had a Ni film grown on SiO<sub>2</sub>/Si with no buffer layer and had the largest (~230 nm) Ni thickness of the group. The annealed sample was extensively dewetted (see figure 3). An SEM image with graphene growth was taken at least the dewetted part of the sample (figures 8(a) and (b)). The darkest areas are the exposed SiO<sub>2</sub> substrate. Graphene growth over the remaining Ni part can be seen as darker regions. The grain boundary regions can also be distinguished. GRP31 was grown on Ni14 film and GRP28 was grown on Ni11 film with the same growth conditions of GRP23. Ni14 film (~400 nm) is thicker than Ni4 film, but also without a buffer layer, thus Ni film is less affected by dewetting. The effect of thickness on graphene coverage can be easily seen by comparing figures 8(a) and (b). Figure 8(c) has almost full coverage over the surface. Graphene grew over the Ni grains, yielding monolayer to multilayer growth. The line profile of SEM image, as indicated by a red line in figure 8(c), can be utilized to gain an impression about the number of graphene layers (figure 8(d)). This is in good agreement with the number of layers of graphene obtained by Raman spectroscopy. Comparing the sample grown over no buffer layer (figure 8(e)) and a buffer



**Figure 8.** SEM images of GRP23 (a and b) GRP31 (c) and (e) and GRP28 (f) at different magnifications. (d) One-dimensional grey value analysis of the red line on (c). (g) Raman spectra of the GRP28 sample which was grown on the Ni11 substrate. The red spectrum and black spectrum belong to different areas on the same film surface. The scale bars on the SEM images of (b), (e), and (f) are 2  $\mu$ m; (a) and (c) are 10  $\mu$ m.

layer (figure 8(f)) of the same thickness and the same growth parameters clearly demonstrates the effect of the buffer layer. The film with a buffer layer had a continuous 1–2-layer graphene growth over the same range.

# 4. Conclusions

Our study indicated that for thinner films (<230 nm) the surface roughness increased with thickness for both the as-grown and annealed samples. On the other hand, for the annealed

thicker films (~400 nm), the surface roughness was inversely proportional to the thickness.

Increasing the annealing temperature resulted in preferential texture in the  $(1 \ 1 \ 1)$  orientation and increased the average grain size; however, it also increased dewetting. Including an Al<sub>2</sub>O<sub>3</sub> buffer layer reduced the dewetting effect, a result that was more pronounced in thicker Ni films. Ni films with a thinner Al<sub>2</sub>O<sub>3</sub> buffer layer (about 30 nm) also had a more pronounced (111) orientated surface than non-buffered Ni films. Between films deposited with an Al<sub>2</sub>O<sub>3</sub> buffer layer, a Cr adhesive layer, and both Al<sub>2</sub>O<sub>3</sub>/Cr layers, the effect of the Cr adhesive layer was greater than that of the Al<sub>2</sub>O<sub>3</sub> buffer layer on texturing in the (1 1 1) orientation of the crystal. Film deposition at a substrate temperature of 450 °C led to (200) oriented Ni film growth. A Cr adhesive layer and 60 min annealing led to Ni films mostly textured in the (1 1 1) direction, even with the substrate heating during deposition. Cr layers increased the as-grown film surface roughness dramatically, but annealing restored the roughness to that of the same thickness films without an Al<sub>2</sub>O<sub>3</sub> layer.

No graphene growth was observed at 800 °C. At 900 and 950 °C, a CH<sub>4</sub> flow rate of 8 sccm was necessary to grow mono or bi-layer graphene with narrow FWHMs and with small D peaks. Under a low CH<sub>4</sub> flow rate over Ni film thicker than 160 nm, mono or bi-layer graphene with broad G' peak FWHMs (38–56 cm<sup>-1</sup>) and significant D and D' peaks was obtained, whereas a CH<sub>4</sub> flow rate of 20–30 sccm for 400 nm thick Ni films restored these values. Ni films with buffer and/ or adhesive layers had lower roughness RMS values after annealing and larger area graphene was successfully grown.

In summary, we suggest that growing high-quality, largearea, 1- or 2-layer graphene on polycrystalline Ni transition metal thin film is optimized by using buffer and/or adhesive layers.

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